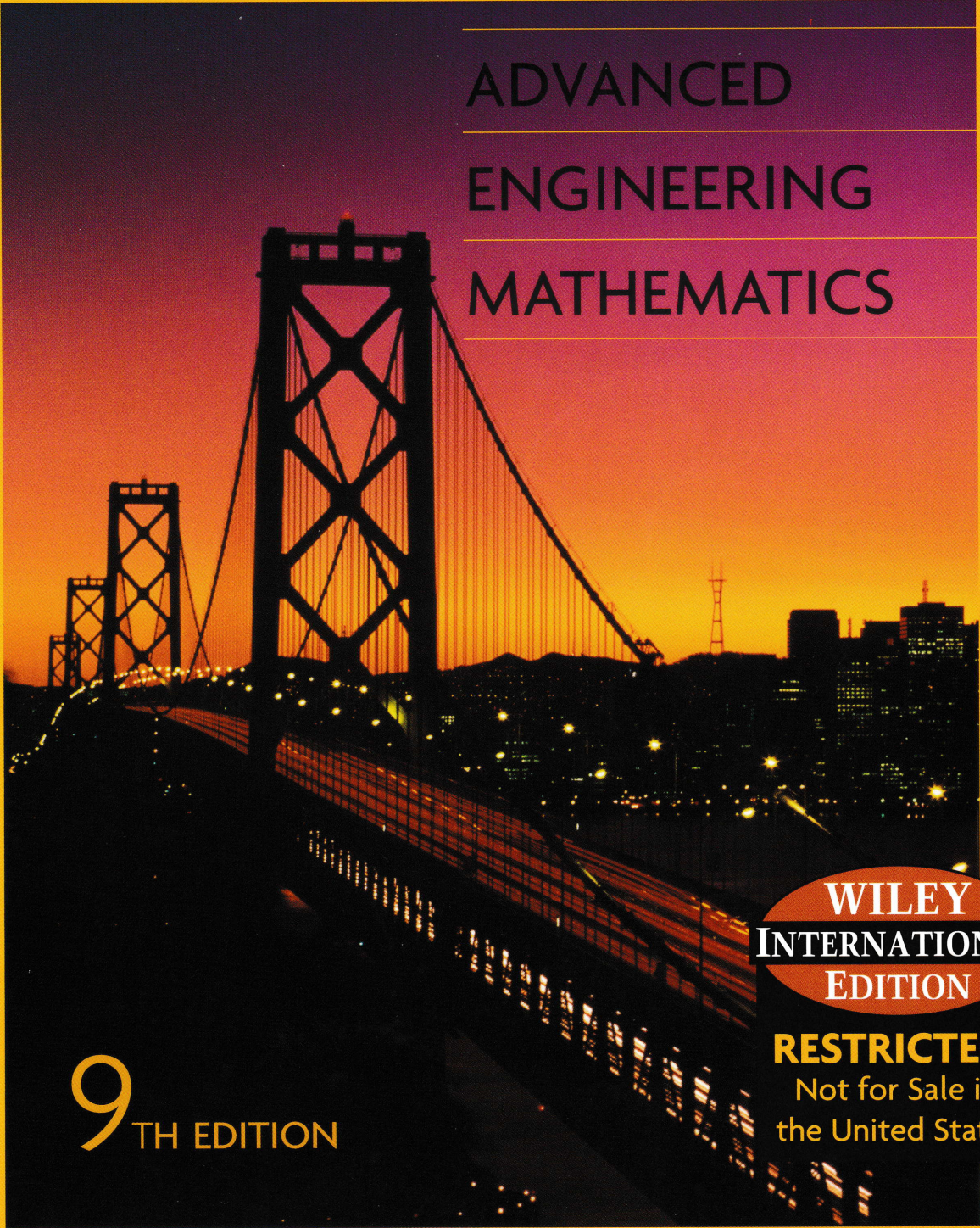


# ERWIN KREYSZIG



ADVANCED  
ENGINEERING  
MATHEMATICS

9<sup>TH</sup> EDITION

WILEY  
INTERNATIONAL  
EDITION

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the United States

## Systems of Units. Some Important Conversion Factors

The most important systems of units are shown in the table below. The mks system is also known as the *International System of Units* (abbreviated *SI*), and the abbreviations s (instead of sec), g (instead of gm), and N (instead of nt) are also used.

System of units	Length	Mass	Time	Force
cgs system	centimeter (cm)	gram (gm)	second (sec)	dyne
mks system	meter (m)	kilogram (kg)	second (sec)	newton (nt)
Engineering system	foot (ft)	slug	second (sec)	pound (lb)

$$1 \text{ inch (in.)} = 2.540000 \text{ cm}$$

$$1 \text{ foot (ft)} = 12 \text{ in.} = 30.480000 \text{ cm}$$

$$1 \text{ yard (yd)} = 3 \text{ ft} = 91.440000 \text{ cm}$$

$$1 \text{ statute mile (mi)} = 5280 \text{ ft} = 1.609344 \text{ km}$$

$$1 \text{ nautical mile} = 6080 \text{ ft} = 1.853184 \text{ km}$$

$$1 \text{ acre} = 4840 \text{ yd}^2 = 4046.8564 \text{ m}^2$$

$$1 \text{ mi}^2 = 640 \text{ acres} = 2.5899881 \text{ km}^2$$

$$1 \text{ fluid ounce} = 1/128 \text{ U.S. gallon} = 231/128 \text{ in.}^3 = 29.573730 \text{ cm}^3$$

$$1 \text{ U.S. gallon} = 4 \text{ quarts (liq)} = 8 \text{ pints (liq)} = 128 \text{ fl oz} = 3785.4118 \text{ cm}^3$$

$$1 \text{ British Imperial and Canadian gallon} = 1.200949 \text{ U.S. gallons} = 4546.087 \text{ cm}^3$$

$$1 \text{ slug} = 14.59390 \text{ kg}$$

$$1 \text{ pound (lb)} = 4.448444 \text{ nt}$$

$$1 \text{ newton (nt)} = 10^5 \text{ dynes}$$

$$1 \text{ British thermal unit (Btu)} = 1054.35 \text{ joules}$$

$$1 \text{ joule} = 10^7 \text{ ergs}$$

$$1 \text{ calorie (cal)} = 4.1840 \text{ joules}$$

$$1 \text{ kilowatt-hour (kWh)} = 3414.4 \text{ Btu} = 3.6 \cdot 10^6 \text{ joules}$$

$$1 \text{ horsepower (hp)} = 2542.48 \text{ Btu/h} = 178.298 \text{ cal/sec} = 0.74570 \text{ kW}$$

$$1 \text{ kilowatt (kW)} = 1000 \text{ watts} = 3414.43 \text{ Btu/h} = 238.662 \text{ cal/sec}$$

$$^{\circ}\text{F} = ^{\circ}\text{C} \cdot 1.8 + 32$$

$$1^{\circ} = 60' = 3600'' = 0.017453293 \text{ radian}$$

For further details see, for example, D. Halliday, R. Resnick, and J. Walker, *Fundamentals of Physics*. 7th ed., New York: Wiley, 2005. See also AN American National Standard, ASTM/IEEE Standard Metric Practice, Institute of Electrical and Electronics Engineers, Inc., 445 Hoes Lane, Piscataway, N. J. 08854.

## Differentiation

$$(cu)' = cu' \quad (c \text{ constant})$$

$$(u + v)' = u' + v'$$

$$(uv)' = u'v + v'u$$

$$\left(\frac{u}{v}\right)' = \frac{u'v - v'u}{v^2}$$

$$\frac{du}{dx} = \frac{du}{dy} \cdot \frac{dy}{dx} \quad (\text{Chain rule})$$

---

$$(x^n)' = nx^{n-1}$$

$$(e^x)' = e^x$$

$$(a^x)' = a^x \ln a$$

$$(\sin x)' = \cos x$$

$$(\cos x)' = -\sin x$$

$$(\tan x)' = \sec^2 x$$

$$(\cot x)' = -\csc^2 x$$

$$(\sinh x)' = \cosh x$$

$$(\cosh x)' = \sinh x$$

$$(\ln x)' = \frac{1}{x}$$

$$(\log_a x)' = \frac{\log_a e}{x}$$

$$(\arcsin x)' = \frac{1}{\sqrt{1-x^2}}$$

$$(\arccos x)' = -\frac{1}{\sqrt{1-x^2}}$$

$$(\arctan x)' = \frac{1}{1+x^2}$$

$$(\operatorname{arccot} x)' = -\frac{1}{1+x^2}$$

## Integration

$$\int uv' dx = uv - \int u'v dx$$

$$\int x^n dx = \frac{x^{n+1}}{n+1} + c \quad (n \neq -1)$$

$$\int \frac{1}{x} dx = \ln |x| + c$$

$$\int e^{ax} dx = \frac{1}{a} e^{ax} + c$$

$$\int \sin x dx = -\cos x + c$$

$$\int \cos x dx = \sin x + c$$

$$\int \tan x dx = -\ln |\cos x| + c$$

$$\int \cot x dx = \ln |\sin x| + c$$

$$\int \sec x dx = \ln |\sec x + \tan x| + c$$

$$\int \csc x dx = \ln |\csc x - \cot x| + c$$

$$\int \frac{dx}{x^2 + a^2} = \frac{1}{a} \arctan \frac{x}{a} + c$$

$$\int \frac{dx}{\sqrt{a^2 - x^2}} = \arcsin \frac{x}{a} + c$$

$$\int \frac{dx}{\sqrt{x^2 + a^2}} = \operatorname{arsinh} \frac{x}{a} + c$$

$$\int \frac{dx}{\sqrt{x^2 - a^2}} = \operatorname{arccosh} \frac{x}{a} + c$$

$$\int \sin^2 x dx = \frac{1}{2}x - \frac{1}{4}\sin 2x + c$$

$$\int \cos^2 x dx = \frac{1}{2}x + \frac{1}{4}\sin 2x + c$$

$$\int \tan^2 x dx = \tan x - x + c$$

$$\int \cot^2 x dx = -\cot x - x + c$$

$$\int \ln x dx = x \ln x - x + c$$

$$\begin{aligned} \int e^{ax} \sin bx dx \\ = \frac{e^{ax}}{a^2 + b^2} (a \sin bx - b \cos bx) + c \end{aligned}$$

$$\begin{aligned} \int e^{ax} \cos bx dx \\ = \frac{e^{ax}}{a^2 + b^2} (a \cos bx + b \sin bx) + c \end{aligned}$$

9<sup>TH</sup> EDITION

# Advanced Engineering Mathematics

ERWIN KREYSZIG

Professor of Mathematics  
Ohio State University  
Columbus, Ohio



WILEY JOHN WILEY & SONS, INC.

*Vice President and Publisher:* Laurie Rosatone  
*Editorial Assistant:* Daniel Grace  
*Associate Production Director:* Lucille Buonocore  
*Senior Production Editor:* Ken Santor  
*Media Editor:* Stefanie Liebman  
*Cover Designer:* Madelyn Lesure  
*Cover Photo:* © John Sohm/Chromosohm/Photo Researchers

This book was set in Times Roman by GGS Information Services

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Kreyszig, Erwin.

Advanced engineering mathematics / Erwin Kreyszig.—9th ed.

p. cm.

Accompanied by instructor's manual.

Includes bibliographical references and index.

1. Mathematical physics. 2. Engineering mathematics. 1. Title.

ISBN-13: 978-0-471-72897-9

ISBN-10: 0-471-72897-7

Printed in Singapore

10 9 8 7 6 5 4 3 2

See also <http://www.wiley.com/college/kreyszig/>

## Goal of the Book. Arrangement of Material

This new edition continues the tradition of providing instructors and students with a comprehensive and up-to-date resource for teaching and learning *engineering mathematics*, that is, *applied mathematics* for engineers and physicists, mathematicians and computer scientists, as well as members of other disciplines. A course in elementary calculus is the sole *prerequisite*.

The subject matter is arranged into seven parts A–G:

- A Ordinary Differential Equations (ODEs) (Chaps. 1–6)
- B Linear Algebra. Vector Calculus (Chaps. 7–9)
- C Fourier Analysis. Partial Differential Equations (PDEs) (Chaps. 11–12)
- D Complex Analysis (Chaps. 13–18)
- E Numeric Analysis (Chaps. 19–21)
- F Optimization, Graphs (Chaps. 22–23)
- G Probability, Statistics (Chaps. 24–25).

This is followed by five appendices:

- App. 1 References (ordered by parts)
- App. 2 Answers to Odd-Numbered Problems
- App. 3 Auxiliary Material (see also inside covers)
- App. 4 Additional Proofs
- App. 5 Tables of Functions.

This book has helped to pave the way for the present development of engineering mathematics. By a modern approach to those areas A–G, this new edition will prepare the student for the tasks of the present and of the future. The latter can be predicted to some extent by a judicious look at the present trend. Among other features, this trend shows the appearance of more complex production processes, more extreme physical conditions (in space travel, high-speed communication, etc.), and new tasks in robotics and communication systems (e.g., fiber optics and scan statistics on random graphs) and elsewhere. This requires the refinement of existing methods and the creation of new ones.

It follows that students need solid knowledge of basic principles, methods, and results, and a clear view of what engineering mathematics is all about, and that it requires proficiency in all three phases of problem solving:

- **Modeling**, that is, translating a physical or other problem into a mathematical form, into a mathematical *model*; this can be an algebraic equation, a differential equation, a graph, or some other mathematical expression.
- **Solving** the model by selecting and applying a suitable mathematical method, often requiring numeric work on a computer.
- **Interpreting** the mathematical result in physical or other terms to see what it practically means and implies.

It would make no sense to overload students with all kinds of little things that might be of occasional use. Instead they should recognize that mathematics rests on relatively few basic concepts and involves powerful unifying principles. This should give them a firm grasp on the *interrelations among theory, computing, and* (physical or other) *experimentation*.

## PARTS AND CHAPTERS OF THE BOOK

<b>PART A</b>	
Chaps. 1–6 Ordinary Differential Equations (ODEs)	
Chaps. 1–4 Basic Material	
↓ Chap. 5 Series Solutions	↓ Chap. 6 Laplace Transforms

<b>PART B</b>	
Chaps. 7–10 Linear Algebra. Vector Calculus	
Chap. 7 Matrices, Linear Systems	Chap. 9 Vector Differential Calculus
↓ Chap. 8 Eigenvalue Problems	↓ Chap. 10 Vector Integral Calculus

<b>PART C</b>	
Chaps. 11–12 Fourier Analysis. Partial Differential Equations (PDEs)	
Chap. 11 Fourier Analysis	
↓	Chap. 12 Partial Differential Equations

<b>PART D</b>	
Chaps. 13–18 Complex Analysis, Potential Theory	
Chaps. 13–17 Basic Material	
↓	Chap. 18 Potential Theory

<b>PART E</b>		
Chaps. 19–21 Numeric Analysis		
Chap. 19 Numerics in General	Chap. 20 Numeric Linear Algebra	Chap. 21 Numerics for ODEs and PDEs

<b>PART F</b>	
Chaps. 22–23 Optimization, Graphs	
Chap. 22 Linear Programming	Chap. 23 Graphs, Optimization

<b>PART G</b>	
Chaps. 24–25 Probability, Statistics	
Chap. 24 Data Analysis. Probability Theory	
↓	Chap. 25 Mathematical Statistics

<b>GUIDES AND MANUALS</b>	
Maple Computer Guide Mathematica Computer Guide	
Student Solutions Manual	
Instructor's Manual	

## General Features of the Book Include:

- **Simplicity of examples**, to make the book teachable—why choose complicated examples when simple ones are as instructive or even better?
- **Independence of chapters**, to provide *flexibility* in tailoring courses to special needs.
- **Self-contained presentation**, except for a few clearly marked places where a proof would exceed the level of the book and a reference is given instead.
- **Modern standard notation**, to help students with other courses, *modern* books, and mathematical and engineering journals.

Many sections were rewritten in a more detailed fashion, to make it a *simpler book*. This also resulted in a *better balance between theory and applications*.

## Use of Computers

The presentation is *adaptable to various levels of technology and use of a computer or graphing calculator*: very little or no use, medium use, or intensive use of a graphing calculator or of an unspecified *CAS* (Computer Algebra System, *Maple*, *Mathematica*, or *Matlab* being popular examples). In either case texts and problem sets form an entity without gaps or jumps. And many problems can be solved by hand or with a computer or both ways. (For *software*, see the beginnings of *Part E* on Numeric Analysis and *Part G* on Probability and Statistics.)

More specifically, this new edition on the one hand gives more prominence to tasks the computer *cannot* do, notably, modeling and interpreting results. On the other hand, it includes *CAS projects*, *CAS problems*, and *CAS experiments*, which *do require* a computer and show its power in solving problems that are difficult or impossible to access otherwise. Here our goal is the combination of *intelligent* computer use with high-quality mathematics. This has resulted in a change from a formula-centered teaching and learning of engineering mathematics to a more quantitative, project-oriented, and visual approach. *CAS experiments* also exhibit the computer as an instrument for observations and experimentations that may become the beginnings of new research, for “proving” or disproving conjectures, or for formalizing empirical relationships that are often quite useful to the engineer as working guidelines. These changes will also help the student in discovering the *experimental aspect of modern applied mathematics*.

Some *routine and drill work* is retained as a necessity for keeping firm contact with the subject matter. In some of it the computer can (but must not) give the student a hand, but there are plenty of problems that are more suitable for pencil-and-paper work.

## Major Changes

**1. New Problem Sets.** Modern engineering mathematics is mostly *teamwork*. It usually combines analytic work in the process of modeling and the use of computer algebra and numerics in the process of solution, followed by critical evaluation of results. Our problems—some straightforward, some more challenging, some “thinking problems” not accessible by a *CAS*, some open-ended—reflect this modern situation with its increased emphasis on qualitative methods and applications, and the problem sets take care of this novel situation by including team projects, *CAS projects*, and writing projects. The latter will also help the student in writing general reports, as they are required in engineering work quite frequently.

**2. Computer Experiments**, using the computer as an instrument of “*experimental mathematics*” for exploration and research (see also above). These are mostly open-ended



experiments, demonstrating the use of computers in experimentally finding results, which may be provable afterward or may be valuable heuristic qualitative guidelines to the engineer, in particular in complicated problems.

**3. More on modeling and selecting methods**, tasks that usually cannot be automated.

**4. Student Solutions Manual and Study Guide enlarged**, upon explicit requests of the users. This Manual contains worked-out solutions to carefully selected odd-numbered problems (to which App. 1 gives only the final answers) as well as general comments and hints on studying the text and working further problems, including explanations on the significance and character of concepts and methods in the various sections of the book.

## Further Changes, New Features

- Electric circuits moved entirely to Chap. 2, to avoid duplication and repetition
- Second-order ODEs and Higher Order ODEs placed into two separate chapters (2 and 3)
- In Chap. 2, applications presented before variation of parameters
- Series solutions somewhat shortened, without changing the order of sections
- Material on Laplace transforms brought into a better logical order: partial fractions used earlier in a more practical approach, unit step and Dirac's delta put into separate subsequent sections, differentiation and integration of transforms (not of functions!) moved to a later section in favor of practically more important topics
- Second- and third-order determinants made into a separate section for reference throughout the book
- Complex matrices made optional
- Three sections on curves and their application in mechanics combined in a single section
- First two sections on Fourier series combined to provide a better, more direct start
- Discrete and Fast Fourier Transforms included
- Conformal mapping presented in a separate chapter and enlarged
- Numeric analysis updated
- Backward Euler method included
- Stiffness of ODEs and systems discussed
- List of software (in Part E) updated; another list for statistics software added (in Part G)
- References updated, now including about 75 books published or reprinted after 1990

## Suggestions for Courses: A Four-Semester Sequence

The material, when taken in sequence, is suitable for four consecutive semester courses, meeting 3–4 hours a week:

1st Semester.	<i>ODEs</i> (Chaps. 1–5 or 6)
2nd Semester.	<i>Linear Algebra. Vector Analysis</i> (Chaps. 7–10)
3rd Semester.	<i>Complex Analysis</i> (Chaps. 13–18)
4th Semester.	<i>Numeric Methods</i> (Chaps. 19–21)

## Suggestions for Independent One-Semester Courses

The book is also suitable for various independent one-semester courses meeting 3 hours a week. For instance:

- Introduction to ODEs (Chaps. 1–2, Sec. 21.1)
- Laplace Transforms (Chap. 6)
- Matrices and Linear Systems (Chaps. 7–8)
- Vector Algebra and Calculus (Chaps. 9–10)
- Fourier Series and PDEs (Chaps. 11–12, Secs. 21.4–21.7)
- Introduction to Complex Analysis (Chaps. 13–17)
- Numeric Analysis (Chaps. 19, 21)
- Numeric Linear Algebra (Chap. 20)
- Optimization (Chaps. 22–23)
- Graphs and Combinatorial Optimization (Chap. 23)
- Probability and Statistics (Chaps. 24–25)

## Acknowledgments

I am indebted to many of my former teachers, colleagues, and students who helped me directly or indirectly in preparing this book, in particular, the present edition. I profited greatly from discussions with engineers, physicists, mathematicians, and computer scientists, and from their written comments. I want to mention particularly Y. Antipov, D. N. Buechler, S. L. Campbell, R. Carr, P. L. Chambre, V. F. Connolly, Z. Davis, J. Delany, J. W. Dettman, D. Dicker, L. D. Drager, D. Ellis, W. Fox, A. Goriely, R. B. Guenther, J. B. Handley, N. Harbertson, A. Hassen, V. W. Howe, H. Kuhn, G. Lamb, M. T. Lusk, H. B. Mann, I. Marx, K. Millet, J. D. Moore, W. D. Munroe, A. Nadim, B. S. Ng, J. N. Ong, Jr., D. Panagiotis, A. Plotkin, P. J. Pritchard, W. O. Ray, J. T. Scheick, L. F. Shampine, H. A. Smith, J. Todd, H. Unz, A. L. Villone, H. J. Weiss, A. Wilansky, C. H. Wilcox, H. Ya Fan, and A. D. Ziebur, all from the United States, Professors E. J. Norminton and R. Vaillancourt from Canada, and Professors H. Florian and H. Unger from Europe. I can offer here only an inadequate acknowledgment of my gratitude and appreciation.

Special cordial thanks go to Privatdozent Dr. M. Kracht and to Mr. Herbert Kreyszig, MBA, the coauthor of the Student Solutions Manual, who both checked the manuscript in all details and made numerous suggestions for improvements and helped me proofread the galley and page proofs.

Furthermore, I wish to thank John Wiley and Sons (see the list on p. iv) as well as GGS Information Services, in particular Mr. K. Bradley and Mr. J. Nystrom, for their effective cooperation and great care in preparing this new edition.

