

**EXAMPLE 1 Eigenvalue Problem**

Find the eigenvalues and eigenvectors of the matrix

$$(16) \quad \mathbf{A} = \begin{bmatrix} -4.0 & 4.0 \\ -1.6 & 1.2 \end{bmatrix}.$$

**Solution.** The characteristic equation is the quadratic equation

$$\det[\mathbf{A} - \lambda\mathbf{I}] = \begin{vmatrix} -4 - \lambda & 4 \\ -1.6 & 1.2 - \lambda \end{vmatrix} = \lambda^2 + 2.8\lambda + 1.6 = 0.$$

It has the solutions  $\lambda_1 = -2$  and  $\lambda_2 = -0.8$ . These are the eigenvalues of  $\mathbf{A}$ .

Eigenvectors are obtained from (14\*). For  $\lambda = \lambda_1 = -2$  we have from (14\*)

$$\begin{aligned} (-4.0 + 2.0)x_1 + 4.0x_2 &= 0 \\ -1.6x_1 + (1.2 + 2.0)x_2 &= 0. \end{aligned}$$

A solution of the first equation is  $x_1 = 2$ ,  $x_2 = 1$ . This also satisfies the second equation. (Why?). Hence an eigenvector of  $\mathbf{A}$  corresponding to  $\lambda_1 = -2.0$  is

$$(17) \quad \mathbf{x}^{(1)} = \begin{bmatrix} 2 \\ 1 \end{bmatrix}. \quad \text{Similarly,} \quad \mathbf{x}^{(2)} = \begin{bmatrix} 1 \\ 0.8 \end{bmatrix}$$

is an eigenvector of  $\mathbf{A}$  corresponding to  $\lambda_2 = -0.8$ , as obtained from (14\*) with  $\lambda = \lambda_2$ . Verify this. ■

## 4.1 Systems of ODEs as Models

We first illustrate with a few typical examples that systems of ODEs can serve as models in various applications. We further show that a higher order ODE (with the highest derivative standing alone on one side) can be reduced to a first-order system. Both facts account for the practical importance of these systems.

**EXAMPLE 1 Mixing Problem Involving Two Tanks**

A mixing problem involving a single tank is modeled by a single ODE, and you may first review the corresponding Example 3 in Sec. 1.3 because the principle of modeling will be the same for two tanks. The model will be a system of two first-order ODEs.

Tank  $T_1$  and  $T_2$  in Fig. 77 contain initially 100 gal of water each. In  $T_1$  the water is pure, whereas 150 lb of fertilizer are dissolved in  $T_2$ . By circulating liquid at a rate of 2 gal/min and stirring (to keep the mixture uniform) the amounts of fertilizer  $y_1(t)$  in  $T_1$  and  $y_2(t)$  in  $T_2$  change with time  $t$ . How long should we let the liquid circulate so that  $T_1$  will contain at least half as much fertilizer as there will be left in  $T_2$ ?

**Solution.** *Step 1. Setting up the model.* As for a single tank, the time rate of change  $y_1'(t)$  of  $y_1(t)$  equals inflow minus outflow. Similarly for tank  $T_2$ . From Fig. 77 we see that

$$y_1' = \text{Inflow/min} - \text{Outflow/min} = \frac{2}{100}y_2 - \frac{2}{100}y_1 \quad (\text{Tank } T_1)$$

$$y_2' = \text{Inflow/min} - \text{Outflow/min} = \frac{2}{100}y_1 - \frac{2}{100}y_2 \quad (\text{Tank } T_2).$$