*Suggestions of many readers worldwide were evaluated in preparing this edition. Further comments and suggestions for improving the book will be gratefully received.*

ERWIN KREYSZIG

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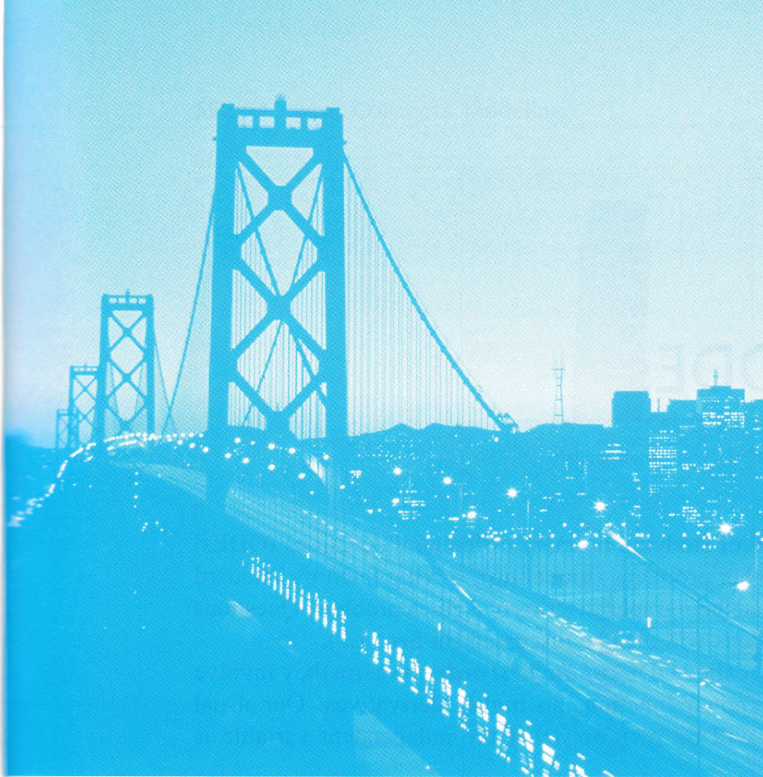
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# PART A

## Ordinary Differential Equations (ODEs)

- CHAPTER 1 **First-Order ODEs**
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- CHAPTER 4 **Systems of ODEs. Phase Plane. Qualitative Methods**
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**Differential equations** are of basic importance in engineering mathematics because many physical laws and relations appear mathematically in the form of a differential equation. In Part A we shall consider various physical and geometric problems that lead to differential equations, with emphasis on *modeling*, that is, the transition from the physical situation to a “mathematical model.” In this chapter the model will be a differential equation, and as we proceed we shall explain the most important standard methods for solving such equations.

Part A concerns *ordinary differential equations (ODEs)*, whose unknown functions depend on a *single* variable. *Partial* differential equations (PDEs), involving unknown functions of *several* variables, follow in Part C.

ODEs are very well suited for computers. *Numeric methods for ODEs can be studied directly after Chaps. 1 or 2.* See Secs. 21.1–21.3, which are independent of the other sections on numerics.



# CHAPTER 1

## First-Order ODEs

In this chapter we begin our program of studying ordinary differential equations (ODEs) by deriving them from physical or other problems (**modeling**), solving them by standard methods, and interpreting solutions and their graphs in terms of a given problem. Questions of existence and uniqueness of solutions will also be discussed (in Sec. 1.7).

We begin with the simplest ODEs, called ODEs *of the first order* because they involve only the first derivative of the unknown function, no higher derivatives. Our usual notation for the unknown function will be  $y(x)$ , or  $y(t)$  if the independent variable is time  $t$ .

If you wish, use your computer algebra system (CAS) for checking solutions, but make sure that you gain a conceptual understanding of the basic terms, such as ODE, direction field, and initial value problem.

**COMMENT.** *Numerics for first-order ODEs can be studied immediately after this chapter.* See Secs. 21.1–21.2, which are independent of other sections on numerics.

*Prerequisite:* Integral calculus.

*Sections that may be omitted in a shorter course:* 1.6, 1.7.

*References and Answers to Problems:* App. 1 Part A, and App. 2

### 1.1 Basic Concepts. Modeling

If we want to solve an engineering problem (usually of a physical nature), we first have to formulate the problem as a mathematical expression in terms of variables, functions, equations, and so forth. Such an expression is known as a mathematical **model** of the given problem. The process of setting up a model, solving it mathematically, and interpreting the result in physical or other terms is called *mathematical modeling* or, briefly, **modeling**. We shall illustrate this process by various examples and problems because modeling requires experience. (Your computer may help you in solving but hardly in setting up models.)

Since many physical concepts, such as velocity and acceleration, are derivatives, a model is very often an equation containing derivatives of an unknown function. Such a model is called a **differential equation**. Of course, we then want to find a solution (a function that satisfies the equation), explore its properties, graph it, find values of it, and interpret it in physical terms so that we can understand the behavior of the physical system in our given problem. However, before we can turn to methods of solution we must first define basic concepts needed throughout this chapter.

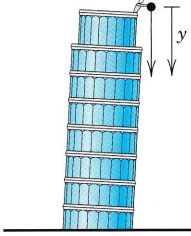
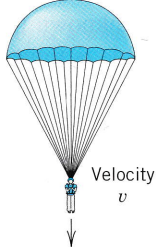
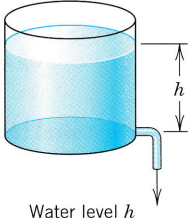
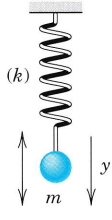
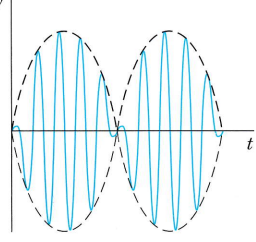
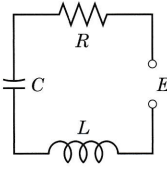
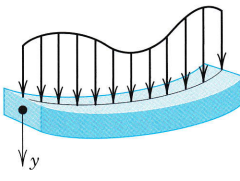
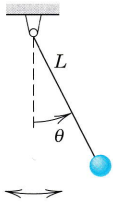
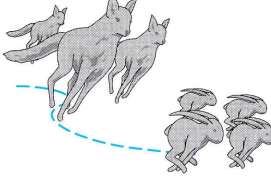
 <p>Falling stone</p> $y'' = g = \text{const.}$ <p>(Sec. 1.1)</p>	 <p>Parachutist</p> $mv' = mg - bv^2$ <p>(Sec. 1.2)</p>	 <p>Water level <math>h</math></p> $h' = -k\sqrt{h}$ <p>(Sec. 1.3)</p>
 <p>Displacement <math>y</math></p> <p>Vibrating mass on a spring</p> $my'' + ky = 0$ <p>(Secs. 2.4, 2.8)</p>	 <p>Beats of a vibrating system</p> $y'' + \omega_0^2 y = \cos \omega t, \quad \omega_0 \approx \omega$ <p>(Sec. 2.8)</p>	 <p>Current <math>I</math> in an <math>RLC</math> circuit</p> $LI'' + RI' + \frac{1}{C}I = E'$ <p>(Sec. 2.9)</p>
 <p>Deformation of a beam</p> $EIy^{iv} = f(x)$ <p>(Sec. 3.3)</p>	 <p>Pendulum</p> $L\theta'' + g \sin \theta = 0$ <p>(Sec. 4.5)</p>	 <p>Lotka–Volterra predator–prey model</p> $y_1' = \alpha y_1 - b y_1 y_2$ $y_2' = k y_1 y_2 - l y_2$ <p>(Sec. 4.5)</p>

Fig. 1. Some applications of differential equations

An **ordinary differential equation (ODE)** is an equation that contains one or several derivatives of an unknown function, which we usually call  $y(x)$  (or sometimes  $y(t)$  if the independent variable is time  $t$ ). The equation may also contain  $y$  itself, known functions of  $x$  (or  $t$ ), and constants. For example,

$$\begin{aligned} (1) \quad & y' = \cos x, \\ (2) \quad & y'' + 9y = 0, \\ (3) \quad & x^2 y''' y' + 2e^x y'' = (x^2 + 2)y^2 \end{aligned}$$

are ordinary differential equations (ODEs). The term *ordinary* distinguishes them from *partial differential equations* (PDEs), which involve partial derivatives of an unknown function of *two or more* variables. For instance, a PDE with unknown function  $u$  of two variables  $x$  and  $y$  is

$$\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} = 0.$$

PDEs are more complicated than ODEs; they will be considered in Chap. 12.

An ODE is said to be of **order**  $n$  if the  $n$ th derivative of the unknown function  $y$  is the highest derivative of  $y$  in the equation. The concept of order gives a useful classification into ODEs of first order, second order, and so on. Thus, (1) is of first order, (2) of second order, and (3) of third order.

In this chapter we shall consider **first-order ODEs**. Such equations contain only the first derivative  $y'$  and may contain  $y$  and any given functions of  $x$ . Hence we can write them as

$$(4) \quad F(x, y, y') = 0$$

or often in the form

$$y' = f(x, y).$$

This is called the *explicit form*, in contrast with the *implicit form* (4). For instance, the implicit ODE  $x^{-3}y' - 4y^2 = 0$  (where  $x \neq 0$ ) can be written explicitly as  $y' = 4x^3y^2$ .

## Concept of Solution

A function

$$y = h(x)$$

is called a **solution** of a given ODE (4) on some open interval  $a < x < b$  if  $h(x)$  is defined and differentiable throughout the interval and is such that the equation becomes an identity if  $y$  and  $y'$  are replaced with  $h$  and  $h'$ , respectively. The curve (the graph) of  $h$  is called a **solution curve**.

Here, **open interval**  $a < x < b$  means that the endpoints  $a$  and  $b$  are not regarded as points belonging to the interval. Also,  $a < x < b$  includes *infinite intervals*  $-\infty < x < b$ ,  $a < x < \infty$ ,  $-\infty < x < \infty$  (the real line) as special cases.

**EXAMPLE 1** Verification of Solution

$y = h(x) = c/x$  ( $c$  an arbitrary constant,  $x \neq 0$ ) is a solution of  $xy' = -y$ . To verify this, differentiate,  $y' = h'(x) = -c/x^2$ , and multiply by  $x$  to get  $xy' = -c/x = -y$ . Thus,  $xy' = -y$ , the given ODE. ■

**EXAMPLE 2** Solution Curves

The ODE  $y' = dy/dx = \cos x$  can be solved directly by integration on both sides. Indeed, using calculus, we obtain  $y = \int \cos x \, dx = \sin x + c$ , where  $c$  is an arbitrary constant. This is a **family of solutions**. Each value of  $c$ , for instance, 2.75 or 0 or  $-8$ , gives one of these curves. Figure 2 shows some of them, for  $c = -3, -2, -1, 0, 1, 2, 3, 4$ . ■

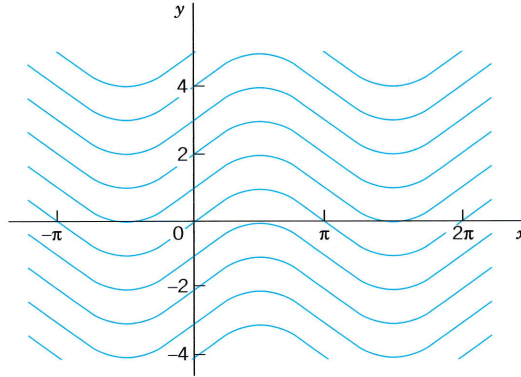


Fig. 2. Solutions  $y = \sin x + c$  of the ODE  $y' = \cos x$

**EXAMPLE 3** Exponential Growth, Exponential Decay

From calculus we know that  $y = ce^{3t}$  ( $c$  any constant) has the derivative (chain rule!)

$$y' = \frac{dy}{dt} = 3ce^{3t} = 3y.$$

This shows that  $y$  is a solution of  $y' = 3y$ . Hence this ODE can model **exponential growth**, for instance, of animal populations or colonies of bacteria. It also applies to humans for small populations in a large country (e.g., the United States in early times) and is then known as **Malthus's law**.<sup>1</sup> We shall say more about this topic in Sec. 1.5.

Similarly,  $y' = -0.2y$  (with a minus on the right!) has the solution  $y = ce^{-0.2t}$ . Hence this ODE models **exponential decay**, for instance, of a radioactive substance (see Example 5). Figure 3 shows solutions for some positive  $c$ . Can you find what the solutions look like for negative  $c$ ? ■

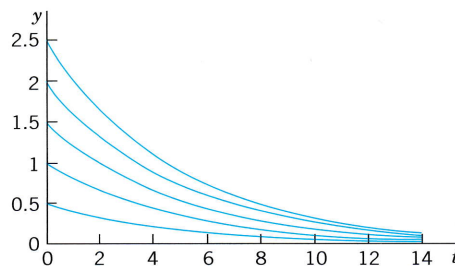


Fig. 3. Solutions of  $y' = -0.2y$  in Example 3

<sup>1</sup>Named after the English pioneer in classic economics, THOMAS ROBERT MALTHUS (1766–1834).

We see that each ODE in these examples has a solution that contains an arbitrary constant  $c$ . Such a solution containing an arbitrary constant  $c$  is called a **general solution** of the ODE.

(We shall see that  $c$  is sometimes not completely arbitrary but must be restricted to some interval to avoid complex expressions in the solution.)

We shall develop methods that will give general solutions *uniquely* (perhaps except for notation). Hence we shall say *the* general solution of a given ODE (instead of *a* general solution).

Geometrically, the general solution of an ODE is a family of infinitely many solution curves, one for each value of the constant  $c$ . If we choose a specific  $c$  (e.g.,  $c = 6.45$  or  $0$  or  $-2.01$ ) we obtain what is called a **particular solution** of the ODE. A particular solution does not contain any arbitrary constants.

In most cases, general solutions exist, and every solution not containing an arbitrary constant is obtained as a particular solution by assigning a suitable value to  $c$ . Exceptions to these rules occur but are of minor interest in applications; see Prob. 16 in Problem Set 1.1.

## Initial Value Problem

In most cases the unique solution of a given problem, hence a particular solution, is obtained from a general solution by an **initial condition**  $y(x_0) = y_0$ , with given values  $x_0$  and  $y_0$ , that is used to determine a value of the arbitrary constant  $c$ . Geometrically this condition means that the solution curve should pass through the point  $(x_0, y_0)$  in the  $xy$ -plane. An ODE together with an initial condition is called an **initial value problem**. Thus, if the ODE is explicit,  $y' = f(x, y)$ , the initial value problem is of the form

$$(5) \quad y' = f(x, y), \quad y(x_0) = y_0.$$

### EXAMPLE 4 Initial Value Problem

Solve the initial value problem

$$y' = \frac{dy}{dx} = 3y, \quad y(0) = 5.7.$$

**Solution.** The general solution is  $y(x) = ce^{3x}$ ; see Example 3. From this solution and the initial condition we obtain  $y(0) = ce^0 = c = 5.7$ . Hence the initial value problem has the solution  $y(x) = 5.7e^{3x}$ . This is a particular solution. ■

## Modeling

The general importance of modeling to the engineer and physicist was emphasized at the beginning of this section. We shall now consider a basic physical problem that will show the typical steps of modeling in detail: Step 1 the transition from the physical situation (the physical system) to its mathematical formulation (its mathematical model); Step 2 the solution by a mathematical method; and Step 3 the physical interpretation of the result. This may be the easiest way to obtain a first idea of the nature and purpose of differential equations and their applications. Realize at the outset that your **computer** (your **CAS**) may perhaps give you a hand in Step 2, but Steps 1 and 3 are basically your work. And Step 2

requires a solid knowledge and good understanding of solution methods available to you—you have to choose the method for your work by hand or by the computer. Keep this in mind, and always check computer results for errors (which may result, for instance, from false inputs).

### EXAMPLE 5 Radioactivity. Exponential Decay

Given an amount of a radioactive substance, say, 0.5 g (gram), find the amount present at any later time.

*Physical Information.* Experiments show that at each instant a radioactive substance decomposes at a rate proportional to the amount present.

**Step 1. Setting up a mathematical model (a differential equation) of the physical process.** Denote by  $y(t)$  the amount of substance still present at any time  $t$ . By the physical law, the time rate of change  $y'(t) = dy/dt$  is proportional to  $y(t)$ . Denote the constant of proportionality by  $k$ . Then

$$(6) \quad \frac{dy}{dt} = ky.$$

The value of  $k$  is known from experiments for various radioactive substances (e.g.,  $k = -1.4 \cdot 10^{-11} \text{sec}^{-1}$ , approximately, for radium  ${}_{88}\text{Ra}^{226}$ ).  $k$  is *negative* because  $y(t)$  decreases with time. The given initial amount is 0.5 g. Denote the corresponding time by  $t = 0$ . Then the initial condition is  $y(0) = 0.5$ . This is the instant at which the process begins; this motivates the term *initial condition* (which, however, is also used more generally when the independent variable is not time or when you choose a  $t$  other than  $t = 0$ ). Hence the model of the process is the **initial value problem**

$$(7) \quad \frac{dy}{dt} = ky, \quad y(0) = 0.5.$$

**Step 2. Mathematical solution.** As in Example 3 we conclude that the ODE (6) models exponential decay and has the general solution (with arbitrary constant  $c$  but definite given  $k$ )

$$(8) \quad y(t) = ce^{kt}.$$

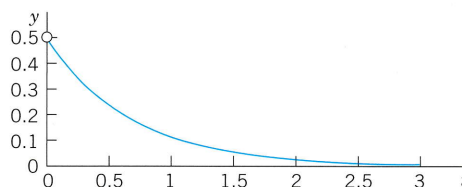
We now use the initial condition to determine  $c$ . Since  $y(0) = c$  from (8), this gives  $y(0) = c = 0.5$ . Hence the particular solution governing this process is

$$(9) \quad y(t) = 0.5e^{kt} \quad (\text{Fig. 4}).$$

**Always check your result**—it may involve human or computer errors! Verify by differentiation (chain rule!) that your solution (9) satisfies (7) as well as  $y(0) = 0.5$ :

$$\frac{dy}{dt} = 0.5ke^{kt} = k \cdot 0.5e^{kt} = ky, \quad y(0) = 0.5e^0 = 0.5.$$

**Step 3. Interpretation of result.** Formula (9) gives the amount of radioactive substance at time  $t$ . It starts from the correct given initial amount and decreases with time because  $k$  (the constant of proportionality, depending on the kind of substance) is negative. The limit of  $y$  as  $t \rightarrow \infty$  is zero. ■



**Fig. 4.** Radioactivity (Exponential decay,  $y = 0.5e^{kt}$ , with  $k = -1.5$  as an example)



**EXAMPLE 6 A Geometric Application**

Geometric problems may also lead to initial value problems. For instance, find the curve through the point  $(1, 1)$  in the  $xy$ -plane having at each of its points the slope  $-y/x$ .

**Solution.** The slope  $y'$  should equal  $-y/x$ . This gives the ODE  $y' = -y/x$ . Its general solution is  $y = c/x$  (see Example 1). This is a family of hyperbolas with the coordinate axes as asymptotes.

Now, for the curve to pass through  $(1, 1)$ , we must have  $y = 1$  when  $x = 1$ . Hence the initial condition is  $y(1) = 1$ . From this condition and  $y = c/x$  we get  $y(1) = c/1 = 1$ ; that is,  $c = 1$ . This gives the particular solution  $y = 1/x$  (drawn somewhat thicker in Fig. 5). ■

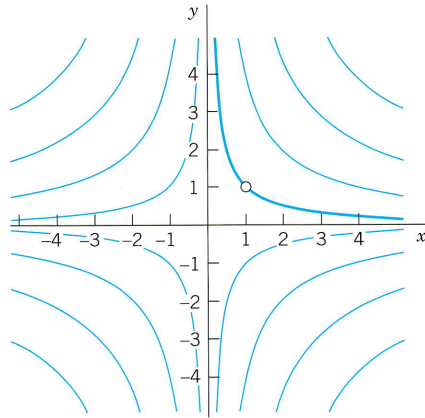


Fig. 5. Solutions of  $y' = -y/x$  (hyperbolas)

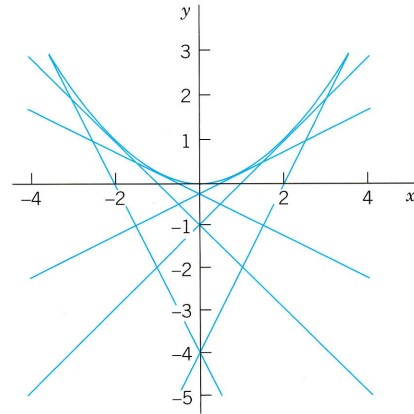


Fig. 6. Particular solutions and singular solution in Problem 16

**PROBLEM SET 1.1****1-4 CALCULUS**

Solve the ODE by integration.

1.  $y' = -\sin \pi x$
2.  $y' = e^{-3x}$
3.  $y' = xe^{x^2/2}$
4.  $y' = \cosh 4x$

**5-9 VERIFICATION OF SOLUTION**

State the order of the ODE. Verify that the given function is a solution. ( $a, b, c$  are arbitrary constants.)

5.  $y' = 1 + y^2$ ,  $y = \tan(x + c)$
6.  $y'' + \pi^2 y = 0$ ,  $y = a \cos \pi x + b \sin \pi x$
7.  $y'' + 2y' + 10y = 0$ ,  $y = 4e^{-x} \sin 3x$
8.  $y' + 2y = 4(x + 1)^2$ ,  $y = 5e^{-2x} + 2x^2 + 2x + 1$
9.  $y''' = \cos x$ ,  $y = -\sin x + ax^2 + bx + c$

**10-14 INITIAL VALUE PROBLEMS**

Verify that  $y$  is a solution of the ODE. Determine from  $y$  the particular solution satisfying the given initial condition. Sketch or graph this solution.

10.  $y' = 0.5y$ ,  $y = ce^{0.5x}$ ,  $y(2) = 2$
11.  $y' = 1 + 4y^2$ ,  $y = \frac{1}{2} \tan(2x + c)$ ,  $y(0) = 0$
12.  $y' = y - x$ ,  $y = ce^x + x + 1$ ,  $y(0) = 3$
13.  $y' + 2xy = 0$ ,  $y = ce^{-x^2}$ ,  $y(1) = 1/e$
14.  $y' = y \tan x$ ,  $y = c \sec x$ ,  $y(0) = \frac{1}{2}\pi$

15. (Existence) (A) Does the ODE  $y'^2 = -1$  have a (real) solution?

(B) Does the ODE  $|y'| + |y| = 0$  have a general solution?

16. (Singular solution) An ODE may sometimes have an additional solution that cannot be obtained from the general solution and is then called a *singular solution*. The ODE  $y'^2 - xy' + y = 0$  is of the kind. Show by differentiation and substitution that it has the general solution  $y = cx - c^2$  and the singular solution  $y = x^2/4$ . Explain Fig. 6.

**17-22 MODELING, APPLICATIONS**

The following problems will give you a first impression of modeling. Many more problems on modeling follow throughout this chapter.

17. (Falling body) If we drop a stone, we can assume air resistance ("drag") to be negligible. Experiments show that under that assumption the acceleration  $y'' = d^2y/dt^2$  of this motion is constant (equal to the so-called acceleration of gravity  $g = 9.80 \text{ m/sec}^2 = 32 \text{ ft/sec}^2$ ). State this as an ODE for  $y(t)$ , the distance fallen as a function of time  $t$ . Solve the ODE to get the familiar law of free fall,  $y = gt^2/2$ .

18. **(Falling body)** If in Prob. 17 the stone starts at  $t = 0$  from initial position  $y_0$  with initial velocity  $v = v_0$ , show that the solution is  $y = gt^2/2 + v_0t + y_0$ . How long does a fall of 100 m take if the body falls from rest? A fall of 200 m? (Guess first.)
19. **(Airplane takeoff)** If an airplane has a run of 3 km, starts with a speed 6 m/sec, moves with constant acceleration, and makes the run in 1 min, with what speed does it take off?
20. **(Subsonic flight)** The efficiency of the engines of subsonic airplanes depends on air pressure and usually is maximum near about 36 000 ft. Find the air pressure  $y(x)$  at this height without calculation. *Physical information.* The rate of change  $y'(x)$  is proportional to the pressure, and at 18 000 ft the pressure has decreased to half its value  $y_0$  at sea level.
21. **(Half-life)** The half-life of a radioactive substance is the time in which half of the given amount disappears. Hence it measures the rapidity of the decay. What is the half-life of radium  ${}_{88}\text{Ra}^{226}$  (in years) in Example 5?
22. **(Interest rates)** Show by algebra that the investment  $y(t)$  from a deposit  $y_0$  after  $t$  years at an interest rate  $r$  is
- $$y_a(t) = y_0[1 + r]^t \quad (\text{Interest compounded annually})$$
- $$y_d(t) = y_0[1 + (r/365)]^{365t} \quad (\text{Interest compounded daily}).$$
- Recall from calculus that
- $$[1 + (1/n)]^n \rightarrow e \text{ as } n \rightarrow \infty;$$
- hence  $[1 + (r/n)]^{nt} \rightarrow e^{rt}$ ; thus
- $$y_c(t) = y_0e^{rt} \quad (\text{Interest compounded continuously}).$$
- What ODE does the last function satisfy? Let the initial investment be \$1000 and  $r = 6\%$ . Compute the value of the investment after 1 year and after 5 years using each of the three formulas. Is there much difference?

## 1.2 Geometric Meaning of $y' = f(x, y)$ . Direction Fields

A first-order ODE

$$(1) \quad y' = f(x, y)$$

has a simple geometric interpretation. From calculus you know that the derivative  $y'(x)$  of  $y(x)$  is the slope of  $y(x)$ . Hence a solution curve of (1) that passes through a point  $(x_0, y_0)$  must have at that point the slope  $y'(x_0)$  equal to the value of  $f$  at that point; that is,

$$y'(x_0) = f(x_0, y_0).$$

Read this paragraph again before you go on, and think about it.

It follows that you can indicate directions of solution curves of (1) by drawing short straight-line segments (*lineal elements*) in the  $xy$ -plane (as in Fig. 7a) and then fitting (approximate) solution curves through the direction field (or *slope field*) thus obtained. This method is important for two reasons.

1. You need not solve (1). This is essential because many ODEs have complicated solution formulas or none at all.
2. The method shows, in graphical form, the whole family of solutions and their typical properties. The accuracy is somewhat limited, but in most cases this does not matter.

Let us illustrate this method for the ODE

$$(2) \quad y' = xy.$$

**Direction Fields by a CAS (Computer Algebra System).** A CAS plots lineal elements at the points of a square grid, as in Fig. 7a for (2), into which you can fit solution curves. Decrease the mesh size of the grid in regions where  $f(x, y)$  varies rapidly.

**Direction Fields by Using Isoclines (the Older Method).** Graph the curves  $f(x, y) = k = \text{const}$ , called *isoclines* (meaning *curves of equal inclination*). For (2) these are the hyperbolas  $f(x, y) = xy = k = \text{const}$  (and the coordinate axes) in Fig. 7b. By (1), these are the curves along which the derivative  $y'$  is constant. These are not yet solution curves—don't get confused. Along each isocline draw many parallel line elements of the corresponding slope  $k$ . This gives the direction field, into which you can now graph approximate solution curves.

We mention that for the ODE (2) in Fig. 7 we would not need the method, because we shall see in the next section that ODEs such as (2) can easily be solved exactly. For the time being, let us verify by substitution that (2) has the general solution

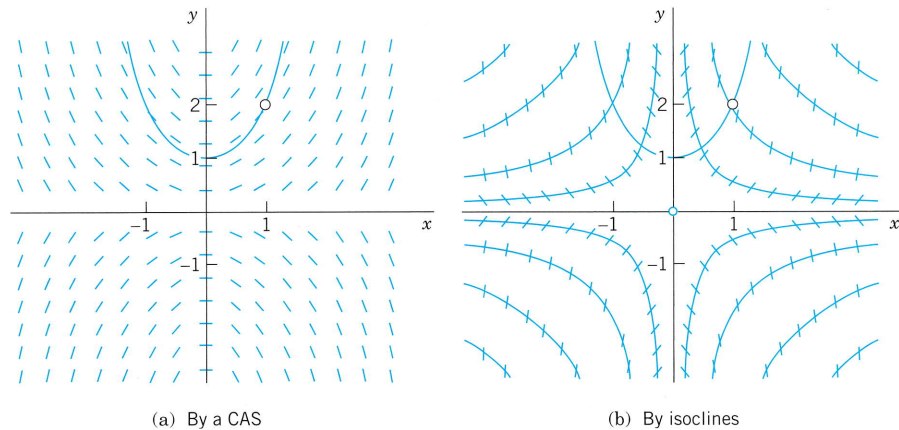
$$y(x) = ce^{x^2/2} \quad (c \text{ arbitrary}).$$

Indeed, by differentiation (chain rule!) we get  $y' = x(ce^{x^2/2}) = xy$ . Of course, knowing the solution, we now have the advantage of obtaining a feel for the accuracy of the method by comparing with the exact solution. The particular solution in Fig. 7 through  $(x, y) = (1, 2)$  must satisfy  $y(1) = 2$ . Thus,  $2 = ce^{1/2}$ ,  $c = 2/\sqrt{e} = 1.213$ , and the particular solution is  $y(x) = 1.213e^{x^2/2}$ .

A famous ODE for which we *do* need direction fields is

$$(3) \quad y' = 0.1(1 - x^2) - \frac{x}{y}.$$

(It is related to the van der Pol equation of electronics, which we shall discuss in Sec. 4.5.) The direction field in Fig. 8 shows lineal elements generated by the computer. We have also added the isoclines for  $k = -5, -3, \frac{1}{4}, 1$  as well as three typical solution curves, one that is (almost) a circle and two spirals approaching it from inside and outside.



**Fig. 7.** Direction field of  $y' = xy$

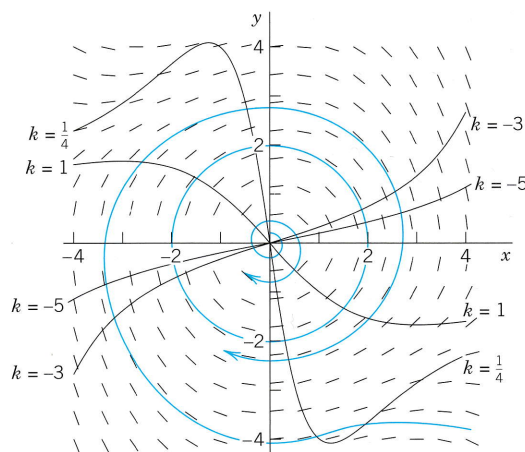


Fig. 8. Direction field of  $y' = 0.1(1 - x^2) - \frac{x}{y}$

## On Numerics

Direction fields give “all” solutions, but with limited accuracy. If we need accurate numeric values of a solution (or of several solutions) for which we have no formula, we can use a **numeric method**. If you want to get an idea of how these methods work, go to Sec. 21.1 and study the first two pages on the **Euler–Cauchy method**, which is typical of more accurate methods later in that section, notably of the classical **Runge–Kutta method**. It would make little sense to interrupt the present flow of ideas by including such methods here; indeed, it would be a duplication of the material in Sec. 21.1. For an excursion to that section you need no extra prerequisites; Sec. 1.1 just discussed is sufficient.

## PROBLEM SET 1.2

### 1–10 DIRECTION FIELDS, SOLUTION CURVES

Graph a direction field (by a CAS or by hand). In the field graph approximate solution curves through the given point or points  $(x, y)$  by hand.

1.  $y' = e^x - y$ ,  $(0, 0)$ ,  $(0, 1)$
2.  $4yy' = -9x$ ,  $(2, 2)$
3.  $y' = 1 + y^2$ ,  $(\frac{1}{4}\pi, 1)$
4.  $y' = y - 2y^2$ ,  $(0, 0)$ ,  $(0, 0.25)$ ,  $(0, 0.5)$ ,  $(0, 1)$
5.  $y' = x^2 - 1/y$ ,  $(1, -2)$
6.  $y' = 1 + \sin y$ ,  $(-1, 0)$ ,  $(1, -4)$
7.  $y' = y^3 + x^3$ ,  $(0, 1)$
8.  $y' = 2xy + 1$ ,  $(-1, 2)$ ,  $(0, 0)$ ,  $(1, -2)$
9.  $y' = y \tanh x - 2$ ,  $(-1, -2)$ ,  $(1, 0)$ ,  $(1, 2)$
10.  $y' = e^{y/x}$ ,  $(1, 1)$ ,  $(2, 2)$ ,  $(3, 3)$

### 11–15 ACCURACY

Direction fields are very useful because you can see solutions (as many as you want) without solving the ODE, which may be difficult or impossible in terms of a formula. To get a feel for the accuracy of the method, graph a field, sketch solution curves in it, and compare them with the exact solutions.

11.  $y' = \sin \frac{1}{2}\pi x$
12.  $y' = 1/x^2$
13.  $y' = -2y$  (Sol.  $y = ce^{-2x}$ )
14.  $y' = 3y/x$  (Sol.  $y = cx^3$ )
15.  $y' = -\ln x$

### 16–18 MOTIONS

A body moves on a straight line, with velocity as given, and  $y(t)$  is its distance from a fixed point 0 and  $t$  time. Find a model of the motion (an ODE). Graph a direction field.

In it sketch a solution curve corresponding to the given initial condition.

16. Velocity equal to the reciprocal of the distance,  $y(1) = 1$   
 17. Product of velocity and distance equal to  $-t$ ,  $y(3) = -3$   
 18. Velocity plus distance equal to the square of time,  $y(0) = 6$   
 19. (**Skydiver**) Two forces act on a parachutist, the attraction by the earth  $mg$  ( $m$  = mass of person plus equipment,  $g = 9.8$  m/sec<sup>2</sup> the acceleration of gravity) and the air resistance, assumed to be proportional to the square of the velocity  $v(t)$ . Using **Newton's second law** of motion (mass  $\times$  acceleration = resultant of the forces), set up a model (an ODE for  $v(t)$ ). Graph a direction field (choosing  $m$  and the constant of proportionality equal to 1). Assume that the parachute opens when  $v = 10$  m/sec. Graph the corresponding solution in the field. What is the limiting velocity?

20. **CAS PROJECT. Direction Fields.** Discuss direction fields as follows.

- (a) Graph a direction field for the ODE  $y' = 1 - y$  and in it the solution satisfying  $y(0) = 5$  showing **exponential approach**. Can you see the limit of any solution directly from the ODE? For what initial condition will the solution be increasing? Constant? Decreasing?
- (b) What do the solution curves of  $y' = -x^3/y^3$  look like, as concluded from a direction field. How do they seem to differ from circles? What are the isoclines? What happens to those curves when you drop the minus on the right? Do they look similar to familiar curves? First, guess.
- (c) Compare, as best as you can, the old and the computer methods, their advantages and disadvantages. Write a short report.

## 1.3 Separable ODEs. Modeling

Many practically useful ODEs can be reduced to the form

$$(1) \quad g(y)y' = f(x)$$

by purely algebraic manipulations. Then we can integrate on both sides with respect to  $x$ , obtaining

$$(2) \quad \int g(y) y' dx = \int f(x) dx + c.$$

On the left we can switch to  $y$  as the variable of integration. By calculus,  $y' dx = dy$ , so that

$$(3) \quad \int g(y) dy = \int f(x) dx + c.$$

If  $f$  and  $g$  are continuous functions, the integrals in (3) exist, and by evaluating them we obtain a general solution of (1). This method of solving ODEs is called the **method of separating variables**, and (1) is called a **separable equation**, because in (3) the variables are now separated:  $x$  appears only on the right and  $y$  only on the left.

### EXAMPLE 1 A Separable ODE

The ODE  $y' = 1 + y^2$  is separable because it can be written

$$\frac{dy}{1 + y^2} = dx. \quad \text{By integration,} \quad \arctan y = x + c \quad \text{or} \quad y = \tan(x + c).$$

*It is very important to introduce the constant of integration immediately when the integration is performed.* If we wrote  $\arctan y = x$ , then  $y = \tan x$ , and then introduced  $c$ , we would have obtained  $y = \tan x + c$ , which is not a solution (when  $c \neq 0$ ). Verify this. ■

## Modeling

The importance of modeling was emphasized in Sec. 1.1, and separable equations yield various useful models. Let us discuss this in terms of some typical examples.

### EXAMPLE 2 Radiocarbon Dating<sup>2</sup>

In September 1991 the famous Iceman (Oetzi), a mummy from the Neolithic period of the Stone Age found in the ice of the Oetztal Alps (hence the name “Oetzi”) in Southern Tyrolia near the Austrian–Italian border, caused a scientific sensation. When did Oetzi approximately live and die if the ratio of carbon  ${}^6\text{C}^{14}$  to carbon  ${}^6\text{C}^{12}$  in this mummy is 52.5% of that of a living organism?

*Physical Information.* In the atmosphere and in living organisms, the ratio of radioactive carbon  ${}^6\text{C}^{14}$  (made radioactive by cosmic rays) to ordinary carbon  ${}^6\text{C}^{12}$  is constant. When an organism dies, its absorption of  ${}^6\text{C}^{14}$  by breathing and eating terminates. Hence one can estimate the age of a fossil by comparing the radioactive carbon ratio in the fossil with that in the atmosphere. To do this, one needs to know the half-life of  ${}^6\text{C}^{14}$ , which is 5715 years (*CRC Handbook of Chemistry and Physics*, 83rd ed., Boca Raton: CRC Press, 2002, page 11–52, line 9).

**Solution.** *Modeling.* Radioactive decay is governed by the ODE  $y' = ky$  (see Sec. 1.1, Example 5). By separation and integration (where  $t$  is time and  $y_0$  is the initial ratio of  ${}^6\text{C}^{14}$  to  ${}^6\text{C}^{12}$ )

$$\frac{dy}{y} = k dt, \quad \ln |y| = kt + c, \quad y = y_0 e^{kt}.$$

Next we use the half-life  $H = 5715$  to determine  $k$ . When  $t = H$ , half of the original substance is still present. Thus,

$$y_0 e^{kH} = 0.5y_0, \quad e^{kH} = 0.5, \quad k = \frac{\ln 0.5}{H} = -\frac{0.693}{5715} = -0.0001213.$$

Finally, we use the ratio 52.5% for determining the time  $t$  when Oetzi died (actually, was killed),

$$e^{kt} = e^{-0.0001213t} = 0.525, \quad t = \frac{\ln 0.525}{-0.0001213} = 5312. \quad \text{Answer:} \quad \text{About 5300 years ago.}$$

Other methods show that radiocarbon dating values are usually too small. According to recent research, this is due to a variation in that carbon ratio because of industrial pollution and other factors, such as nuclear testing. ■

### EXAMPLE 3 Mixing Problem

Mixing problems occur quite frequently in chemical industry. We explain here how to solve the basic model involving a single tank. The tank in Fig. 9 contains 1000 gal of water in which initially 100 lb of salt is dissolved. Brine runs in at a rate of 10 gal/min, and each gallon contains 5 lb of dissolved salt. The mixture in the tank is kept uniform by stirring. Brine runs out at 10 gal/min. Find the amount of salt in the tank at any time  $t$ .

**Solution.** *Step 1. Setting up a model.* Let  $y(t)$  denote the amount of salt in the tank at time  $t$ . Its time rate of change is

$$y' = \text{Salt inflow rate} - \text{Salt outflow rate} \quad \text{“Balance law”}.$$

5 lb times 10 gal gives an inflow of 50 lb of salt. Now, the outflow is 10 gal of brine. This is  $10/1000 = 0.01$  (= 1%) of the total brine content in the tank, hence 0.01 of the salt content  $y(t)$ , that is,  $0.01y(t)$ . Thus the model is the ODE

$$(4) \quad y' = 50 - 0.01y = -0.01(y - 5000).$$

<sup>2</sup>Method by WILLARD FRANK LIBBY (1908–1980), American chemist, who was awarded for this work the 1960 Nobel Prize in chemistry.

**Step 2. Solution of the model.** The ODE (4) is separable. Separation, integration, and taking exponents on both sides gives

$$\frac{dy}{y - 5000} = -0.01 dt, \quad \ln |y - 5000| = -0.01t + c^*, \quad y - 5000 = ce^{-0.01t}.$$

Initially the tank contains 100 lb of salt. Hence  $y(0) = 100$  is the initial condition that will give the unique solution. Substituting  $y = 100$  and  $t = 0$  in the last equation gives  $100 - 5000 = ce^0 = c$ . Hence  $c = -4900$ . Hence the amount of salt in the tank at time  $t$  is

$$(5) \quad y(t) = 5000 - 4900e^{-0.01t}.$$

This function shows an exponential approach to the limit 5000 lb; see Fig. 9. Can you explain physically that  $y(t)$  should increase with time? That its limit is 5000 lb? Can you see the limit directly from the ODE?

The model discussed becomes more realistic in problems on pollutants in lakes (see Problem Set 1.5, Prob. 27) or drugs in organs. These types of problems are more difficult because the mixing may be imperfect and the flow rates (in and out) may be different and known only very roughly. ■

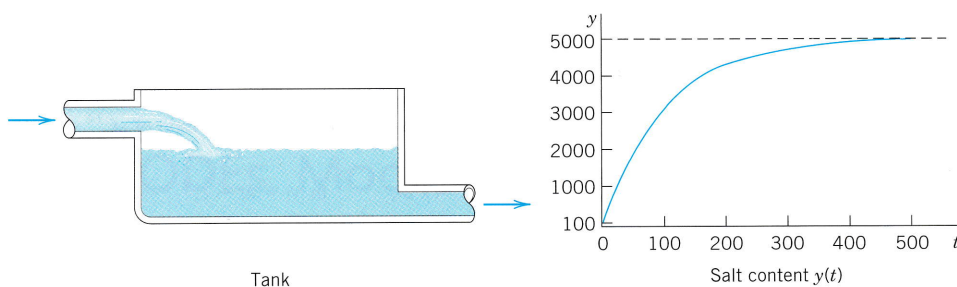


Fig. 9. Mixing problem in Example 3

#### EXAMPLE 4 Heating an Office Building (Newton's Law of Cooling<sup>3</sup>)

Suppose that in Winter the daytime temperature in a certain office building is maintained at 70°F. The heating is shut off at 10 P.M. and turned on again at 6 A.M. On a certain day the temperature inside the building at 2 A.M. was found to be 65°F. The outside temperature was 50°F at 10 P.M. and had dropped to 40°F by 6 A.M. What was the temperature inside the building when the heat was turned on at 6 A.M.?

*Physical information.* Experiments show that the time rate of change of the temperature  $T$  of a body  $B$  (which conducts heat well, as, for example, a copper ball does) is proportional to the difference between  $T$  and the temperature of the surrounding medium (**Newton's law of cooling**).

**Solution.** *Step 1. Setting up a model.* Let  $T(t)$  be the temperature inside the building and  $T_A$  the outside temperature (assumed to be constant in Newton's law). Then by Newton's law,

$$(6) \quad \frac{dT}{dt} = k(T - T_A).$$

Such experimental laws are derived under idealized assumptions that rarely hold exactly. However, even if a model seems to fit the reality only poorly (as in the present case), it may still give valuable qualitative information. To see how good a model is, the engineer will collect experimental data and compare them with calculations from the model.

<sup>3</sup>Sir ISAAC NEWTON (1642–1727), great English physicist and mathematician, became a professor at Cambridge in 1669 and Master of the Mint in 1699. He and the German mathematician and philosopher GOTTFRIED WILHELM LEIBNIZ (1646–1716) invented (independently) the differential and integral calculus. Newton discovered many basic physical laws and created the method of investigating physical problems by means of calculus. His *Philosophiae naturalis principia mathematica* (*Mathematical Principles of Natural Philosophy*, 1687) contains the development of classical mechanics. His work is of greatest importance to both mathematics and physics.

**Step 2. General solution.** We cannot solve (6) because we do not know  $T_A$ , just that it varied between 50°F and 40°F, so we follow the **Golden Rule**: *If you cannot solve your problem, try to solve a simpler one.* We solve (6) with the unknown function  $T_A$  replaced with the average of the two known values, or 45°F. For physical reasons we may expect that this will give us a reasonable approximate value of  $T$  in the building at 6 A.M.

For constant  $T_A = 45$  (or any other *constant* value) the ODE (6) is separable. Separation, integration, and taking exponents gives the general solution

$$\frac{dT}{T - 45} = k dt, \quad \ln |T - 45| = kt + c^*, \quad T(t) = 45 + ce^{kt} \quad (c = e^{c^*}).$$

**Step 3. Particular solution.** We choose 10 P.M. to be  $t = 0$ . Then the given initial condition is  $T(0) = 70$  and yields a particular solution, call it  $T_p$ . By substitution,

$$T(0) = 45 + ce^0 = 70, \quad c = 70 - 45 = 25, \quad T_p(t) = 45 + 25e^{kt}.$$

**Step 4. Determination of  $k$ .** We use  $T(4) = 65$ , where  $t = 4$  is 2 A.M. Solving algebraically for  $k$  and inserting  $k$  into  $T_p(t)$  gives (Fig. 10)

$$T_p(4) = 45 + 25e^{4k} = 65, \quad e^{4k} = 0.8, \quad k = \frac{1}{4} \ln 0.8 = -0.056, \quad T_p(t) = 45 + 25e^{-0.056t}.$$

**Step 5. Answer and interpretation.** 6 A.M. is  $t = 8$  (namely, 8 hours after 10 P.M.), and

$$T_p(8) = 45 + 25e^{-0.056 \cdot 8} = 61 [^\circ\text{F}].$$

Hence the temperature in the building dropped 9°F, a result that looks reasonable. ■

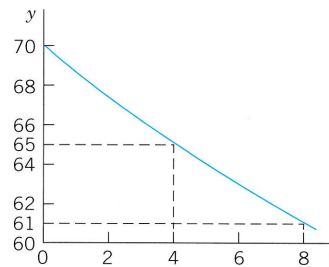


Fig. 10. Particular solution (temperature) in Example 4

### EXAMPLE 5 Leaking Tank. Outflow of Water Through a Hole (Torricelli's Law)

This is another prototype engineering problem that leads to an ODE. It concerns the outflow of water from a cylindrical tank with a hole at the bottom (Fig. 11). You are asked to find the height of the water in the tank at any time if the tank has diameter 2 m, the hole has diameter 1 cm, and the initial height of the water when the hole is opened is 2.25 m. When will the tank be empty?

*Physical information.* Under the influence of gravity the outflowing water has velocity

$$(7) \quad v(t) = 0.600\sqrt{2gh(t)} \quad (\text{Torricelli's law}^4),$$

where  $h(t)$  is the height of the water above the hole at time  $t$ , and  $g = 980 \text{ cm/sec}^2 = 32.17 \text{ ft/sec}^2$  is the acceleration of gravity at the surface of the earth.