Hence the mathematical model of our mixture problem is the system of first-order ODEs

$$y_1' = -0.02y_1 + 0.02y_2 \quad (\text{Tank } T_1)$$

$$y_2' = 0.02y_1 - 0.02y_2 \quad (\text{Tank } T_2).$$

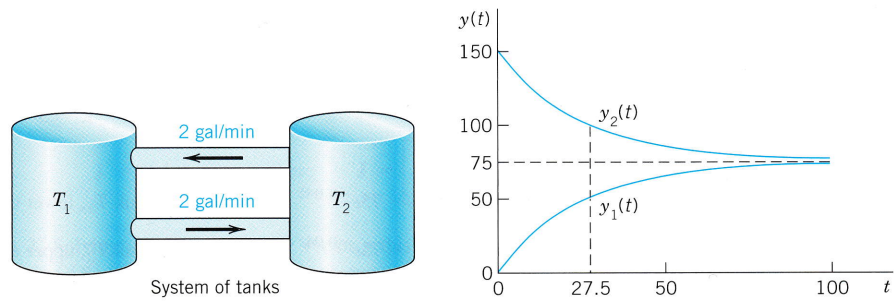


Fig. 77. Fertilizer content in Tanks  $T_1$  (lower curve) and  $T_2$

As a vector equation with column vector  $\mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \end{bmatrix}$  and matrix  $\mathbf{A}$  this becomes

$$\mathbf{y}' = \mathbf{A}\mathbf{y}, \quad \text{where} \quad \mathbf{A} = \begin{bmatrix} -0.02 & 0.02 \\ 0.02 & -0.02 \end{bmatrix}.$$

**Step 2. General solution.** As for a single equation, we try an exponential function of  $t$ ,

$$(1) \quad \mathbf{y} = \mathbf{x}e^{\lambda t}. \quad \text{Then} \quad \mathbf{y}' = \lambda \mathbf{x}e^{\lambda t} = \mathbf{A}\mathbf{x}e^{\lambda t}.$$

Dividing the last equation  $\lambda \mathbf{x}e^{\lambda t} = \mathbf{A}\mathbf{x}e^{\lambda t}$  by  $e^{\lambda t}$  and interchanging the left and right sides, we obtain

$$\mathbf{A}\mathbf{x} = \lambda \mathbf{x}.$$

We need nontrivial solutions (solutions that are not identically zero). Hence we have to look for eigenvalues and eigenvectors of  $\mathbf{A}$ . The eigenvalues are the solutions of the characteristic equation

$$(2) \quad \det(\mathbf{A} - \lambda \mathbf{I}) = \begin{vmatrix} -0.02 - \lambda & 0.02 \\ 0.02 & -0.02 - \lambda \end{vmatrix} = (-0.02 - \lambda)^2 - 0.02^2 = \lambda(\lambda + 0.04) = 0.$$

We see that  $\lambda_1 = 0$  (which can very well happen—don't get mixed up—it is *eigenvectors* that must not be zero) and  $\lambda_2 = -0.04$ . Eigenvectors are obtained from (14\*) in Sec. 4.0 with  $\lambda = 0$  and  $\lambda = -0.04$ . For our present  $\mathbf{A}$  this gives [we need only the first equation in (14\*)]

$$-0.02x_1 + 0.02x_2 = 0 \quad \text{and} \quad (-0.02 + 0.04)x_1 + 0.02x_2 = 0,$$

respectively. Hence  $x_1 = x_2$  and  $x_1 = -x_2$ , respectively, and we can take  $x_1 = x_2 = 1$  and  $x_1 = -x_2 = 1$ . This gives two eigenvectors corresponding to  $\lambda_1 = 0$  and  $\lambda_2 = -0.04$ , respectively, namely,

$$\mathbf{x}^{(1)} = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \quad \text{and} \quad \mathbf{x}^{(2)} = \begin{bmatrix} 1 \\ -1 \end{bmatrix}.$$

From (1) and the superposition principle (which continues to hold for systems of homogeneous linear ODEs) we thus obtain a solution

$$(3) \quad \mathbf{y} = c_1 \mathbf{x}^{(1)} e^{\lambda_1 t} + c_2 \mathbf{x}^{(2)} e^{\lambda_2 t} = c_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} + c_2 \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{-0.04t}$$

where  $c_1$  and  $c_2$  are arbitrary constants. Later we shall call this a **general solution**.