**Solution.** *Step 1. Setting up the model.* To get an equation, we relate the decrease in water level  $h(t)$  to the outflow. The volume  $\Delta V$  of the outflow during a short time  $\Delta t$  is

$$\Delta V = Av \Delta t \quad (A = \text{Area of hole}).$$

<sup>4</sup>EVANGELISTA TORRICELLI (1608–1647), Italian physicist, pupil and successor of GALILEO GALILEI (1564–1642) at Florence. The “contraction factor” 0.600 was introduced by J. C. BORDA in 1766 because the stream has a smaller cross section than the area of the hole.



$\Delta V$  must equal the change  $\Delta V^*$  of the volume of the water in the tank. Now

$$\Delta V^* = -B \Delta h \quad (B = \text{Cross-sectional area of tank})$$

where  $\Delta h (> 0)$  is the decrease of the height  $h(t)$  of the water. The minus sign appears because the volume of the water in the tank decreases. Equating  $\Delta V$  and  $\Delta V^*$  gives

$$-B \Delta h = Av \Delta t.$$

We now express  $v$  according to Torricelli's law and then let  $\Delta t$  (the length of the time interval considered) approach 0—this is a *standard way* of obtaining an ODE as a model. That is, we have

$$\frac{\Delta h}{\Delta t} = -\frac{A}{B} v = -\frac{A}{B} 0.600\sqrt{2gh(t)},$$

and by letting  $\Delta t \rightarrow 0$  we obtain the ODE

$$\frac{dh}{dt} = -26.56 \frac{A}{B} \sqrt{h},$$

where  $26.56 = 0.600 \sqrt{2 \cdot 980}$ . This is our model, a first-order ODE.

**Step 2. General solution.** Our ODE is separable.  $A/B$  is constant. Separation and integration gives

$$\frac{dh}{\sqrt{h}} = -26.56 \frac{A}{B} dt \quad \text{and} \quad 2\sqrt{h} = c^* - 26.56 \frac{A}{B} t.$$

Dividing by 2 and squaring gives  $h = (c - 13.28At/B)^2$ . Inserting  $13.28A/B = 13.28 \cdot 0.5^2 \pi / 100^2 \pi = 0.000332$  yields the general solution

$$h(t) = (c - 0.000332t)^2.$$

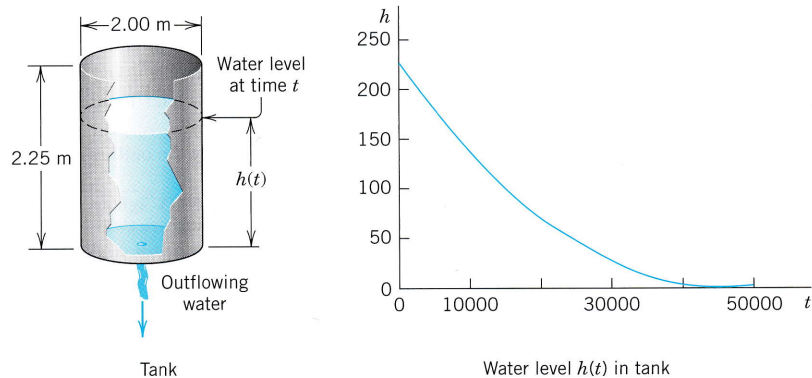
**Step 3. Particular solution.** The initial height (the initial condition) is  $h(0) = 225$  cm. Substitution of  $t = 0$  and  $h = 225$  gives from the general solution  $c^2 = 225$ ,  $c = 15.00$  and thus the particular solution (Fig. 11)

$$h_p(t) = (15.00 - 0.000332t)^2.$$

**Step 4. Tank empty.**  $h_p(t) = 0$  if  $t = 15.00/0.000332 = 45\,181$  [sec] = 12.6 [hours].

Here you see distinctly the *importance of the choice of units*—we have been working with the Cgs system, in which time is measured in seconds! We used  $g = 980$  cm/sec<sup>2</sup>.

**Step 5. Checking.** Check the result. ■



**Fig. 11.** Example 5. Outflow from a cylindrical tank ("leaking tank"). Torricelli's law

## Extended Method: Reduction to Separable Form

Certain nonseparable ODEs can be made separable by transformations that introduce for  $y$  a new unknown function. We discuss this technique for a class of ODEs of practical

importance, namely, for equations

$$(8) \quad y' = f\left(\frac{y}{x}\right).$$

Here,  $f$  is any (differentiable) function of  $y/x$ , such as  $\sin(y/x)$ ,  $(y/x)^4$ , and so on. (Such an ODE is sometimes called a *homogeneous ODE*, a term we shall not use but reserve for a more important purpose in Sec. 1.5.)

The form of such an ODE suggests that we set  $y/x = u$ ; thus,

$$(9) \quad y = ux \quad \text{and by product differentiation} \quad y' = u'x + u.$$

Substitution into  $y' = f(y/x)$  then gives  $u'x + u = f(u)$  or  $u'x = f(u) - u$ . We see that this can be separated:

$$(10) \quad \frac{du}{f(u) - u} = \frac{dx}{x}.$$

### EXAMPLE 6 Reduction to Separable Form

Solve

$$2xyy' = y^2 - x^2.$$

**Solution.** To get the usual explicit form, divide the given equation by  $2xy$ ,

$$y' = \frac{y^2 - x^2}{2xy} = \frac{y}{2x} - \frac{x}{2y}.$$

Now substitute  $y$  and  $y'$  from (9) and then simplify by subtracting  $u$  on both sides,

$$u'x + u = \frac{u}{2} - \frac{1}{2u}, \quad u'x = -\frac{u}{2} - \frac{1}{2u} = \frac{-u^2 - 1}{2u}.$$

You see that in the last equation you can now separate the variables,

$$\frac{2u \, du}{1 + u^2} = -\frac{dx}{x}. \quad \text{By integration,} \quad \ln(1 + u^2) = -\ln|x| + c^* = \ln\left|\frac{1}{x}\right| + c^*.$$

Take exponents on both sides to get  $1 + u^2 = c/x$  or  $1 + (y/x)^2 = c/x$ . Multiply the last equation by  $x^2$  to obtain (Fig. 12)

$$x^2 + y^2 = cx. \quad \text{Thus} \quad \left(x - \frac{c}{2}\right)^2 + y^2 = \frac{c^2}{4}.$$

This general solution represents a family of circles passing through the origin with centers on the  $x$ -axis. ■

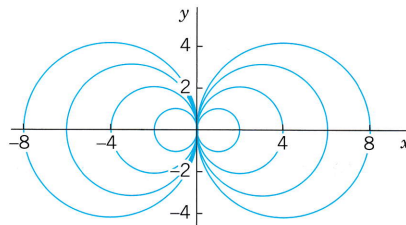


Fig. 12. General solution (family of circles) in Example 6

## PROBLEM SET 1.3

1. **(Constant of integration)** An arbitrary constant of integration must be introduced immediately when the integration is performed. Why is this important? Give an example of your own.

### 2-9 GENERAL SOLUTION

Find a general solution. Show the steps of derivation. Check your answer by substitution.

2.  $y' + (x + 2)y^2 = 0$
3.  $y' = 2 \sec 2y$
4.  $y' = (y + 9x)^2 \quad (y + 9x = v)$
5.  $yy' + 36x = 0$
6.  $y' = (4x^2 + y^2)/(xy)$
7.  $y' \sin \pi x = y \cos \pi x$
8.  $xy' = \frac{1}{2}y^2 + y$
9.  $y' e^{\pi x} = y^2 + 1$

### 10-19 INITIAL VALUE PROBLEMS

Find the particular solution. Show the steps of derivation, beginning with the general solution. ( $L, R, b$  are constants.)

10.  $yy' + 4x = 0, y(0) = 3$
11.  $dr/dt = -2tr, r(0) = r_0$
12.  $2xyy' = 3y^2 + x^2, y(1) = 2$
13.  $L \, dI/dt + RI = 0, I(0) = I_0$
14.  $y' = y/x + (2x^3/y) \cos(x^2), y(\sqrt{\pi}/2) = \sqrt{\pi}$
15.  $e^{2x}y' = 2(x + 2)y^3, y(0) = 1/\sqrt{5} \approx 0.45$
16.  $xy' = y + 4x^5 \cos^2(y/x), y(2) = 0$
17.  $y'x \ln x = y, y(3) = \ln 81$
18.  $dr/d\theta = b[(dr/d\theta) \cos \theta + r \sin \theta], r(\frac{1}{2}\pi) = \pi, 0 < b < 1$
19.  $yy' = (x - 1)e^{-y^2}, y(0) = 1$
20. **(Particular solution)** Introduce limits of integration in (3) such that  $y$  obtained from (3) satisfies the initial condition  $y(x_0) = y_0$ . Try the formula out on Prob. 19.

### 21-36 APPLICATIONS, MODELING

21. **(Curves)** Find all curves in the  $xy$ -plane whose tangents all pass through a given point  $(a, b)$ .
22. **(Curves)** Show that any (nonvertical) straight line through the origin of the  $xy$ -plane intersects all solution curves of  $y' = g(y/x)$  at the same angle.
23. **(Exponential growth)** If the growth rate of the amount of yeast at any time  $t$  is proportional to the amount present at that time and doubles in 1 week, how much yeast can be expected after 2 weeks? After 4 weeks?
24. **(Population model)** If in a population of bacteria the birth rate and death rate are proportional to the number of individuals present, what is the population as a function of time? Figure out the limiting situation for increasing time and interpret it.
25. **(Radiocarbon dating)** If a fossilized tree is claimed to be 4000 years old, what should be its  ${}_6C^{14}$  content expressed as a percent of the ratio of  ${}_6C^{14}$  to  ${}_6C^{12}$  in a living organism?
26. **(Gompertz growth in tumors)** The Gompertz model is  $y' = -Ay \ln y$  ( $A > 0$ ), where  $y(t)$  is the mass of tumor cells at time  $t$ . The model agrees well with clinical observations. The declining growth rate with increasing  $y > 1$  corresponds to the fact that cells in the interior of a tumor may die because of insufficient oxygen and nutrients. Use the ODE to discuss the growth and decline of solutions (tumors) and to find constant solutions. Then solve the ODE.
27. **(Dryer)** If wet laundry loses half of its moisture during the first 5 minutes of drying in a dryer and if the rate of loss of moisture is proportional to the moisture content, when will the laundry be practically dry, say, when will it have lost 95% of its moisture? First guess.
28. **(Alibi?)** Jack, arrested when leaving a bar, claims that he has been inside for at least half an hour (which would provide him with an alibi). The police check the water temperature of his car (parked near the entrance of the bar) at the instant of arrest and again 30 minutes later, obtaining the values  $190^\circ\text{F}$  and  $110^\circ\text{F}$ , respectively. Do these results give Jack an alibi? (Solve by inspection.)
29. **(Law of cooling)** A thermometer, reading  $10^\circ\text{C}$ , is brought into a room whose temperature is  $23^\circ\text{C}$ . Two minutes later the thermometer reading is  $18^\circ\text{C}$ . How long will it take until the reading is practically  $23^\circ\text{C}$ , say,  $22.8^\circ\text{C}$ ? First guess.
30. **(Torricelli's law)** How does the answer in Example 5 (the time when the tank is empty) change if the diameter of the hole is doubled? First guess.
31. **(Torricelli's law)** Show that (7) looks reasonable inasmuch as  $\sqrt{2gh(t)}$  is the speed a body gains if it falls a distance  $h$  (and air resistance is neglected).
32. **(Rope)** To tie a boat in a harbor, how many times must a rope be wound around a bollard (a vertical rough cylindrical post fixed on the ground) so that a man holding one end of the rope can resist a force exerted by the boat one thousand times greater than the man can exert? First guess. Experiments show that the change  $\Delta S$  of the force  $S$  in a small portion of the rope is proportional to  $S$  and to the small angle  $\Delta\phi$  in Fig. 13. Take the proportionality constant 0.15.

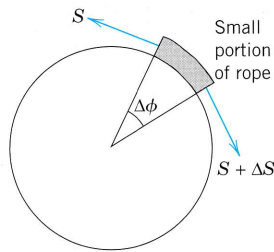


Fig. 13. Problem 32

33. **(Mixing)** A tank contains 800 gal of water in which 200 lb of salt is dissolved. Two gallons of fresh water runs in per minute, and 2 gal of the mixture in the tank, kept uniform by stirring, runs out per minute. How much salt is left in the tank after 5 hours?
34. **WRITING PROJECT. Exponential Increase, Decay, Approach.** Collect, order, and present all the information on the ODE  $y' = ky$  and its applications from the text and the problems. Add examples of your own.
35. **CAS EXPERIMENT. Graphing Solutions.** A CAS can usually graph solutions even if they are given by integrals that cannot be evaluated by the usual methods of calculus. Show this as follows.

(A) Graph the curves for the seven initial value problems  $y' = e^{-x^2/2}$ ,  $y(0) = 0, \pm 1, \pm 2, \pm 3$ , common axes. Are these curves congruent? Why?

(B) Experiment with approximate curves of  $n$ th partial sums of the Maclaurin series obtained by termwise integration of that of  $y$  in (A); graph them and describe qualitatively the accuracy for a fixed interval  $0 \leq x \leq b$  and increasing  $n$ , and then for fixed  $n$  and increasing  $b$ .

(C) Experiment with  $y' = \cos(x^2)$  as in (B).

(D) Find an initial value problem with solution

$$y = e^{x^2} \int_0^x e^{-t^2} dt \text{ and experiment with it as in (B).}$$

36. **TEAM PROJECT. Torricelli's Law.** Suppose that the tank in Example 5 is hemispherical, of radius  $R$ , initially full of water, and has an outlet of  $5 \text{ cm}^2$  cross-sectional area at the bottom. (Make a sketch.) Set up the model for outflow. Indicate what portion of your work in Example 5 you can use (so that it can become part of the general method independent of the shape of the tank). Find the time  $t$  to empty the tank (a) for any  $R$ , (b) for  $R = 1 \text{ m}$ . Plot  $t$  as function of  $R$ . Find the time when  $h = R/2$  (a) for any  $R$ , (b) for  $R = 1 \text{ m}$ .

## 1.4 Exact ODEs. Integrating Factors

We remember from calculus that if a function  $u(x, y)$  has continuous partial derivatives, its **differential** (also called its *total differential*) is

$$du = \frac{\partial u}{\partial x} dx + \frac{\partial u}{\partial y} dy.$$

From this it follows that if  $u(x, y) = c = \text{const}$ , then  $du = 0$ .

For example, if  $u = x + x^2y^3 = c$ , then

$$du = (1 + 2xy^3) dx + 3x^2y^2 dy = 0$$

or

$$y' = \frac{dy}{dx} = -\frac{1 + 2xy^3}{3x^2y^2},$$

an ODE that we can solve by going backward. This idea leads to a powerful solution method as follows.

A first-order ODE  $M(x, y) + N(x, y)y' = 0$ , written as (use  $dy = y' dx$  as in Sec. 1.3)

$$(1) \quad M(x, y) dx + N(x, y) dy = 0$$

is called an **exact differential equation** if the **differential form**  $M(x, y) dx + N(x, y) dy$  is **exact**, that is, this form is the differential

$$(2) \quad du = \frac{\partial u}{\partial x} dx + \frac{\partial u}{\partial y} dy$$

of some function  $u(x, y)$ . Then (1) can be written

$$du = 0.$$

By integration we immediately obtain the general solution of (1) in the form

$$(3) \quad u(x, y) = c.$$

This is called an **implicit solution**, in contrast with a solution  $y = h(x)$  as defined in Sec. 1.1, which is also called an *explicit solution*, for distinction. Sometimes an implicit solution can be converted to explicit form. (Do this for  $x^2 + y^2 = 1$ .) If this is not possible, your CAS may graph a figure of the **contour lines** (3) of the function  $u(x, y)$  and help you in understanding the solution.

Comparing (1) and (2), we see that (1) is an exact differential equation if there is some function  $u(x, y)$  such that

$$(4) \quad (a) \quad \frac{\partial u}{\partial x} = M, \quad (b) \quad \frac{\partial u}{\partial y} = N.$$

From this we can derive a formula for checking whether (1) is exact or not, as follows.

Let  $M$  and  $N$  be continuous and have continuous first partial derivatives in a region in the  $xy$ -plane whose boundary is a closed curve without self-intersections. Then by partial differentiation of (4) (see App. 3.2 for notation),

$$\begin{aligned} \frac{\partial M}{\partial y} &= \frac{\partial^2 u}{\partial y \partial x}, \\ \frac{\partial N}{\partial x} &= \frac{\partial^2 u}{\partial x \partial y}. \end{aligned}$$

By the assumption of continuity the two second partial derivatives are equal. Thus

$$(5) \quad \frac{\partial M}{\partial y} = \frac{\partial N}{\partial x}.$$

This condition is not only necessary but also sufficient for (1) to be an exact differential equation. (We shall prove this in Sec. 10.2 in another context. Some calculus books (e.g., Ref. [GR11] also contain a proof.)

If (1) is exact, the function  $u(x, y)$  can be found by inspection or in the following systematic way. From (4a) we have by integration with respect to  $x$

$$(6) \quad u = \int M dx + k(y);$$

in this integration,  $y$  is to be regarded as a constant, and  $k(y)$  plays the role of a “constant” of integration. To determine  $k(y)$ , we derive  $\partial u/\partial y$  from (6), use (4b) to get  $dk/dy$ , and integrate  $dk/dy$  to get  $k$ .

Formula (6) was obtained from (4a). Instead of (4a) we may equally well use (4b). Then instead of (6) we first have by integration with respect to  $y$

$$(6^*) \quad u = \int N dy + l(x).$$

To determine  $l(x)$ , we derive  $\partial u/\partial x$  from (6\*), use (4a) to get  $dll/dx$ , and integrate. We illustrate all this by the following typical examples.

### EXAMPLE 1 An Exact ODE

Solve

$$(7) \quad \cos(x+y) dx + (3y^2 + 2y + \cos(x+y)) dy = 0.$$

**Solution.** *Step 1. Test for exactness.* Our equation is of the form (1) with

$$M = \cos(x+y),$$

$$N = 3y^2 + 2y + \cos(x+y).$$

Thus

$$\frac{\partial M}{\partial y} = -\sin(x+y),$$

$$\frac{\partial N}{\partial x} = -\sin(x+y).$$

From this and (5) we see that (7) is exact.

*Step 2. Implicit general solution.* From (6) we obtain by integration

$$(8) \quad u = \int M dx + k(y) = \int \cos(x+y) dx + k(y) = \sin(x+y) + k(y).$$

To find  $k(y)$ , we differentiate this formula with respect to  $y$  and use formula (4b), obtaining

$$\frac{\partial u}{\partial y} = \cos(x+y) + \frac{dk}{dy} = N = 3y^2 + 2y + \cos(x+y).$$

Hence  $dk/dy = 3y^2 + 2y$ . By integration,  $k = y^3 + y^2 + c^*$ . Inserting this result into (8) and observing (3), we obtain the *answer*

$$u(x, y) = \sin(x+y) + y^3 + y^2 = c.$$

*Step 3. Checking an implicit solution.* We can check by differentiating the implicit solution  $u(x, y) = c$  implicitly and see whether this leads to the given ODE (7):

$$(9) \quad du = \frac{\partial u}{\partial x} dx + \frac{\partial u}{\partial y} dy = \cos(x+y) dx + (\cos(x+y) + 3y^2 + 2y) dy = 0.$$

This completes the check. ■

**EXAMPLE 2 An Initial Value Problem**

Solve the initial value problem

$$(10) \quad (\cos y \sinh x + 1) dx - \sin y \cosh x dy = 0, \quad y(1) = 2.$$

**Solution.** You may verify that the given ODE is exact. We find  $u$ . For a change, let us use (6\*),

$$u = - \int \sin y \cosh x dy + l(x) = \cos y \cosh x + l(x).$$

From this,  $\partial u / \partial x = \cos y \sinh x + dl/dx = M = \cos y \sinh x + 1$ . Hence  $dl/dx = 1$ . By integration,  $l(x) = x + c^*$ . This gives the general solution  $u(x, y) = \cos y \cosh x + x = c$ . From the initial condition,  $\cos 2 \cosh 1 + 1 = 0.358 = c$ . Hence the answer is  $\cos y \cosh x + x = 0.358$ . Figure 14 shows the particular solutions for  $c = 0, 0.358$  (thicker curve), 1, 2, 3. Check that the answer satisfies the ODE. (Proceed as in Example 1.) Also check that the initial condition is satisfied. ■

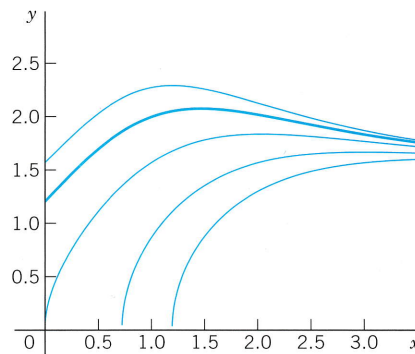


Fig. 14. Particular solutions in Example 2

**EXAMPLE 3 WARNING! Breakdown in the Case of Nonexactness**

The equation  $-y dx + x dy = 0$  is not exact because  $M = -y$  and  $N = x$ , so that in (5),  $\partial M / \partial y = -1$  but  $\partial N / \partial x = 1$ . Let us show that in such a case the present method does not work. From (6),

$$u = \int M dx + k(y) = -xy + k(y), \quad \text{hence} \quad \frac{\partial u}{\partial y} = -x + \frac{dk}{dy}.$$

Now,  $\partial u / \partial y$  should equal  $N = x$ , by (4b). However, this is impossible because  $k(y)$  can depend only on  $y$ . Try (6\*); it will also fail. Solve the equation by another method that we have discussed. ■

**Reduction to Exact Form. Integrating Factors**

The ODE in Example 3 is  $-y dx + x dy = 0$ . It is not exact. However, if we multiply it by  $1/x^2$ , we get an exact equation [check exactness by (5)!],

$$(11) \quad \frac{-y dx + x dy}{x^2} = -\frac{y}{x^2} dx + \frac{1}{x} dy = d\left(\frac{y}{x}\right) = 0.$$

Integration of (11) then gives the general solution  $y/x = c = \text{const.}$

This example gives the idea. All we did was multiply a given nonexact equation, say,

$$(12) \quad P(x, y) dx + Q(x, y) dy = 0,$$

by a function  $F$  that, in general, will be a function of both  $x$  and  $y$ . The result was an equation

$$(13) \quad FP dx + FQ dy = 0$$

that is exact, so we can solve it as just discussed. Such a function  $F(x, y)$  is then called an **integrating factor** of (12).

#### EXAMPLE 4 Integrating Factor

The integrating factor in (11) is  $F = 1/x^2$ . Hence in this case the exact equation (13) is

$$FP dx + FQ dy = \frac{-y dx + x dy}{x^2} = d\left(\frac{y}{x}\right) = 0. \quad \text{Solution} \quad \frac{y}{x} = c.$$

These are straight lines  $y = cx$  through the origin.

It is remarkable that we can readily find other integrating factors for the equation  $-y dx + x dy = 0$ , namely,  $1/y^2$ ,  $1/(xy)$ , and  $1/(x^2 + y^2)$ , because

$$(14) \quad \frac{-y dx + x dy}{y^2} = d\left(\frac{x}{y}\right), \quad \frac{-y dx + x dy}{xy} = -d\left(\ln \frac{x}{y}\right), \quad \frac{-y dx + x dy}{x^2 + y^2} = d\left(\arctan \frac{y}{x}\right). \quad \blacksquare$$

## How to Find Integrating Factors

In simpler cases we may find integrating factors by inspection or perhaps after some trials, keeping (14) in mind. In the general case, the idea is the following.

For  $M dx + N dy = 0$  the exactness condition (4) is  $\partial M/\partial y = \partial N/\partial x$ . Hence for (13),  $FP dx + FQ dy = 0$ , the exactness condition is

$$(15) \quad \frac{\partial}{\partial y} (FP) = \frac{\partial}{\partial x} (FQ).$$

By the product rule, with subscripts denoting partial derivatives, this gives

$$F_y P + FP_y = F_x Q + FQ_x.$$

In the general case, this would be complicated and useless. So we follow the **Golden Rule**: *If you cannot solve your problem, try to solve a simpler one*—the result may be useful (and may also help you later on). Hence we look for an integrating factor depending only on **one** variable; fortunately, in many practical cases, there are such factors, as we shall see. Thus, let  $F = F(x)$ . Then  $F_y = 0$ , and  $F_x = F' = dF/dx$ , so that (15) becomes

$$FP_y = F'Q + FQ_x.$$

Dividing by  $FQ$  and reshuffling terms, we have

$$(16) \quad \frac{1}{F} \frac{dF}{dx} = R, \quad \text{where} \quad R = \frac{1}{Q} \left( \frac{\partial P}{\partial y} - \frac{\partial Q}{\partial x} \right).$$

This proves the following theorem.



**THEOREM 1****Integrating Factor  $F(x)$** 

If (12) is such that the right side  $R$  of (16), depends only on  $x$ , then (12) has an integrating factor  $F = F(x)$ , which is obtained by integrating (16) and taking exponents on both sides,

$$(17) \quad F(x) = \exp \int R(x) dx.$$

Similarly, if  $F^* = F^*(y)$ , then instead of (16) we get

$$(18) \quad \frac{1}{F^*} \frac{dF^*}{dy} = R^*, \quad \text{where} \quad R^* = \frac{1}{P} \left( \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right)$$

and we have the companion

**THEOREM 2****Integrating Factor  $F^*(y)$** 

If (12) is such that the right side  $R^*$  of (18) depends only on  $y$ , then (12) has an integrating factor  $F^* = F^*(y)$ , which is obtained from (18) in the form

$$(19) \quad F^*(y) = \exp \int R^*(y) dy.$$

**EXAMPLE 5****Application of Theorems 1 and 2. Initial Value Problem**

Using Theorem 1 or 2, find an integrating factor and solve the initial value problem

$$(20) \quad (e^{x+y} + ye^y) dx + (xe^y - 1) dy = 0, \quad y(0) = -1$$

**Solution.** *Step 1. Nonexactness.* The exactness check fails:

$$\frac{\partial P}{\partial y} = \frac{\partial}{\partial y} (e^{x+y} + ye^y) = e^{x+y} + e^y + ye^y \quad \text{but} \quad \frac{\partial Q}{\partial x} = \frac{\partial}{\partial x} (xe^y - 1) = e^y.$$

*Step 2. Integrating factor. General solution.* Theorem 1 fails because  $R$  [the right side of (16)] depends on both  $x$  and  $y$ ,

$$R = \frac{1}{Q} \left( \frac{\partial P}{\partial y} - \frac{\partial Q}{\partial x} \right) = \frac{1}{xe^y - 1} (e^{x+y} + e^y + ye^y - e^y).$$

Try Theorem 2. The right side of (18) is

$$R^* = \frac{1}{P} \left( \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) = \frac{1}{e^{x+y} + ye^y} (e^y - e^{x+y} - e^y - ye^y) = -1.$$

Hence (19) gives the integrating factor  $F^*(y) = e^{-y}$ . From this result and (20) you get the exact equation

$$(e^x + y) dx + (x - e^{-y}) dy = 0.$$

Test for exactness; you will get 1 on both sides of the exactness condition. By integration, using (4a),

$$u = \int (e^x + y) dx = e^x + xy + k(y).$$

Differentiate this with respect to  $y$  and use (4b) to get

$$\frac{\partial u}{\partial y} = x + \frac{dk}{dy} = N = x - e^{-y}, \quad \frac{dk}{dy} = -e^{-y}, \quad k = e^{-y} + c^*$$

Hence the general solution is

$$u(x, y) = e^x + xy + e^{-y} = c.$$

**Step 3. Particular solution.** The initial condition  $y(0) = 1$  gives  $u(0, -1) = 1 + 0 + e = 3.72$ . Hence the answer is  $e^x + xy + e^{-y} = 1 + e = 3.72$ . Figure 15 shows several particular solutions obtained as level curves of  $u(x, y) = c$ , obtained by a CAS, a convenient way in cases in which it is impossible or difficult to cast a solution into explicit form. Note the curve that (nearly) satisfies the initial condition.

**Step 4. Checking.** Check by substitution that the answer satisfies the given equation as well as the initial condition. ■

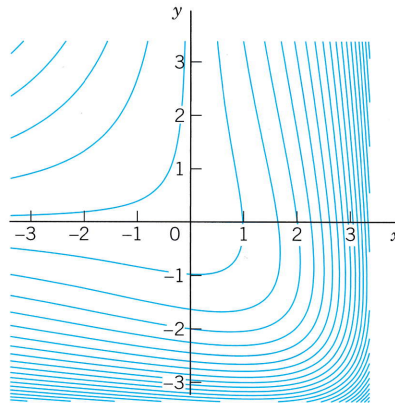


Fig. 15. Particular solutions in Example 5

## PROBLEM SET 1.4

### 1–20 EXACT ODEs. INTEGRATING FACTORS

Test for exactness. If exact, solve. If not, use an integrating factor as given or find it by inspection or from the theorems in the text. Also, if an initial condition is given, determine the corresponding particular solution.

1.  $x^3 dx + y^3 dy = 0$
2.  $(x - y)(dx - dy) = 0$
3.  $-\pi \sin \pi x \sinh y dx + \cos \pi x \cosh y dy = 0$
4.  $(e^y - ye^x) dx + (xe^y - e^x) dy = 0$
5.  $9x dx + 4y dy = 0$
6.  $e^x(\cos y dx - \sin y dy) = 0$
7.  $e^{-2\theta} dr - 2re^{-2\theta} d\theta = 0$
8.  $(2x + 1/y - y/x^2) dx + (2y + 1/x - x/y^2) dy = 0$
9.  $(-y/x^2 + 2 \cos 2x) dx + (1/x - 2 \sin 2y) dy = 0$
10.  $-2xy \sin(x^2) dx + \cos(x^2) dy = 0$
11.  $-y dx + x dy = 0$
12.  $(e^{x+y} - y) dx + (xe^{x+y} + 1) dy = 0$
13.  $-3y dx + 2x dy = 0, F(x, y) = y/x^4$
14.  $(x^4 + y^2) dx - xy dy = 0, y(2) = 1$
15.  $e^{2x}(2 \cos y dx - \sin y dy) = 0, y(0) = 0$
16.  $-\sin xy (y dx + x dy) = 0, y(1) = \pi$
17.  $(\cos \omega x + \omega \sin \omega x) dx + e^x dy = 0, y(0) = 1$
18.  $(\cos xy + x/y) dx + (1 + (x/y) \cos xy) dy = 0$
19.  $e^{-y} dx + e^{-x}(-e^{-y} + 1) dy = 0, F = e^{x+y}$
20.  $(\sin y \cos y + x \cos^2 y) dx + x dy = 0$
21. Under what conditions for the constants  $A, B, C, D$  is  $(Ax + By) dx + (Cx + Dy) dy = 0$  exact? Solve the exact equation.

**22. CAS PROJECT. Graphing Particular Solutions**

Graph particular solutions of the following ODE, proceeding as explained.

$$(21) \quad y \cos x \, dx + \frac{1}{y} \, dy = 0$$

- (a) Test for exactness. If necessary, find an integrating factor. Find the general solution  $u(x, y) = c$ .  
 (b) Solve (21) by separating variables. Is this simpler than (a)?  
 (c) Graph contours  $u(x, y) = c$  by your CAS. (Cf. Fig. 16.)

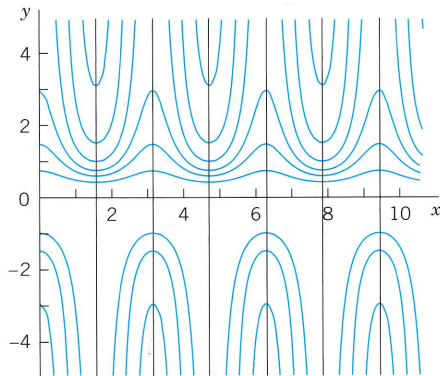


Fig. 16. Particular solutions in CAS Project 22

(d) In another graph show the solution curves satisfying  $y(0) = \pm 1, \pm 2, \pm 3, \pm 4$ . Compare the quality of (c) and (d) and comment.

(e) Do the same steps for another nonexact ODE of your choice.

**23. WRITING PROJECT. Working Backward.**

Start from solutions  $u(x, y) = c$  of your choice, find a corresponding exact ODE, destroy exactness by a multiplication or division. This should give you a feel for the form of ODEs you can reach by the method of integrating factors. (Working backward is useful in other areas, too; Euler and other great masters frequently did it.)

**24. TEAM PROJECT. Solution by Several Methods.**

Show this as indicated. Compare the amount of work.

(A)  $e^y(\sinh x \, dx + \cosh x \, dy) = 0$  as an exact ODE and by separation.

(B)  $(1 + 2x) \cos y \, dx + dy/\cos y = 0$  by Theorem 2 and by separation.

(C)  $(x^2 + y^2) \, dx - 2xy \, dy = 0$  by Theorem 1 or 2 and by separation with  $v = y/x$ .

(D)  $3x^2 y \, dx + 4x^3 \, dy = 0$  by Theorems 1 and 2 and by separation.

(E) Search the text and the problems for further ODEs that can be solved by more than one of the methods discussed so far. Make a list of these ODEs. Find further cases of your own.

## 1.5 Linear ODEs. Bernoulli Equation. Population Dynamics

Linear ODEs or ODEs that can be transformed to linear form are models of various phenomena, for instance, in physics, biology, population dynamics, and ecology, as we shall see. A first-order ODE is said to be **linear** if it can be written

$$(1) \quad y' + p(x)y = r(x).$$

The defining feature of this equation is that it is linear in both the unknown function  $y$  and its derivative  $y' = dy/dx$ , whereas  $p$  and  $r$  may be **any** given functions of  $x$ . If in an application the independent variable is time, we write  $t$  instead of  $x$ .

If the first term is  $f(x)y'$  (instead of  $y'$ ), divide the equation by  $f(x)$  to get the “**standard form**” (1), with  $y'$  as the first term, which is practical.

For instance,  $y' \cos x + y \sin x = x$  is a linear ODE, and its standard form is  $y' + y \tan x = x \sec x$ .

The function  $r(x)$  on the right may be a force, and the solution  $y(x)$  a displacement in a motion or an electrical current or some other physical quantity. In engineering,  $r(x)$  is frequently called the **input**, and  $y(x)$  is called the **output** or the *response* to the input (and, if given, to the initial condition).

**Homogeneous Linear ODE.** We want to solve (1) in some interval  $a < x < b$ , call it  $J$ , and we begin with the simpler special case that  $r(x)$  is zero for all  $x$  in  $J$ . (This is sometimes written  $r(x) \equiv 0$ .) Then the ODE (1) becomes

$$(2) \quad y' + p(x)y = 0$$

and is called **homogeneous**. By separating variables and integrating we then obtain

$$\frac{dy}{y} = -p(x) dx, \quad \text{thus} \quad \ln |y| = -\int p(x) dx + c^*.$$

Taking exponents on both sides, we obtain the general solution of the homogeneous ODE (2),

$$(3) \quad y(x) = ce^{-\int p(x) dx} \quad (c = \pm e^{c^*} \text{ when } y \geq 0);$$

here we may also choose  $c = 0$  and obtain the **trivial solution**  $y(x) = 0$  for all  $x$  in that interval.

**Nonhomogeneous Linear ODE.** We now solve (1) in the case that  $r(x)$  in (1) is not everywhere zero in the interval  $J$  considered. Then the ODE (1) is called **nonhomogeneous**. It turns out that in this case, (1) has a pleasant property; namely, it has an integrating factor depending only on  $x$ . We can find this factor  $F(x)$  by Theorem 1 in the last section. For this purpose we write (1) as

$$(py - r) dx + dy = 0.$$

This is  $P dx + Q dy = 0$ , where  $P = py - r$  and  $Q = 1$ . Hence the right side of (16) in Sec. 1.4 is simply  $1(p - 0) = p$ , so that (16) becomes

$$\frac{1}{F} \frac{dF}{dx} = p(x).$$

Separation and integration gives

$$\frac{dF}{F} = p dx \quad \text{and} \quad \ln |F| = \int p dx.$$

Taking exponents on both sides, we obtain the desired integrating factor  $F(x)$ ,

$$F(x) = e^{\int p dx}.$$

We now multiply (1) on both sides by this  $F$ . Then by the product rule,

$$e^{\int p dx}(y' + py) = (e^{\int p dx} y)' = e^{\int p dx} r.$$

By integrating the second and third of these three expressions with respect to  $x$  we get

$$e^{\int p dx} y = \int e^{\int p dx} r dx + c.$$

Dividing this equation by  $e^{\int p dx}$  and denoting the exponent  $\int p dx$  by  $h$ , we obtain

$$(4) \quad y(x) = e^{-h} \left( \int e^h r dx + c \right), \quad h = \int p(x) dx.$$

(The constant of integration in  $h$  does not matter; see Prob. 2.) Formula (4) is the general solution of (1) in the form of an integral. Solving (1) is now reduced to the evaluation of an integral. In cases in which this cannot be done by the usual methods of calculus, one may have to use a numeric method for integrals (Sec. 19.5) or for the ODE itself (Sec. 21.1).

The structure of (4) is interesting. The only quantity depending on a given initial condition is  $c$ . Accordingly, writing (4) as a sum of two terms,

$$(4^*) \quad y(x) = e^{-h} \int e^{hr} dx + ce^{-h},$$

we see the following:

$$(5) \quad \text{Total Output} = \text{Response to the Input } r + \text{Response to the Initial Data.}$$

### EXAMPLE 1 First-Order ODE, General Solution

Solve the linear ODE

$$y' - y = e^{2x}.$$

**Solution.** Here,

$$p = -1, \quad r = e^{2x}, \quad h = \int p dx = -x$$

and from (4) we obtain the general solution

$$y(x) = e^x \left( \int e^{-x} e^{2x} dx + c \right) = e^x(e^x + c) = ce^x + e^{2x}.$$

From (4\*) and (5) we see that the response to the input is  $e^{2x}$ .

In simpler cases, such as the present, we may not need the general formula (4), but may wish to proceed directly, multiplying the given equation by  $e^h = e^{-x}$ . This gives

$$(y' - y)e^{-x} = (ye^{-x})' = e^{2x}e^{-x} = e^x.$$

Integrating on both sides, we obtain the same result as before:

$$ye^{-x} = e^x + c, \quad \text{hence} \quad y = e^{2x} + ce^x. \quad \blacksquare$$

### EXAMPLE 2 First-Order ODE, Initial Value Problem

Solve the initial value problem

$$y' + y \tan x = \sin 2x, \quad y(0) = 1.$$

**Solution.** Here  $p = \tan x$ ,  $r = \sin 2x = 2 \sin x \cos x$ , and

$$\int p dx = \int \tan x dx = \ln |\sec x|.$$

From this we see that in (4),

$$e^h = \sec x, \quad e^{-h} = \cos x, \quad e^{hr} = (\sec x)(2 \sin x \cos x) = 2 \sin x,$$

and the general solution of our equation is

$$y(x) = \cos x \left( 2 \int \sin x dx + c \right) = c \cos x - 2 \cos^2 x.$$

From this and the initial condition,  $1 = c \cdot 1 - 2 \cdot 1^2$ ; thus  $c = 3$  and the solution of our initial value problem is  $y = 3 \cos x - 2 \cos^2 x$ . Here  $3 \cos x$  is the response to the initial data, and  $-2 \cos^2 x$  is the response to the input  $\sin 2x$ . \blacksquare

**EXAMPLE 3 Hormone Level**

Assume that the level of a certain hormone in the blood of a patient varies with time. Suppose that the time rate of change is the difference between a sinusoidal input of a 24-hour period from the thyroid gland and a continuous removal rate proportional to the level present. Set up a model for the hormone level in the blood and find its general solution. Find the particular solution satisfying a suitable initial condition.

**Solution.** *Step 1. Setting up a model.* Let  $y(t)$  be the hormone level at time  $t$ . Then the removal rate is  $Ky(t)$ . The input rate is  $A + B \cos(2\pi t/24)$ , where  $A$  is the average input rate, and  $A \geq B$  to make the input nonnegative. (The constants  $A$ ,  $B$ , and  $K$  can be determined by measurements.) Hence the model is

$$y'(t) = \text{In} - \text{Out} = A + B \cos\left(\frac{1}{12}\pi t\right) - Ky(t) \quad \text{or} \quad y' + Ky = A + B \cos\left(\frac{1}{12}\pi t\right).$$

The initial condition for a particular solution  $y_{part}$  is  $y_{part}(0) = y_0$  with  $t = 0$  suitably chosen, e.g., 6:00 A.M.

*Step 2. General solution.* In (4) we have  $p = K = \text{const}$ ,  $h = Kt$ , and  $r = A + B \cos(\frac{1}{12}\pi t)$ . Hence (4) gives the general solution

$$\begin{aligned} y(t) &= e^{-Kt} \int e^{Kt} \left( A + B \cos \frac{\pi t}{12} \right) dt + ce^{-Kt} \\ &= e^{-Kt} e^{Kt} \left[ \frac{A}{K} + \frac{B}{144K^2 + \pi^2} \left( 144K \cos \frac{\pi t}{12} + 12\pi \sin \frac{\pi t}{12} \right) \right] + ce^{-Kt} \\ &= \frac{A}{K} + \frac{B}{144K^2 + \pi^2} \left( 144K \cos \frac{\pi t}{12} + 12\pi \sin \frac{\pi t}{12} \right) + ce^{-Kt}. \end{aligned}$$

The last term decreases to 0 as  $t$  increases, practically after a short time and regardless of  $c$  (that is, of the initial condition). The other part of  $y(t)$  is called the **steady-state solution** because it consists of constant and periodic terms. The entire solution is called the **transient-state solution** because it models the transition from rest to the steady state. These terms are used quite generally for physical and other systems whose behavior depends on time.

*Step 3. Particular solution.* Setting  $t = 0$  in  $y(t)$  and choosing  $y_0 = 0$ , we have

$$y(0) = \frac{A}{K} + \frac{B}{144K^2 + \pi^2} \cdot 144K + c = 0, \quad \text{thus} \quad c = -\frac{A}{K} - \frac{B}{144K^2 + \pi^2} \cdot 144K.$$

Inserting this result into  $y(t)$ , we obtain the particular solution

$$y_{part}(t) = \frac{A}{K} + \frac{B}{144K^2 + \pi^2} \left( 144K \cos \frac{\pi t}{12} + 12\pi \sin \frac{\pi t}{12} \right) - \left( \frac{A}{K} + \frac{144KB}{144K^2 + \pi^2} \right) e^{-Kt}$$

with the steady-state part as before. To plot  $y_{part}$  we must specify values for the constants, say,  $A = B = 1$  and  $K = 0.05$ . Figure 17 shows this solution. Notice that the transition period is relatively short (although  $K$  is small), and the curve soon looks sinusoidal; this is the response to the input  $A + B \cos(\frac{1}{12}\pi t) = 1 + \cos(\frac{1}{12}\pi t)$ . ■

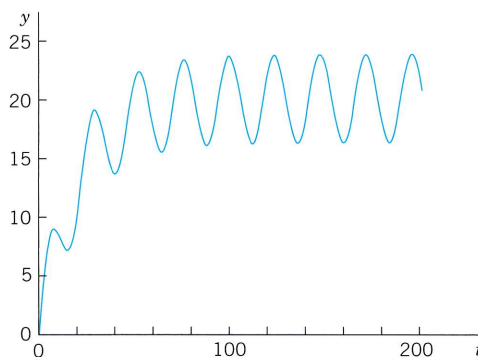


Fig. 17. Particular solution in Example 3

## Reduction to Linear Form. Bernoulli Equation

Numerous applications can be modeled by ODEs that are nonlinear but can be transformed to linear ODEs. One of the most useful ones of these is the **Bernoulli equation**<sup>5</sup>

$$(6) \quad y' + p(x)y = g(x)y^a \quad (a \text{ any real number}).$$

If  $a = 0$  or  $a = 1$ , Equation (6) is linear. Otherwise it is nonlinear. Then we set

$$u(x) = [y(x)]^{1-a}.$$

We differentiate this and substitute  $y'$  from (6), obtaining

$$u' = (1 - a)y^{-a}y' = (1 - a)y^{-a}(gy^a - py).$$

Simplification gives

$$u' = (1 - a)(g - py^{1-a}),$$

where  $y^{1-a} = u$  on the right, so that we get the linear ODE

$$(7) \quad u' + (1 - a)pu = (1 - a)g.$$

For further ODEs reducible to linear form, see Ince's classic [A11] listed in App. 1. See also Team Project 44 in Problem Set 1.5.

### EXAMPLE 4 Logistic Equation

Solve the following Bernoulli equation, known as the **logistic equation** (or **Verhulst equation**<sup>6</sup>):

$$(8) \quad y' = Ay - By^2$$

**Solution.** Write (8) in the form (6), that is,

$$y' - Ay = -By^2$$

to see that  $a = 2$ , so that  $u = y^{1-a} = y^{-1}$ . Differentiate this  $u$  and substitute  $y'$  from (8),

$$u' = -y^{-2}y' = -y^{-2}(Ay - By^2) = B - Ay^{-1}.$$

The last term is  $-Ay^{-1} = -Au$ . Hence we have obtained the linear ODE

<sup>5</sup>JAKOB BERNOULLI (1654–1705), Swiss mathematician, professor at Basel, also known for his contribution to elasticity theory and mathematical probability. The method for solving Bernoulli's equation was discovered by the Leibniz in 1696. Jakob Bernoulli's students included his nephew NIKLAUS BERNOULLI (1687–1759), who contributed to probability theory and infinite series, and his youngest brother JOHANN BERNOULLI (1667–1748), who had profound influence on the development of calculus, became Jakob's successor at Basel, and had among his students GABRIEL CRAMER (see Sec. 7.7) and LEONHARD EULER (see Sec. 2.5). His son DANIEL BERNOULLI (1700–1782) is known for his basic work in fluid flow and the kinetic theory of gases.