**Step 3. Use of initial conditions.** The initial conditions are  $y_1(0) = 0$  (no fertilizer in tank  $T_1$ ) and  $y_2(0) = 150$ . From this and (3) with  $t = 0$  we obtain

$$\mathbf{y}(0) = c_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} + c_2 \begin{bmatrix} 1 \\ -1 \end{bmatrix} = \begin{bmatrix} c_1 + c_2 \\ c_1 - c_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 150 \end{bmatrix}.$$

In components this is  $c_1 + c_2 = 0$ ,  $c_1 - c_2 = 150$ . The solution is  $c_1 = 75$ ,  $c_2 = -75$ . This gives the answer

$$y = 75x^{(1)} - 75x^{(2)}e^{-0.04t} = 75 \begin{bmatrix} 1 \\ 1 \end{bmatrix} - 75 \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{-0.04t}.$$

In components,

$$y_1 = 75 - 75e^{-0.04t} \quad (\text{Tank } T_1, \text{ lower curve})$$

$$y_2 = 75 + 75e^{-0.04t} \quad (\text{Tank } T_2, \text{ upper curve}).$$

Figure 77 shows the exponential increase of  $y_1$  and the exponential decrease of  $y_2$  to the common limit 75 lb. Did you expect this for physical reasons? Can you physically explain why the curves look “symmetric”? Would the limit change if  $T_1$  initially contained 100 lb of fertilizer and  $T_2$  contained 50 lb?

**Step 4. Answer.**  $T_1$  contains half the fertilizer amount of  $T_2$  if it contains 1/3 of the total amount, that is, 50 lb. Thus

$$y_1 = 75 - 75e^{-0.04t} = 50, \quad e^{-0.04t} = \frac{1}{3}, \quad t = (\ln 3)/0.04 = 27.5.$$

Hence the fluid should circulate for at least about half an hour. ■

### EXAMPLE 2 Electrical Network

Find the currents  $I_1(t)$  and  $I_2(t)$  in the network in Fig. 78. Assume all currents and charges to be zero at  $t = 0$ , the instant when the switch is closed.

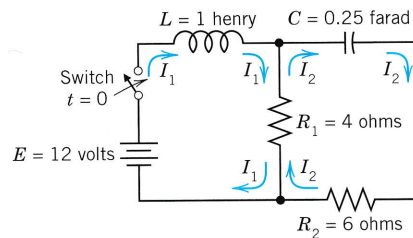


Fig. 78. Electrical network in Example 2

**Solution. Step 1. Setting up the mathematical model.** The model of this network is obtained from Kirchhoff's voltage law, as in Sec. 2.9 (where we considered single circuits). Let  $I_1(t)$  and  $I_2(t)$  be the currents in the left and right loops, respectively. In the left loop the voltage drops are  $LI_1' = I_1'$  [V] over the inductor and  $R_1(I_1 - I_2) = 4(I_1 - I_2)$  [V] over the resistor, the difference because  $I_1$  and  $I_2$  flow through the resistor in opposite directions. By Kirchhoff's voltage law the sum of these drops equals the voltage of the battery; that is,  $I_1' + 4(I_1 - I_2) = 12$ , hence

$$(4a) \quad I_1' = -4I_1 + 4I_2 + 12.$$

In the right loop the voltage drops are  $R_2I_2 = 6I_2$  [V] and  $R_1(I_2 - I_1) = 4(I_2 - I_1)$  [V] over the resistors and  $(1/C)\int I_2 dt = 4 \int I_2 dt$  [V] over the capacitor, and their sum is zero,

$$6I_2 + 4(I_2 - I_1) + 4 \int I_2 dt = 0 \quad \text{or} \quad 10I_2 - 4I_1 + 4 \int I_2 dt = 0.$$

Division by 10 and differentiation gives  $I_2' - 0.4I_1' + 0.4I_2 = 0$ .

To simplify the solution process, we first get rid of  $0.4I_1'$ , which by (4a) equals  $0.4(-4I_1 + 4I_2 + 12)$ . Substitution into the present ODE gives

$$I_2' = 0.4I_1' - 0.4I_2 = 0.4(-4I_1 + 4I_2 + 12) - 0.4I_2$$