<sup>6</sup>PIERRE-FRANÇOIS VERHULST, Belgian statistician, who introduced Eq. (8) as a model for human population growth in 1838.

$$u' + Au = B.$$

The general solution is [by (4)]

$$u = ce^{-At} + B/A.$$

Since  $u = 1/y$ , this gives the general solution of (8),

$$(9) \quad y = \frac{1}{u} = \frac{1}{ce^{-At} + B/A} \quad (\text{Fig. 18}).$$

Directly from (8) we see that  $y \equiv 0$  ( $y(t) = 0$  for all  $t$ ) is also a solution. ■

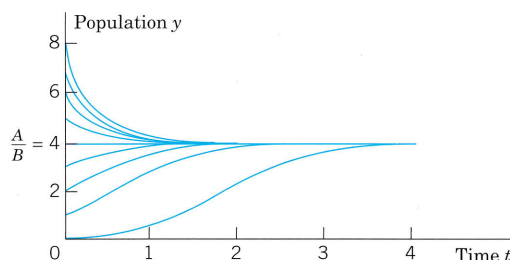


Fig. 18. Logistic population model. Curves (9) in Example 4 with  $A/B = 4$

## Population Dynamics

The logistic equation (8) plays an important role in **population dynamics**, a field that models the evolution of populations of plants, animals, or humans over time  $t$ . If  $B = 0$ , then (8) is  $y' = dy/dt = Ay$ . In this case its solution (9) is  $y = (1/c)e^{At}$  and gives exponential growth, as for a small population in a large country (the United States in early times!). This is called **Malthus's law**. (See also Example 3 in Sec. 1.1.)

The term  $-By^2$  in (8) is a “braking term” that prevents the population from growing without bound. Indeed, if we write  $y' = Ay[1 - (B/A)y]$ , we see that if  $y < A/B$ , then  $y' > 0$ , so that an initially small population keeps growing as long as  $y < A/B$ . But if  $y > A/B$ , then  $y' < 0$  and the population is decreasing as long as  $y > A/B$ . The limit is the same in both cases, namely,  $A/B$ . See Fig. 18.

We see that in the logistic equation (8) the independent variable  $t$  does not occur explicitly. An ODE  $y' = f(t, y)$  in which  $t$  does not occur explicitly is of the form

$$(10) \quad y' = f(y)$$

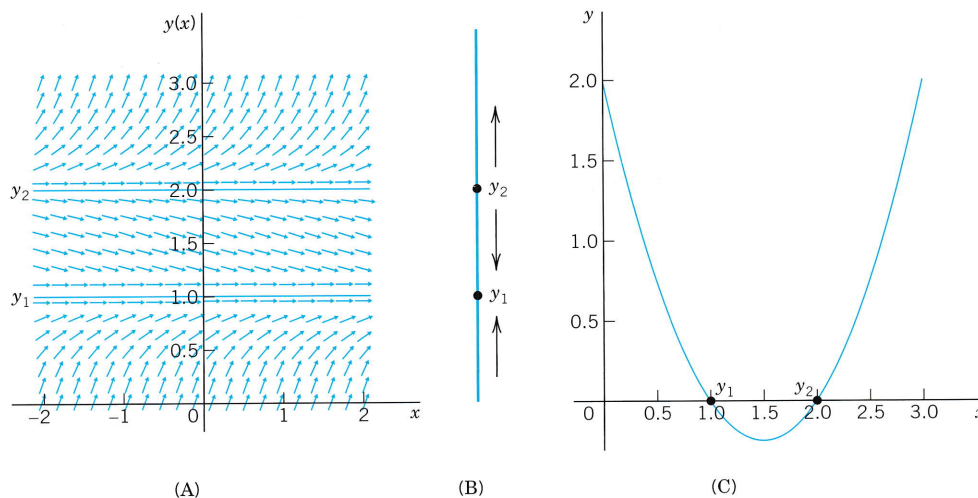
and is called an **autonomous ODE**. Thus the logistic equation (8) is autonomous.

Equation (10) has constant solutions, called **equilibrium solutions** or **equilibrium points**. These are determined by the zeros of  $f(y)$ , because  $f(y) = 0$  gives  $y' = 0$  by (10); hence  $y = \text{const}$ . These zeros are known as **critical points** of (10). An equilibrium solution is called **stable** if solutions close to it for some  $t$  remain close to it for all further  $t$ . It is called **unstable** if solutions initially close to it do not remain close to it as  $t$  increases. For instance,  $y = 0$  in Fig. 18 is an unstable equilibrium solution, and  $y = 4$  is a stable one.



**EXAMPLE 5** Stable and Unstable Equilibrium Solutions. “Phase Line Plot”

The ODE  $y' = (y - 1)(y - 2)$  has the stable equilibrium solution  $y_1 = 1$  and the unstable  $y_2 = 2$ , as the direction field in Fig. 19 suggests. The values  $y_1$  and  $y_2$  are the zeros of the parabola  $f(y) = (y - 1)(y - 2)$  in the figure. Now, since the ODE is autonomous, we can “condense” the direction field to a “phase line plot” giving  $y_1$  and  $y_2$ , and the direction (upward or downward) of the arrows in the field, and thus giving information about the stability or instability of the equilibrium solutions. ■



**Fig. 19.** Example 5. (A) Direction field. (B) “Phase line”. (C) Parabola  $f(y)$

A few further population models will be discussed in the problem set. For some more details of population dynamics, see C. W. Clark, *Mathematical Bioeconomics*, New York, Wiley, 1976.

Further important applications of linear ODEs follow in the next section.

**PROBLEM SET 1.5**

- (CAUTION!)** Show that  $e^{-\ln x} = 1/x$  (not  $-x$ ) and  $e^{-\ln(\sec x)} = \cos x$ .
- (Integration constant)** Give a reason why in (4) you may choose the constant of integration in  $\int p \, dx$  to be zero.

**3–17** GENERAL SOLUTION. INITIAL VALUE PROBLEMS

Find the general solution. If an initial condition is given, find also the corresponding particular solution and graph or sketch it. (Show the details of your work.)

- $y' + 3.5y = 2.8$
- $y' = 4y + x$
- $y' + 1.25y = 5, \quad y(0) = 6.6$
- $x^2y' + 3xy = 1/x, \quad y(1) = -1$
- $y' + ky = e^{2kx}$
- $y' + 2y = 4 \cos 2x, \quad y(\frac{1}{4}\pi) = 2$
- $y' = 6(y - 2.5) \tanh 1.5x$
- $y' + 4x^2y = (4x^2 - x)e^{-x^2/2}$
- $y' + 2y \sin 2x = 2e^{\cos 2x}, \quad y(0) = 0$
- $y' \tan x = 2y - 8, \quad y(\frac{1}{2}\pi) = 0$
- $y' + 4y \cot 2x = 6 \cos 2x, \quad y(\frac{1}{4}\pi) = 2$
- $y' + y \tan x = e^{-0.01x} \cos x, \quad y(0) = 0$
- $y' + y/x^2 = 2xe^{1/x}, \quad y(1) = 13.86$
- $y' \cos^2 x + 3y = 1, \quad y(\frac{1}{4}\pi) = \frac{4}{3}$
- $x^3y' + 3x^2y = 5 \sinh 10x$

**18–24** NONLINEAR ODEs

Using a method of this section or separating variables, find the general solution. If an initial condition is given, find also the particular solution and sketch or graph it.

18.  $y' + y = y^2$ ,  $y(0) = -1$
19.  $y' = 5.7y - 6.5y^2$
20.  $(x^2 + 1)y' = -\tan y$ ,  $y(0) = \frac{1}{2}\pi$
21.  $y' + (x + 1)y = e^{x^2}y^3$ ,  $y(0) = 0.5$
22.  $y' \sin 2y + x \cos 2y = 2x$
23.  $2yy' + y^2 \sin x = \sin x$ ,  $y(0) = \sqrt{2}$
24.  $y' + x^2y = (e^{-x^3} \sinh x)/(3y^2)$

**25–36** FURTHER APPLICATIONS

25. **(Investment programs)** Bill opens a retirement savings account with an initial amount  $y_0$  and then adds  $\$k$  to the account at the beginning of every year until retirement at age 65. Assume that the interest is compounded continuously at the same rate  $R$  over the years. Set up a model for the balance in the account and find the general solution as well as the particular solution, letting  $t = 0$  be the instant when the account is opened. How much money will Bill have in the account at age 65 if he starts at 25 and invests  $\$1000$  initially as well as annually, and the interest rate  $R$  is 6%? How much should he invest initially and annually (same amounts) to obtain the same final balance as before if he starts at age 45? First, guess.
26. **(Mixing problem)** A tank (as in Fig. 9 in Sec. 1.3) contains 1000 gal of water in which 200 lb of salt is dissolved. 50 gal of brine, each gallon containing  $(1 + \cos t)$  lb of dissolved salt, runs into the tank per minute. The mixture, kept uniform by stirring, runs out at the same rate. Find the amount of salt in the tank at any time  $t$  (Fig. 20).

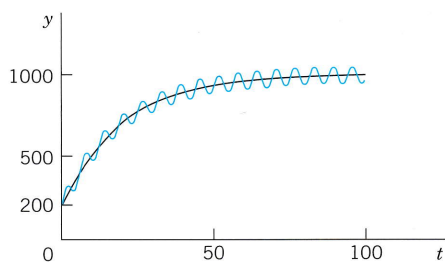


Fig. 20. Amount of salt  $y(t)$  in the tank in Problem 26

27. **(Lake Erie)** Lake Erie has a water volume of about  $450 \text{ km}^3$  and a flow rate (in and out) of about  $175 \text{ km}^3$  per year. If at some instant the lake has pollution concentration  $p = 0.04\%$ , how long, approximately, will it take to decrease it to  $p/2$ , assuming that the inflow is much cleaner, say, it has pollution

concentration  $p/4$ , and the mixture is uniform (an assumption that is only very imperfectly true)? First, guess.

28. **(Heating and cooling of a building)** Heating and cooling of a building can be modeled by the ODE

$$T' = k_1(T - T_a) + k_2(T - T_w) + P,$$

where  $T = T(t)$  is the temperature in the building at time  $t$ ,  $T_a$  the outside temperature,  $T_w$  the temperature wanted in the building, and  $P$  the rate of increase of  $T$  due to machines and people in the building, and  $k_1$  and  $k_2$  are (negative) constants. Solve this ODE, assuming  $P = \text{const}$ ,  $T_w = \text{const}$ , and  $T_a$  varying sinusoidally over 24 hours, say,  $T_a = A - C \cos(2\pi/24)t$ . Discuss the effect of each term of the equation on the solution.

29. **(Drug injection)** Find and solve the model for drug injection into the bloodstream if, beginning at  $t = 0$ , a constant amount  $A$  g/min is injected and the drug is simultaneously removed at a rate proportional to the amount of the drug present at time  $t$ .
30. **(Epidemics)** A model for the spread of contagious diseases is obtained by assuming that the rate of spread is proportional to the number of contacts between infected and noninfected persons, who are assumed to move freely among each other. Set up the model. Find the equilibrium solutions and indicate their stability or instability. Solve the ODE. Find the limit of the proportion of infected persons as  $t \rightarrow \infty$  and explain what it means.
31. **(Extinction vs. unlimited growth)** If in a population  $y(t)$  the death rate is proportional to the population, and the birth rate is proportional to the chance encounters of meeting mates for reproduction, what will the model be? Without solving, find out what will eventually happen to a small initial population. To a large one. Then solve the model.
32. **(Harvesting renewable resources. Fishing)** Suppose that the population  $y(t)$  of a certain kind of fish is given by the logistic equation (8), and fish are caught at a rate  $Hy$  proportional to  $y$ . Solve this so-called *Schaefer model*. Find the equilibrium solutions  $y_1$  and  $y_2$  ( $> 0$ ) when  $H < A$ . The expression  $Y = Hy_2$  is called the **equilibrium harvest** or **sustainable yield** corresponding to  $H$ . Why?
33. **(Harvesting)** In Prob. 32 find and graph the solution satisfying  $y(0) = 2$  when (for simplicity)  $A = B = 1$  and  $H = 0.2$ . What is the limit? What does it mean? What if there were no fishing?
34. **(Intermittent harvesting)** In Prob. 32 assume that you fish for 3 years, then fishing is banned for the next 3 years. Thereafter you start again. And so on. This is called *intermittent harvesting*. Describe qualitatively how the population will develop if intermitting is

continued periodically. Find and graph the solution for the first 9 years, assuming that  $A = B = 1$ ,  $H = 0.2$ , and  $y(0) = 2$ .

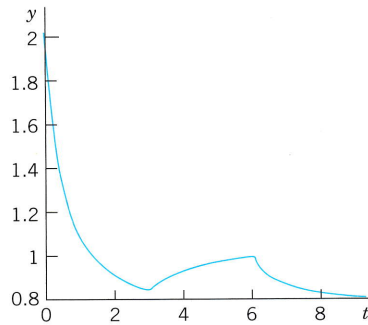


Fig. 21. Fish population in Problem 34

35. (**Harvesting**) If a population of mice (in multiples of 1000) follows the logistic law with  $A = 1$  and  $B = 0.25$ , and if owls catch at a time rate of 10% of the population present, what is the model, its equilibrium harvest for that catch, and its solution?
36. (**Harvesting**) Do you save work in Prob. 34 if you first transform the ODE to a linear ODE? Do this transformation. Solve the resulting ODE. Does the resulting  $y(t)$  agree with that in Prob. 34?

### 37–40 GENERAL PROPERTIES OF LINEAR ODEs

These properties are of practical and theoretical importance because they enable us to obtain new solutions from given ones. Thus in modeling, whenever possible, we prefer linear ODEs over nonlinear ones, which have no similar properties.

Show that nonhomogeneous linear ODEs (1) and homogeneous linear ODEs (2) have the following properties. Illustrate each property by a calculation for two or three equations of your choice. Give proofs.

37. The sum  $y_1 + y_2$  of two solutions  $y_1$  and  $y_2$  of the homogeneous equation (2) is a solution of (2), and so is a scalar multiple  $ay_1$  for any constant  $a$ . These properties are not true for (1)!
38.  $y = 0$  (that is,  $y(x) = 0$  for all  $x$ , also written  $y(x) \equiv 0$ ) is a solution of (2) [not of (1) if  $r(x) \neq 0$ !], called the **trivial solution**.
39. The sum of a solution of (1) and a solution of (2) is a solution of (1).
40. The difference of two solutions of (1) is a solution of (2).
41. If  $y_1$  is a solution of (1), what can you say about  $cy_1$ ?
42. If  $y_1$  and  $y_2$  are solutions of  $y_1' + py_1 = r_1$  and  $y_2' + py_2 = r_2$ , respectively (with the same  $p$ !), what can you say about the sum  $y_1 + y_2$ ?

43. **CAS EXPERIMENT.** (a) Solve the ODE  $y' - y/x = -x^{-1} \cos(1/x)$ . Find an initial condition for which the arbitrary constant is zero. Graph the resulting particular solution, experimenting to obtain a good figure near  $x = 0$ .

(b) Generalizing (a) from  $n = 1$  to arbitrary  $n$ , solve the ODE  $y' - ny/x = -x^{n-2} \cos(1/x)$ . Find an initial condition as in (a), and experiment with the graph.

44. **TEAM PROJECT. Riccati Equation, Clairaut Equation.** A **Riccati equation** is of the form

$$(11) \quad y' + p(x)y = g(x)y^2 + h(x).$$

A **Clairaut equation** is of the form

$$(12) \quad y = xy' + g(y').$$

(a) Apply the transformation  $y = Y + 1/u$  to the Riccati equation (11), where  $Y$  is a solution of (11), and obtain for  $u$  the linear ODE  $u' + (2Yg - p)u = -g$ . Explain the effect of the transformation by writing it as  $y = Y + v$ ,  $v = 1/u$ .

(b) Show that  $y = Y = x$  is a solution of  $y' - (2x^3 + 1)y = -x^2y^2 - x^4 - x + 1$  and solve this Riccati equation, showing the details.

(c) Solve  $y' + (3 - 2x^2 \sin x)y = -y^2 \sin x + 2x + 3x^2 - x^4 \sin x$ , using (and verifying) that  $y = x^2$  is a solution.

(d) By working “backward” from the  $u$ -equation find further Riccati equations that have relatively simple solutions.

(e) Solve the Clairaut equation  $y = xy' + 1/y'$ . *Hint.* Differentiate this ODE with respect to  $x$ .

(f) Solve the Clairaut equation  $y'^2 - xy' + y = 0$  in Prob. 16 of Problem Set 1.1.

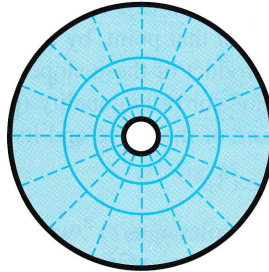
(g) Show that the Clairaut equation (12) has as solutions a family of straight lines  $y = cx + g(c)$  and a singular solution determined by  $g'(s) = -x$ , where  $s = y'$ , that forms the envelope of that family.

45. (**Variation of parameter**) Another method of obtaining (4) results from the following idea. Write (3) as  $cy^*$ , where  $y^*$  is the exponential function, which is a solution of the homogeneous linear ODE  $y^{*'} + py^* = 0$ . Replace the arbitrary constant  $c$  in (3) with a function  $u$  to be determined so that the resulting function  $y = uy^*$  is a solution of the nonhomogeneous linear ODE  $y' + py = r$ .

46. **TEAM PROJECT. Transformations of ODEs.** We have transformed ODEs to separable form, to exact form, and to linear form. The purpose of such transformations is an extension of solution methods to larger classes of ODEs. Describe the key idea of each of these transformations and give three typical examples of your choice for each transformation, showing each step (not just the transformed ODE).

## 1.6 Orthogonal Trajectories. *Optional*

An important type of problem in physics or geometry is to find a family of curves that intersect a given family of curves at right angles. The new curves are called **orthogonal trajectories** of the given curves (and conversely). Examples are curves of equal temperature (*isotherms*) and curves of heat flow, curves of equal altitude (*contour lines*) on a map and curves of steepest descent on that map, curves of equal potential (*equipotential curves*, curves of equal voltage—the concentric circles in Fig. 22), and curves of electric force (the straight radial segments in Fig. 22).



**Fig. 22.** Equipotential lines and curves of electric force (dashed) between two concentric (black) circles (cylinders in space)

Here the **angle of intersection** between two curves is defined to be the angle between the tangents of the curves at the intersection point. *Orthogonal* is another word for *perpendicular*.

In many cases orthogonal trajectories can be found by using ODEs, as follows. Let

$$(1) \quad G(x, y, c) = 0$$

be a given family of curves in the  $xy$ -plane, where each curve is specified by some value of  $c$ . This is called a **one-parameter family of curves**, and  $c$  is called the *parameter* of the family. For instance, a one-parameter family of quadratic parabolas is given by (Fig. 23)

$$y = cx^2 \quad \text{or, written as in (1),} \quad G(x, y, c) = y - cx^2 = 0.$$

**Step 1.** Find an ODE for which the given family is a general solution. Of course, this ODE must no longer contain the parameter  $c$ . In our example we solve algebraically for  $c$  and then differentiate and simplify; thus,

$$\frac{y}{x^2} = c, \quad \frac{y'x^2 - 2xy}{x^4} = 0,$$

hence

$$y' = \frac{2y}{x}.$$

The last of these equations is the ODE of the given family of curves. It is of the form

$$(2) \quad y' = f(x, y).$$

**Step 2.** Write down the ODE of the orthogonal trajectories, that is, the ODE whose general solution gives the orthogonal trajectories of the given curves. This ODE is

$$(3) \quad \tilde{y}' = -\frac{1}{f(x, \tilde{y})}$$

with the same  $f$  as in (2). Why? Well, a given curve passing through a point  $(x_0, y_0)$  has slope  $f(x_0, y_0)$  at that point, by (2). The trajectory through  $(x_0, y_0)$  has slope  $-1/f(x_0, y_0)$  by (3). The product of these slopes is  $-1$ , as we see. From calculus it is known that this is the condition for orthogonality (perpendicularity) of two straight lines (the tangents at  $(x_0, y_0)$ ), hence of the curve and its orthogonal trajectory at  $(x_0, y_0)$ .

**Step 3.** Solve (3).

For our parabolas  $y = cx^2$  we have  $y' = 2y/x$ . Hence their orthogonal trajectories are obtained from  $\tilde{y}' = -x/2\tilde{y}$  or  $2\tilde{y}\tilde{y}' + x = 0$ . By integration,  $\tilde{y}^2 + \frac{1}{2}x^2 = c^*$ . These are the ellipses in Fig. 23 with semi-axes  $\sqrt{2c^*}$  and  $\sqrt{c^*}$ . Here,  $c^* > 0$  because  $c^* = 0$  gives just the origin, and  $c^* < 0$  gives no real solution at all.

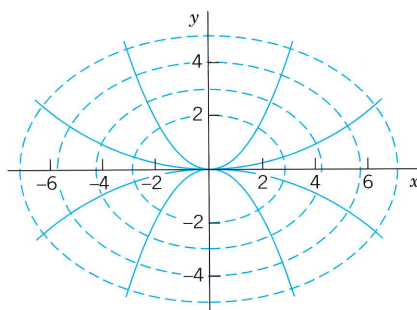


Fig. 23. Parabolas and orthogonal trajectories (ellipses) in the text

## PROBLEM SET 1.6

### 1–12 ORTHOGONAL TRAJECTORIES

Sketch or graph some of the given curves. Guess what their orthogonal trajectories may look like. Find these trajectories.

(Show the details of your work.)

1.  $y = 4x + c$
2.  $y = c/x$
3.  $y = cx$
4.  $y^2 = 2x^2 + c$
5.  $x^2y = c$
6.  $y = ce^{-3x}$

$$7. y = ce^{x^2/2}$$

$$9. 4x^2 + y^2 = c$$

$$11. x = ce^{y/4}$$

$$8. x^2 - y^2 = c$$

$$10. x = c\sqrt{y}$$

$$12. x^2 + (y - c)^2 = c^2$$

### 13–15 OTHER FORMS OF THE ODES (2) AND (3)

13. (**y as independent variable**) Show that (3) may be written  $dx/d\tilde{y} = -f(x, \tilde{y})$ . Use this form to find the orthogonal trajectories of  $y = 2x + ce^{-x}$ .

14. **(Family  $g(x, y) = c$ )** Show that if a family is given as  $g(x, y) = c$ , then the orthogonal trajectories can be obtained from the following ODE, and use the latter to solve Prob. 6 written in the form  $g(x, y) = c$ .

$$\frac{d\tilde{y}}{dx} = \frac{\partial g/\partial \tilde{y}}{\partial g/\partial x}$$

15. **(Cauchy–Riemann equations)** Show that for a family  $u(x, y) = c = \text{const}$  the orthogonal trajectories  $v(x, y) = c^* = \text{const}$  can be obtained from the following *Cauchy–Riemann equations* (which are basic in complex analysis in Chap. 13) and use them to find the orthogonal trajectories of  $e^x \sin y = \text{const}$ . (Here, subscripts denote partial derivatives.)

$$u_x = v_y, \quad u_y = -v_x$$

**16–20 APPLICATIONS**

16. **(Fluid flow)** Suppose that the *streamlines* of the flow (paths of the particles of the fluid) in Fig. 24 are  $\Psi(x, y) = xy = \text{const}$ . Find their orthogonal trajectories (called **equipotential lines**, for reasons given in Sec. 18.4).

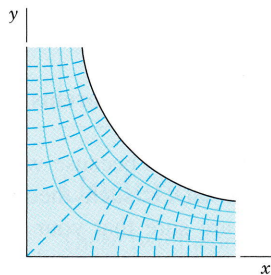


Fig. 24. Flow in a channel in Problem 16

17. **(Electric field)** Let the electric equipotential lines (curves of constant potential) between two concentric cylinders (Fig. 22) be given by  $u(x, y) = x^2 + y^2 = c$ . Use the method in the text to find their orthogonal trajectories (the curves of electric force).

18. **(Electric field)** The lines of electric force of two opposite charges of the same strength at  $(-1, 0)$  and  $(1, 0)$  are the circles through  $(-1, 0)$  and  $(1, 0)$ . Show that these circles are given by  $x^2 + (y - c)^2 = 1 + c^2$ . Show that the **equipotential lines** (orthogonal trajectories of those circles) are the circles given by  $(x + c^*)^2 + \tilde{y}^2 = c^{*2} - 1$  (dashed in Fig. 25).

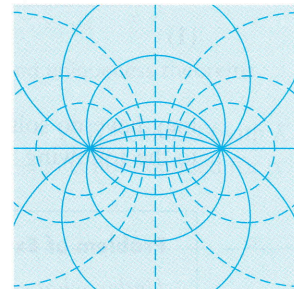


Fig. 25. Electric field in Problem 18

19. **(Temperature field)** Let the **isotherms** (curves of constant temperature) in a body in the upper half-plane  $y > 0$  be given by  $4x^2 + 9y^2 = c$ . Find the orthogonal trajectories (the curves along which heat will flow in regions filled with heat-conducting material and free of heat sources or heat sinks).

20. **TEAM PROJECT. Conic Sections.** (A) State the main steps of the present method of obtaining orthogonal trajectories.

(B) Find conditions under which the orthogonal trajectories of families of ellipses  $x^2/a^2 + y^2/b^2 = c$  are again conic sections. Illustrate your result graphically by sketches or by using your CAS. What happens if  $a \rightarrow 0$ ? If  $b \rightarrow 0$ ?

(C) Investigate families of hyperbolas  $x^2/a^2 - y^2/b^2 = c$  in a similar fashion.

(D) Can you find more complicated curves for which you get ODEs that you can solve? Give it a try.

## 1.7 Existence and Uniqueness of Solutions

The initial value problem

$$|y'| + |y| = 0, \quad y(0) = 1$$

has no solution because  $y = 0$  (that is,  $y(x) = 0$  for all  $x$ ) is the only solution of the ODE. The initial value problem

$$y' = 2x, \quad y(0) = 1$$

has precisely one solution, namely,  $y = x^2 + 1$ . The initial value problem

$$xy' = y - 1, \quad y(0) = 1$$

has infinitely many solutions, namely,  $y = 1 + cx$ , where  $c$  is an arbitrary constant because  $y(0) = 1$  for all  $c$ .

From these examples we see that an **initial value problem**

$$(1) \quad y' = f(x, y), \quad y(x_0) = y_0$$

may have no solution, precisely one solution, or more than one solution. This fact leads to the following two fundamental questions.

#### Problem of Existence

*Under what conditions does an initial value problem of the form (1) have at least one solution (hence one or several solutions)?*

#### Problem of Uniqueness

*Under what conditions does that problem have at most one solution (hence excluding the case that it has more than one solution)?*

Theorems that state such conditions are called **existence theorems** and **uniqueness theorems**, respectively.

Of course, for our simple examples we need no theorems because we can solve these examples by inspection; however, for complicated ODEs such theorems may be of considerable practical importance. Even when you are sure that your physical or other system behaves uniquely, occasionally your model may be oversimplified and may not give a faithful picture of the reality.

### THEOREM 1

#### Existence Theorem

Let the right side  $f(x, y)$  of the ODE in the initial value problem

$$(1) \quad y' = f(x, y), \quad y(x_0) = y_0$$

be continuous at all points  $(x, y)$  in some rectangle

$$R: |x - x_0| < a, \quad |y - y_0| < b \quad (\text{Fig. 26})$$

and **bounded** in  $R$ ; that is, there is a number  $K$  such that

$$(2) \quad |f(x, y)| \leq K \quad \text{for all } (x, y) \text{ in } R.$$

Then the initial value problem (1) has at least one solution  $y(x)$ . This solution exists at least for all  $x$  in the subinterval  $|x - x_0| < \alpha$  of the interval  $|x - x_0| < a$ ; here,  $\alpha$  is the smaller of the two numbers  $a$  and  $b/K$ .

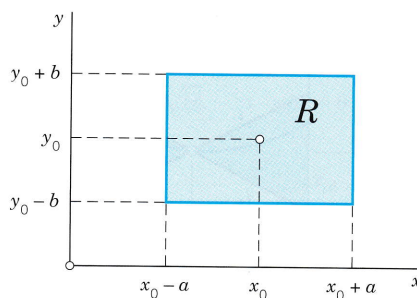


Fig. 26. Rectangle  $R$  in the existence and uniqueness theorems

(Example of Boundedness. The function  $f(x, y) = x^2 + y^2$  is bounded (with  $K = 2$ ) in the square  $|x| < 1$ ,  $|y| < 1$ . The function  $f(x, y) = \tan(x + y)$  is not bounded for  $|x + y| < \pi/2$ . Explain!)

## THEOREM 2

### Uniqueness Theorem

Let  $f$  and its partial derivative  $f_y = \partial f / \partial y$  be continuous for all  $(x, y)$  in the rectangle  $R$  (Fig. 26) and bounded, say,

$$(3) \quad (a) \quad |f(x, y)| \leq K, \quad (b) \quad |f_y(x, y)| \leq M \quad \text{for all } (x, y) \text{ in } R.$$

Then the initial value problem (1) has at most one solution  $y(x)$ . Thus, by Theorem 1, the problem has precisely one solution. This solution exists at least for all  $x$  in that subinterval  $|x - x_0| < \alpha$ .

## Understanding These Theorems

These two theorems take care of almost all practical cases. Theorem 1 says that if  $f(x, y)$  is continuous in some region in the  $xy$ -plane containing the point  $(x_0, y_0)$ , then the initial value problem (1) has at least one solution.

Theorem 2 says that if, moreover, the partial derivative  $\partial f / \partial y$  of  $f$  with respect to  $y$  exists and is continuous in that region, then (1) can have at most one solution; hence, by Theorem 1, it has precisely one solution.

Read again what you have just read—these are entirely new ideas in our discussion.

Proofs of these theorems are beyond the level of this book (see Ref. [A11] in App. 1); however, the following remarks and examples may help you to a good understanding of the theorems.

Since  $y' = f(x, y)$ , the condition (2) implies that  $|y'| \leq K$ ; that is, the slope of any solution curve  $y(x)$  in  $R$  is at least  $-K$  and at most  $K$ . Hence a solution curve that passes through the point  $(x_0, y_0)$  must lie in the colored region in Fig. 27 on the next page bounded by the lines  $l_1$  and  $l_2$  whose slopes are  $-K$  and  $K$ , respectively. Depending on the form of  $R$ , two different cases may arise. In the first case, shown in Fig. 27a, we have  $b/K \geq a$  and therefore  $\alpha = a$  in the existence theorem, which then asserts that the solution exists for all  $x$  between  $x_0 - a$  and  $x_0 + a$ . In the second case, shown in Fig. 27b, we have  $b/K < a$ . Therefore,  $\alpha = b/K < a$ , and all we can conclude from the theorems is that the solution exists for all  $x$  between  $x_0 - b/K$  and  $x_0 + b/K$ . For larger or smaller  $x$ 's the solution curve may leave the rectangle  $R$ , and since nothing is assumed about  $f$  outside  $R$ , nothing can be concluded about the solution for those larger or smaller  $x$ 's; that is, for such  $x$ 's the solution may or may not exist—we don't know.



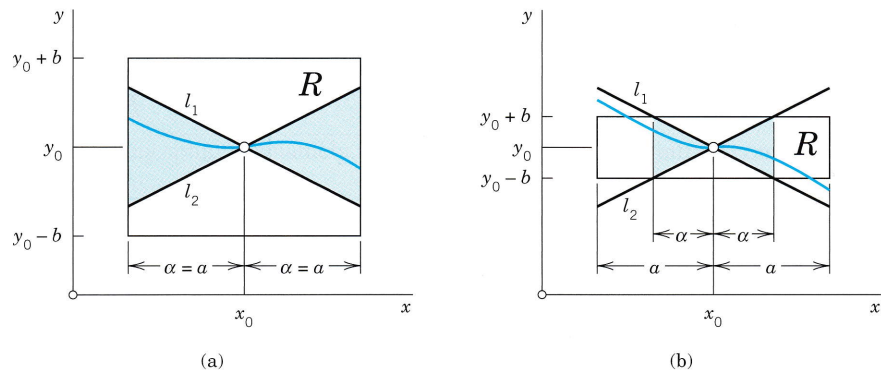


Fig. 27. The condition (2) of the existence theorem. (a) First case. (b) Second case

Let us illustrate our discussion with a simple example. We shall see that our choice of a rectangle  $R$  with a large base (a long  $x$ -interval) will lead to the case in Fig. 27b.

### EXAMPLE 1 Choice of a Rectangle

Consider the initial value problem

$$y' = 1 + y^2, \quad y(0) = 0$$

and take the rectangle  $R$ ;  $|x| < 5$ ,  $|y| < 3$ . Then  $a = 5$ ,  $b = 3$ , and

$$|f(x, y)| = |1 + y^2| \leq K = 10,$$

$$\left| \frac{\partial f}{\partial y} \right| = 2|y| \leq M = 6,$$

$$\alpha = \frac{b}{K} = 0.3 < a.$$

Indeed, the solution of the problem is  $y = \tan x$  (see Sec. 1.3, Example 1). This solution is discontinuous at  $\pm \pi/2$ , and there is no *continuous* solution valid in the entire interval  $|x| < 5$  from which we started. ■

The conditions in the two theorems are sufficient conditions rather than necessary ones, and can be lessened. In particular, by the mean value theorem of differential calculus we have

$$f(x, y_2) - f(x, y_1) = (y_2 - y_1) \frac{\partial f}{\partial y} \Big|_{y=\tilde{y}}$$

where  $(x, y_1)$  and  $(x, y_2)$  are assumed to be in  $R$ , and  $\tilde{y}$  is a suitable value between  $y_1$  and  $y_2$ . From this and (3b) it follows that

$$(4) \quad |f(x, y_2) - f(x, y_1)| \leq M|y_2 - y_1|.$$

It can be shown that (3b) may be replaced by the weaker condition (4), which is known as a **Lipschitz condition**.<sup>7</sup> However, continuity of  $f(x, y)$  is not enough to guarantee the *uniqueness* of the solution. This may be illustrated by the following example.

**EXAMPLE 2** Nonuniqueness

The initial value problem

$$y' = \sqrt{|y|}, \quad y(0) = 0$$

has the two solutions

$$y \equiv 0 \quad \text{and} \quad y^* = \begin{cases} x^2/4 & \text{if } x \geq 0 \\ -x^2/4 & \text{if } x < 0 \end{cases}$$

although  $f(x, y) = \sqrt{|y|}$  is continuous for all  $y$ . The Lipschitz condition (4) is violated in any region that includes the line  $y = 0$ , because for  $y_1 = 0$  and positive  $y_2$  we have

$$(5) \quad \frac{|f(x, y_2) - f(x, y_1)|}{|y_2 - y_1|} = \frac{\sqrt{y_2}}{y_2} = \frac{1}{\sqrt{y_2}}, \quad (\sqrt{y_2} > 0)$$

and this can be made as large as we please by choosing  $y_2$  sufficiently small, whereas (4) requires that the quotient on the left side of (5) should not exceed a fixed constant  $M$ . ■

**PROBLEM SET 1.7**

- (Vertical strip)** If the assumptions of Theorems 1 and 2 are satisfied not merely in a rectangle but in a vertical infinite strip  $|x - x_0| < a$ , in what interval will the solution of (1) exist?
- (Existence?)** Does the initial value problem  $(x - 1)y' = 2y$ ,  $y(1) = 1$  have a solution? Does your result contradict our present theorems?
- (Common points)** Can two solution curves of the same ODE have a common point in a rectangle in which the assumptions of the present theorems are satisfied?
- (Change of initial condition)** What happens in Prob. 2 if you replace  $y(1) = 1$  with  $y(1) = k$ ?
- (Linear ODE)** If  $p$  and  $r$  in  $y' + p(x)y = r(x)$  are continuous for all  $x$  in an interval  $|x - x_0| \leq a$ , show that  $f(x, y)$  in this ODE satisfies the conditions of our present theorems, so that a corresponding initial value problem has a unique solution. Do you actually need these theorems for this ODE?
- (Three possible cases)** Find all initial conditions such that  $(x^2 - 4x)y' = (2x - 4)y$  has no solution, precisely one solution, and more than one solution.
- (Length of  $x$ -interval)** In most cases the solution of an initial value problem (1) exists in an  $x$ -interval larger than that guaranteed by the present theorems. Show this fact for  $y' = 2y^2$ ,  $y(1) = 1$  by finding the best possible  $\alpha$  (choosing  $b$  optimally) and comparing the result with the actual solution.
- PROJECT. Lipschitz Condition.** (A) State the definition of a Lipschitz condition. Explain its relation to the existence of a partial derivative. Explain its significance in our present context. Illustrate your statements by examples of your own.  
  
(B) Show that for a *linear* ODE  $y' + p(x)y = r(x)$  with continuous  $p$  and  $r$  in  $|x - x_0| \leq a$  a Lipschitz condition holds. This is remarkable because it means that for a *linear* ODE the continuity of  $f(x, y)$  guarantees not only the existence but also the uniqueness of the solution of an initial value problem. (Of course, this also follows directly from (4) in Sec. 1.5.)  
  
(C) Discuss the uniqueness of solution for a few simple ODEs that you can solve by one of the methods considered, and find whether a Lipschitz condition is satisfied.
- (Maximum  $\alpha$ )** What is the largest possible  $\alpha$  in Example 1 in the text?
- CAS PROJECT. Picard Iteration.** (A) Show that by integrating the ODE in (1) and observing the initial condition you obtain
 
$$(6) \quad y(x) = y_0 + \int_{x_0}^x f(t, y(t)) dt.$$

<sup>7</sup>RUDOLF LIPSCHITZ (1832–1903), German mathematician. Lipschitz and similar conditions are important in modern theories, for instance, in partial differential equations.

This form (6) of (1) suggests **Picard's iteration method**<sup>8</sup>, which is defined by

$$(7) \quad y_n(x) = y_0 + \int_{x_0}^x f(t, y_{n-1}(t)) dt, \quad n = 1, 2, \dots$$

It gives approximations  $y_1, y_2, y_3, \dots$  of the unknown solution  $y$  of (1). Indeed, you obtain  $y_1$  by substituting  $y = y_0$  on the right and integrating—this is the first step—, then  $y_2$  by substituting  $y = y_1$  on the right and integrating—this is the second step—, and so on. Write a program of the iteration that gives a printout of the first approximations  $y_0, y_1, \dots, y_N$  as well as their graphs on common axes. Try your program on two initial value problems of your own choice.

(B) Apply the iteration to  $y' = x + y, y(0) = 0$ . Also solve the problem exactly.

(C) Apply the iteration to  $y' = 2y^2, y(0) = 1$ . Also solve the problem exactly.

(D) Find all solutions of  $y' = 2\sqrt{y}, y(1) = 0$ . Which of them does Picard's iteration approximate?

(E) Experiment with the conjecture that Picard's iteration converges to the solution of the problem for any initial choice of  $y$  in the integrand in (7) (leaving  $y_0$  outside the integral as it is). Begin with a simple ODE and see what happens. When you are reasonably sure, take a slightly more complicated ODE and give it a try.

## CHAPTER 1 REVIEW QUESTIONS AND PROBLEMS

1. Explain the terms *ordinary differential equation (ODE)*, *partial differential equation (PDE)*, *order*, *general solution*, and *particular solution*. Give examples. Why are these concepts of importance?
2. What is an initial condition? How is this condition used in an initial value problem?
3. What is a homogeneous linear ODE? A nonhomogeneous linear ODE? Why are these equations simpler than nonlinear ODEs?
4. What do you know about direction fields and their practical importance?
5. Give examples of mechanical problems that lead to ODEs.
6. Why do electric circuits lead to ODEs?
7. Make a list of the solution methods considered. Explain each method with a few short sentences and illustrate it by a typical example.
8. Can certain ODEs be solved by more than one method? Give three examples.
9. What are integrating factors? Explain the idea. Give examples.
10. Does every first-order ODE have a solution? A general solution? What do you know about uniqueness of solutions?

### 11–14 DIRECTION FIELDS

Graph a direction field (by a CAS or by hand) and sketch some of the solution curves. Solve the ODE exactly and compare.

11.  $y' = 1 + 4y^2$

12.  $y' = 3y - 2x$

13.  $y' = 4y - y^2$

14.  $y' = 16x/y$

### 15–26 GENERAL SOLUTION

Find the general solution. Indicate which method in this chapter you are using. Show the details of your work.

15.  $y' = x^2(1 + y^2)$

16.  $y' = x(y - x^2 + 1)$

17.  $yy' + xy^2 = x$

18.  $-\pi \sin \pi x \cosh 3y dx + 3 \cos \pi x \sinh 3y dy = 0$

19.  $y' + y \sin x = \sin x$

20.  $y' - y = 1/y$

21.  $3 \sin 2y dx + 2x \cos 2y dy = 0$

22.  $xy' = x \tan(y/x) + y$

23.  $(y \cos xy - 2x) dx + (x \cos xy + 2y) dy = 0$

24.  $xy' = (y - 2x)^2 + y$  (Set  $y - 2x = z$ .)

25.  $\sin(y - x) dx + [\cos(y - x) - \sin(y - x)] dy = 0$

26.  $xy' = (y/x)^3 + y$

### 27–32 INITIAL VALUE PROBLEMS

Solve the following initial value problems. Indicate the method used. Show the details of your work.

27.  $yy' + x = 0, y(3) = 4$

28.  $y' - 3y = -12y^2, y(0) = 2$

29.  $y' = 1 + y^2, y(\frac{1}{4}\pi) = 0$

30.  $y' + \pi y = 2b \cos \pi x, y(0) = 0$

31.  $(2xy^2 - \sin x) dx + (2 + 2x^2y) dy = 0, y(0) = 1$

32.  $[2y + y^2/x + e^x(1 + 1/x)] dx + (x + 2y) dy = 0, y(1) = 1$

<sup>8</sup>EMILE PICARD (1856–1941), French mathematician, also known for his important contributions to complex analysis (see Sec. 16.2 for his famous theorem). Picard used his method to prove Theorems 1 and 2 as well as the convergence of the sequence (7) to the solution of (1). In precomputer times the iteration was of little *practical* value because of the integrations.

## 33–43 APPLICATIONS, MODELING

33. **(Heat flow)** If the isotherms in a region are  $x^2 - y^2 = c$ , what are the curves of heat flow (assuming orthogonality)?
34. **(Law of cooling)** A thermometer showing  $10^\circ\text{C}$  is brought into a room whose temperature is  $25^\circ\text{C}$ . After 5 minutes it shows  $20^\circ\text{C}$ . When will the thermometer practically reach the room temperature, say,  $24.9^\circ\text{C}$ ?
35. **(Half-life)** If 10% of a radioactive substance disintegrates in 4 days, what is its half-life?
36. **(Half-life)** What is the half-life of a substance if after 5 days, 0.020 g is present and after 10 days, 0.015 g?
37. **(Half-life)** When will 99% of the substance in Prob. 35 have disintegrated?
38. **(Air circulation)** In a room containing 20 000 ft<sup>3</sup> of air, 600 ft<sup>3</sup> of fresh air flows in per minute, and the mixture (made practically uniform by circulating fans) is exhausted at a rate of 600 cubic feet per minute (cfm). What is the amount of fresh air  $y(t)$  at any time if  $y(0) = 0$ ? After what time will 90% of the air be fresh?
39. **(Electric field)** If the equipotential lines in a region of the  $xy$ -plane are  $4x^2 + y^2 = c$ , what are the curves of the electrical force? Sketch both families of curves.
40. **(Chemistry)** In a bimolecular reaction  $A + B \rightarrow M$ ,  $a$  moles per liter of a substance  $A$  and  $b$  moles per liter of a substance  $B$  are combined. Under constant temperature the rate of reaction is
- $$y' = k(a - y)(b - y) \quad \text{(Law of mass action);}$$
- that is,  $y'$  is proportional to the product of the concentrations of the substances that are reacting, where  $y(t)$  is the number of moles per liter which have reacted after time  $t$ . Solve this ODE, assuming that  $a \neq b$ .
41. **(Population)** Find the population  $y(t)$  if the birth rate is proportional to  $y(t)$  and the death rate is proportional to the square of  $y(t)$ .
42. **(Curves)** Find all curves in the first quadrant of the  $xy$ -plane such that for every tangent, the segment between the coordinate axes is bisected by the point of tangency. (Make a sketch.)
43. **(Optics) Lambert's law of absorption**<sup>9</sup> states that the absorption of light in a thin transparent layer is proportional to the thickness of the layer and to the amount of light incident on that layer. Formulate this law as an ODE and solve it.

## SUMMARY OF CHAPTER 1

## First-Order ODEs

This chapter concerns **ordinary differential equations (ODEs) of first order** and their applications. These are equations of the form

$$(1) \quad F(x, y, y') = 0 \quad \text{or in explicit form} \quad y' = f(x, y)$$

involving the derivative  $y' = dy/dx$  of an unknown function  $y$ , given functions of  $x$ , and, perhaps,  $y$  itself. If the independent variable  $x$  is time, we denote it by  $t$ .

In Sec. 1.1 we explained the basic concepts and the process of **modeling**, that is, of expressing a physical or other problem in some mathematical form and solving it. Then we discussed the method of direction fields (Sec. 1.2), solution methods and models (Secs. 1.3–1.6), and, finally, ideas on existence and uniqueness of solutions (Sec. 1.7).

<sup>9</sup>JOHANN HEINRICH LAMBERT (1728–1777), German physicist and mathematician.

A first-order ODE usually has a **general solution**, that is, a solution involving an arbitrary constant, which we denote by  $c$ . In applications we usually have to find a unique solution by determining a value of  $c$  from an **initial condition**  $y(x_0) = y_0$ . Together with the ODE this is called an **initial value problem**

$$(2) \quad y' = f(x, y), \quad y(x_0) = y_0 \quad (x_0, y_0 \text{ given numbers})$$

and its solution is a **particular solution** of the ODE. Geometrically, a general solution represents a family of curves, which can be graphed by using **direction fields** (Sec. 1.2). And each particular solution corresponds to one of these curves.

A **separable ODE** is one that we can put into the form

$$(3) \quad g(y) dy = f(x) dx \quad (\text{Sec. 1.3})$$

by algebraic manipulations (possibly combined with transformations, such as  $y/x = u$ ) and solve by integrating on both sides.

An **exact ODE** is of the form

$$(4) \quad M(x, y) dx + N(x, y) dy = 0 \quad (\text{Sec. 1.4})$$

where  $M dx + N dy$  is the **differential**

$$du = u_x dx + u_y dy$$

of a function  $u(x, y)$ , so that from  $du = 0$  we immediately get the implicit general solution  $u(x, y) = c$ . This method extends to nonexact ODEs that can be made exact by multiplying them by some function  $F(x, y)$ , called an **integrating factor** (Sec. 1.4).

**Linear ODEs**

$$(5) \quad y' + p(x)y = r(x)$$

are very important. Their solutions are given by the integral formula (4), Sec. 1.5. Certain nonlinear ODEs can be transformed to linear form in terms of new variables. This holds for the **Bernoulli equation**

$$y' + p(x)y = g(x)y^a \quad (\text{Sec. 1.5}).$$

**Applications and modeling** are discussed throughout the chapter, in particular in Secs. 1.1, 1.3, 1.5 (**population dynamics**, etc.), and 1.6 (**trajectories**).

Picard's **existence and uniqueness theorems** are explained in Sec. 1.7 (and *Picard's iteration* in Problem Set 1.7).

**Numeric methods** for first-order ODEs can be studied in Secs. 21.1 and 21.2 immediately after this chapter, as indicated in the chapter opening.

## Second-Order Linear ODEs

Ordinary differential equations (ODEs) may be divided into two large classes, **linear ODEs** and **nonlinear ODEs**. Whereas nonlinear ODEs of second (and higher) order generally are difficult to solve, linear ODEs are much simpler because various properties of their solutions can be characterized in a general way, and there are standard methods for solving many of these equations.

Linear ODEs *of the second order* are the most important ones because of their applications in mechanical and electrical engineering (Secs. 2.4, 2.8, 2.9). And their theory is typical of that of all linear ODEs, but the formulas are simpler than for higher order equations. Also the transition to higher order (in Chap. 3) will be almost immediate.

This chapter includes the derivation of general and particular solutions, the latter in connection with initial value problems.

(Boundary value problems follow in Chap. 5, which also contains solution methods for Legendre's, Bessel's, and the hypergeometric equations.)

**COMMENT.** *Numerics for second-order ODEs can be studied immediately after this chapter.* See Sec. 21.3, which is independent of other sections in Chaps. 19–21.

*Prerequisite:* Chap. 1, in particular, Sec. 1.5.

*Sections that may be omitted in a shorter course:* 2.3, 2.9, 2.10.

*References and Answers to Problems:* App. 1 Part A, and App. 2.

### 2.1 Homogeneous Linear ODEs of Second Order

We have already considered first-order linear ODEs (Sec. 1.5) and shall now define and discuss linear ODEs of second order. These equations have important engineering applications, especially in connection with mechanical and electrical vibrations (Secs. 2.4, 2.8, 2.9) as well as in wave motion, heat conduction, and other parts of physics, as we shall see in Chap. 12.

A second-order ODE is called **linear** if it can be written

$$(1) \quad y'' + p(x)y' + q(x)y = r(x)$$

and **nonlinear** if it cannot be written in this form.

The distinctive feature of this equation is that it is *linear in  $y$  and its derivatives*, whereas the functions  $p$ ,  $q$ , and  $r$  on the right may be any given functions of  $x$ . If the equation begins with, say,  $f(x)y''$ , then divide by  $f(x)$  to have the **standard form** (1) with  $y''$  as the first term, which is practical.

If  $r(x) \equiv 0$  (that is,  $r(x) = 0$  for all  $x$  considered; read “ $r(x)$  is identically zero”), then (1) reduces to

$$(2) \quad y'' + p(x)y' + q(x)y = 0$$

and is called **homogeneous**. If  $r(x) \neq 0$ , then (1) is called **nonhomogeneous**. This is similar to Sec. 1.5.

For instance, a nonhomogeneous linear ODE is

$$y'' + 25y = e^{-x} \cos x,$$

and a homogeneous linear ODE is

$$xy'' + y' + xy = 0, \quad \text{in standard form} \quad y'' + \frac{1}{x}y' + y = 0.$$

An example of a nonlinear ODE is

$$y''y + y'^2 = 0.$$

The functions  $p$  and  $q$  in (1) and (2) are called the **coefficients** of the ODEs.

**Solutions** are defined similarly as for first-order ODEs in Chap. 1. A function

$$y = h(x)$$

is called a *solution* of a (linear or nonlinear) second-order ODE on some open interval  $I$  if  $h$  is defined and twice differentiable throughout that interval and is such that the ODE becomes an identity if we replace the unknown  $y$  by  $h$ , the derivative  $y'$  by  $h'$ , and the second derivative  $y''$  by  $h''$ . Examples are given below.

## Homogeneous Linear ODEs: Superposition Principle

Sections 2.1–2.6 will be devoted to **homogeneous** linear ODEs (2) and the remaining sections of the chapter to nonhomogeneous linear ODEs.

Linear ODEs have a rich solution structure. For the homogeneous equation the backbone of this structure is the *superposition principle* or *linearity principle*, which says that we can obtain further solutions from given ones by adding them or by multiplying them with any constants. Of course, this is a great advantage of homogeneous linear ODEs. Let us first discuss an example.

### EXAMPLE 1 Homogeneous Linear ODEs: Superposition of Solutions

The functions  $y = \cos x$  and  $y = \sin x$  are solutions of the homogeneous linear ODE

$$y'' + y = 0$$

for all  $x$ . We verify this by differentiation and substitution. We obtain  $(\cos x)'' = -\cos x$ ; hence

$$y'' + y = (\cos x)'' + \cos x = -\cos x + \cos x = 0.$$

Similarly for  $y = \sin x$  (verify!). We can go an important step further. We multiply  $\cos x$  by any constant, for instance, 4.7, and  $\sin x$  by, say,  $-2$ , and take the sum of the results, claiming that it is a solution. Indeed, differentiation and substitution gives

$$(4.7 \cos x - 2 \sin x)'' + (4.7 \cos x - 2 \sin x) = -4.7 \cos x + 2 \sin x + 4.7 \cos x - 2 \sin x = 0. \quad \blacksquare$$

In this example we have obtained from  $y_1 (= \cos x)$  and  $y_2 (= \sin x)$  a function of the form

$$(3) \quad y = c_1 y_1 + c_2 y_2 \quad (c_1, c_2 \text{ arbitrary constants}).$$

This is called a **linear combination** of  $y_1$  and  $y_2$ . In terms of this concept we can now formulate the result suggested by our example, often called the **superposition principle** or **linearity principle**.

**THEOREM 1****Fundamental Theorem for the Homogeneous Linear ODE (2)**

*For a homogeneous linear ODE (2), any linear combination of two solutions on an open interval  $I$  is again a solution of (2) on  $I$ . In particular, for such an equation, sums and constant multiples of solutions are again solutions.*

**PROOF**

Let  $y_1$  and  $y_2$  be solutions of (2) on  $I$ . Then by substituting  $y = c_1 y_1 + c_2 y_2$  and its derivatives into (2), and using the familiar rule  $(c_1 y_1 + c_2 y_2)' = c_1 y_1' + c_2 y_2'$ , etc., we get

$$\begin{aligned} y'' + py' + qy &= (c_1 y_1 + c_2 y_2)'' + p(c_1 y_1 + c_2 y_2)' + q(c_1 y_1 + c_2 y_2) \\ &= c_1 y_1'' + c_2 y_2'' + p(c_1 y_1' + c_2 y_2') + q(c_1 y_1 + c_2 y_2) \\ &= c_1 (y_1'' + py_1' + qy_1) + c_2 (y_2'' + py_2' + qy_2) = 0, \end{aligned}$$

since in the last line,  $(\cdot \cdot \cdot) = 0$  because  $y_1$  and  $y_2$  are solutions, by assumption. This shows that  $y$  is a solution of (2) on  $I$ . ■

**CAUTION!** Don't forget that this highly important theorem holds for *homogeneous linear* ODEs only but **does not hold** for nonhomogeneous linear or nonlinear ODEs, as the following two examples illustrate.

**EXAMPLE 2****A Nonhomogeneous Linear ODE**

Verify by substitution that the functions  $y = 1 + \cos x$  and  $y = 1 + \sin x$  are solutions of the nonhomogeneous linear ODE

$$y'' + y = 1,$$

but their sum is not a solution. Neither is, for instance,  $2(1 + \cos x)$  or  $5(1 + \sin x)$ . ■

**EXAMPLE 3****A Nonlinear ODE**

Verify by substitution that the functions  $y = x^2$  and  $y = 1$  are solutions of the nonlinear ODE

$$y''y - xy' = 0,$$

but their sum is not a solution. Neither is  $-x^2$ , so you cannot even multiply by  $-1$ ! ■

## Initial Value Problem. Basis. General Solution

Recall from Chap. 1 that for a first-order ODE, an *initial value problem* consists of the ODE and one *initial condition*  $y(x_0) = y_0$ . The initial condition is used to determine the *arbitrary constant*  $c$  in the *general solution* of the ODE. This results in a unique solution, as we need it in most applications. That solution is called a *particular solution* of the ODE. These ideas extend to second-order equations as follows.



For a second-order homogeneous linear ODE (2) an **initial value problem** consists of (2) and two **initial conditions**

$$(4) \quad y(x_0) = K_0, \quad y'(x_0) = K_1.$$

These conditions prescribe given values  $K_0$  and  $K_1$  of the solution and its first derivative (the slope of its curve) at the same given  $x = x_0$  in the open interval considered.

The conditions (4) are used to determine the two arbitrary constants  $c_1$  and  $c_2$  in a **general solution**

$$(5) \quad y = c_1 y_1 + c_2 y_2$$

of the ODE; here,  $y_1$  and  $y_2$  are suitable solutions of the ODE, with “suitable” to be explained after the next example. This results in a unique solution, passing through the point  $(x_0, K_0)$  with  $K_1$  as the tangent direction (the slope) at that point. That solution is called a **particular solution** of the ODE (2).

#### EXAMPLE 4 Initial Value Problem

Solve the initial value problem

$$y'' + y = 0, \quad y(0) = 3.0, \quad y'(0) = -0.5.$$

**Solution.** *Step 1. General solution.* The functions  $\cos x$  and  $\sin x$  are solutions of the ODE (by Example 1), and we take

$$y = c_1 \cos x + c_2 \sin x.$$

This will turn out to be a general solution as defined below.

*Step 2. Particular solution.* We need the derivative  $y' = -c_1 \sin x + c_2 \cos x$ . From this and the initial values we obtain, since  $\cos 0 = 1$  and  $\sin 0 = 0$ ,

$$y(0) = c_1 = 3.0 \quad \text{and} \quad y'(0) = c_2 = -0.5.$$

This gives as the solution of our initial value problem the particular solution

$$y = 3.0 \cos x - 0.5 \sin x.$$

Figure 28 shows that at  $x = 0$  it has the value 3.0 and the slope  $-0.5$ , so that its tangent intersects the  $x$ -axis at  $x = 3.0/0.5 = 6.0$ . (The scales on the axes differ!) ■

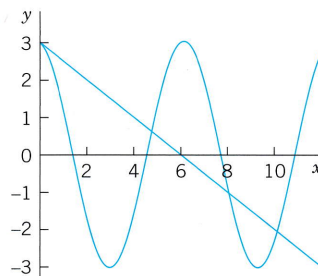


Fig. 28. Particular solution and initial tangent in Example 4

**Observation.** Our choice of  $y_1$  and  $y_2$  was general enough to satisfy both initial conditions. Now let us take instead two proportional solutions  $y_1 = \cos x$  and

$y_2 = k \cos x$ , so that  $y_1/y_2 = 1/k = \text{const}$ . Then we can write  $y = c_1 y_1 + c_2 y_2$  in the form

$$y = c_1 \cos x + c_2(k \cos x) = C \cos x \quad \text{where} \quad C = c_1 + c_2 k.$$

Hence we are no longer able to satisfy two initial conditions with only one arbitrary constant  $C$ . Consequently, in defining the concept of a general solution, we must exclude proportionality. And we see at the same time why the concept of a general solution is of importance in connection with initial value problems.

**DEFINITION****General Solution, Basis, Particular Solution**

A **general solution** of an ODE (2) on an open interval  $I$  is a solution (5) in which  $y_1$  and  $y_2$  are solutions of (2) on  $I$  that are not proportional, and  $c_1$  and  $c_2$  are arbitrary constants. These  $y_1, y_2$  are called a **basis** (or a **fundamental system**) of solutions of (2) on  $I$ .

A **particular solution** of (2) on  $I$  is obtained if we assign specific values to  $c_1$  and  $c_2$  in (5).

For the definition of an *interval* see Sec. 1.1. Also,  $c_1$  and  $c_2$  must sometimes be restricted to some interval in order to avoid complex expressions in the solution. Furthermore, as usual,  $y_1$  and  $y_2$  are called *proportional* on  $I$  if for all  $x$  on  $I$ ,

$$(6) \quad (a) \quad y_1 = k y_2 \quad \text{or} \quad (b) \quad y_2 = l y_1$$

where  $k$  and  $l$  are numbers, zero or not. (Note that (a) implies (b) if and only if  $k \neq 0$ ).

Actually, we can reformulate our definition of a basis by using a concept of general importance. Namely, two functions  $y_1$  and  $y_2$  are called **linearly independent** on an interval  $I$  where they are defined if

$$(7) \quad k_1 y_1(x) + k_2 y_2(x) = 0 \quad \text{everywhere on } I \text{ implies} \quad k_1 = 0 \text{ and } k_2 = 0.$$

And  $y_1$  and  $y_2$  are called **linearly dependent** on  $I$  if (7) also holds for some constants  $k_1, k_2$  not both zero. Then if  $k_1 \neq 0$  or  $k_2 \neq 0$ , we can divide and see that  $y_1$  and  $y_2$  are proportional,

$$y_1 = -\frac{k_2}{k_1} y_2 \quad \text{or} \quad y_2 = -\frac{k_1}{k_2} y_1.$$

In contrast, in the case of linear *independence* these functions are not proportional because then we cannot divide in (7). This gives the following

**DEFINITION****Basis (Reformulated)**

A **basis** of solutions of (2) on an open interval  $I$  is a pair of linearly independent solutions of (2) on  $I$ .

If the coefficients  $p$  and  $q$  of (2) are continuous on some open interval  $I$ , then (2) has a general solution. It yields the unique solution of any initial value problem (2), (4). It

includes all solutions of (2) on  $I$ ; hence (2) has no *singular solutions* (solutions not obtainable from a general solution; see also Problem Set 1.1). All this will be shown in Sec. 2.6.

### EXAMPLE 5 Basis, General Solution, Particular Solution

$\cos x$  and  $\sin x$  in Example 4 form a basis of solutions of the ODE  $y'' + y = 0$  for all  $x$  because their quotient is  $\cot x \neq \text{const}$  (or  $\tan x \neq \text{const}$ ). Hence  $y = c_1 \cos x + c_2 \sin x$  is a general solution. The solution  $y = 3.0 \cos x - 0.5 \sin x$  of the initial value problem is a particular solution. ■

### EXAMPLE 6 Basis, General Solution, Particular Solution

Verify by substitution that  $y_1 = e^x$  and  $y_2 = e^{-x}$  are solutions of the ODE  $y'' - y = 0$ . Then solve the initial value problem

$$y'' - y = 0, \quad y(0) = 6, \quad y'(0) = -2.$$

**Solution.**  $(e^x)'' - e^x = 0$  and  $(e^{-x})'' - e^{-x} = 0$  shows that  $e^x$  and  $e^{-x}$  are solutions. They are not proportional,  $e^x/e^{-x} = e^{2x} \neq \text{const}$ . Hence  $e^x, e^{-x}$  form a basis for all  $x$ . We now write down the corresponding general solution and its derivative and equate their values at 0 to the given initial conditions,

$$y = c_1 e^x + c_2 e^{-x}, \quad y' = c_1 e^x - c_2 e^{-x}, \quad y(0) = c_1 + c_2 = 6, \quad y'(0) = c_1 - c_2 = -2.$$

By addition and subtraction,  $c_1 = 2, c_2 = 4$ , so that the *answer* is  $y = 2e^x + 4e^{-x}$ . This is the particular solution satisfying the two initial conditions. ■

## Find a Basis if One Solution Is Known. Reduction of Order

It happens quite often that one solution can be found by inspection or in some other way. Then a second linearly independent solution can be obtained by solving a first-order ODE. This is called the method of **reduction of order**.<sup>1</sup> We first show this method for an example and then in general.

### EXAMPLE 7 Reduction of Order if a Solution Is Known. Basis

Find a basis of solutions of the ODE

$$(x^2 - x)y'' - xy' + y = 0.$$

**Solution.** Inspection shows that  $y_1 = x$  is a solution because  $y_1' = 1$  and  $y_1'' = 0$ , so that the first term vanishes identically and the second and third terms cancel. The idea of the method is to substitute

$$y = uy_1 = ux, \quad y' = u'x + u, \quad y'' = u''x + 2u'$$

into the ODE. This gives

$$(x^2 - x)(u''x + 2u') - x(u'x + u) + ux = 0.$$

$ux$  and  $-xu$  cancel and we are left with the following ODE, which we divide by  $x$ , order, and simplify,

$$(x^2 - x)(u''x + 2u') - x^2u' = 0, \quad (x^2 - x)u'' + (x - 2)u' = 0.$$

<sup>1</sup>Credited to the great mathematician JOSEPH LOUIS LAGRANGE (1736–1813), who was born in Turin, of French extraction, got his first professorship when he was 19 (at the Military Academy of Turin), became director of the mathematical section of the Berlin Academy in 1766, and moved to Paris in 1787. His important major work was in the calculus of variations, celestial mechanics, general mechanics (*Mécanique analytique*, Paris, 1788), differential equations, approximation theory, algebra, and number theory.

This ODE is of first order in  $v = u'$ , namely,  $(x^2 - x)v' + (x - 2)v = 0$ . Separation of variables and integration gives

$$\frac{dv}{v} = -\frac{x-2}{x^2-x} dx = \left(\frac{1}{x-1} - \frac{2}{x}\right) dx, \quad \ln |v| = \ln |x-1| - 2 \ln |x| = \ln \frac{|x-1|}{x^2}.$$

We need no constant of integration because we want to obtain a particular solution; similarly in the next integration. Taking exponents and integrating again, we obtain

$$v = \frac{x-1}{x^2} = \frac{1}{x} - \frac{1}{x^2}, \quad u = \int v dx = \ln |x| + \frac{1}{x}, \quad \text{hence } y_2 = ux = x \ln |x| + 1.$$

Since  $y_1 = x$  and  $y_2 = x \ln |x| + 1$  are linearly independent (their quotient is not constant), we have obtained a basis of solutions, valid for all positive  $x$ . ■

In this example we applied **reduction of order** to a homogeneous linear ODE [see (2)]

$$y'' + p(x)y' + q(x)y = 0.$$

Note that we now take the ODE in standard form, with  $y''$ , not  $f(x)y''$ —this is essential in applying our subsequent formulas. We assume a solution  $y_1$  of (2) on an open interval  $I$  to be known and want to find a basis. For this we need a second linearly independent solution  $y_2$  of (2) on  $I$ . To get  $y_2$ , we substitute

$$y = y_2 = uy_1, \quad y' = y_2' = u'y_1 + uy_1', \quad y'' = y_2'' = u''y_1 + 2u'y_1' + uy_1''$$

into (2). This gives

$$(8) \quad u''y_1 + 2u'y_1' + uy_1'' + p(u'y_1 + uy_1') + qu_1y_1 = 0.$$

Collecting terms in  $u''$ ,  $u'$ , and  $u$ , we have

$$u''y_1 + u'(2y_1' + py_1) + u(y_1'' + py_1' + qy_1) = 0.$$

Now comes the main point. Since  $y_1$  is a solution of (2), the expression in the last parentheses is zero. Hence  $u$  is gone, and we are left with an ODE in  $u'$  and  $u''$ . We divide this remaining ODE by  $y_1$  and set  $u' = U$ ,  $u'' = U'$ ,

$$u'' + u' \frac{2y_1' + py_1}{y_1} = 0, \quad \text{thus} \quad U' + \left(\frac{2y_1'}{y_1} + p\right)U = 0.$$

This is the desired first-order ODE, the reduced ODE. Separation of variables and integration gives

$$\frac{dU}{U} = -\left(\frac{2y_1'}{y_1} + p\right) dx \quad \text{and} \quad \ln |U| = -2 \ln |y_1| - \int p dx.$$

By taking exponents we finally obtain

$$(9) \quad U = \frac{1}{y_1^2} e^{-\int p dx}.$$

Here  $U = u'$ , so that  $u = \int U dx$ . Hence the desired second solution is

$$y_2 = y_1 u = y_1 \int U dx.$$

The quotient  $y_2/y_1 = u = \int U dx$  cannot be constant (since  $U > 0$ ), so that  $y_1$  and  $y_2$  form a basis of solutions.

## PROBLEM SET 2.1

### 1–6 GENERAL SOLUTION. INITIAL VALUE PROBLEM

(More in the next problem set.) Verify by substitution that the given functions form a basis. Solve the given initial value problem. (Show the details of your work.)

- $y'' - 16y = 0$ ,  $e^{4x}$ ,  $e^{-4x}$ ,  $y(0) = 3$ ,  $y'(0) = 8$
- $y'' + 25y = 0$ ,  $\cos 5x$ ,  $\sin 5x$ ,  $y(0) = 0.8$ ,  $y'(0) = -6.5$
- $y'' + 2y' + 2y = 0$ ,  $e^{-x} \cos x$ ,  $e^{-x} \sin x$ ,  $y(0) = 1$ ,  $y'(0) = -1$
- $y'' - 6y' + 9y = 0$ ,  $e^{3x}$ ,  $xe^{3x}$ ,  $y(0) = -1.4$ ,  $y'(0) = 4.6$
- $x^2 y'' + xy' - 4y = 0$ ,  $x^2$ ,  $x^{-2}$ ,  $y(1) = 11$ ,  $y'(1) = -6$
- $x^2 y'' - 7xy' + 15y = 0$ ,  $x^3$ ,  $x^5$ ,  $y(1) = 0.4$ ,  $y'(1) = 1.0$

### 7–14 LINEAR INDEPENDENCE AND DEPENDENCE

Are the following functions linearly independent on the given interval?

- $x$ ,  $x \ln x$  ( $0 < x < 10$ )
- $3x^2$ ,  $2x^n$  ( $0 < x < 1$ )
- $e^{ax}$ ,  $e^{-ax}$  (any interval)
- $\cos^2 x$ ,  $\sin^2 x$  (any interval)
- $\ln x$ ,  $\ln x^2$  ( $x > 0$ )
- $x - 2$ ,  $x + 2$  ( $-2 < x < 2$ )
- $5 \sin x \cos x$ ,  $3 \sin 2x$  ( $x > 0$ )
- $0$ ,  $\sinh \pi x$  ( $x > 0$ )

**REDUCTION OF ORDER** is important because it gives a simpler ODE. A second-order ODE  $F(x, y, y', y'') = 0$ , linear or not, can be reduced to first order if  $y$  does not occur explicitly (Prob. 15) or if  $x$  does not occur explicitly (Prob. 16) or if the ODE is homogeneous linear and we know a solution (see the text).

- (Reduction)** Show that  $F(x, y', y'') = 0$  can be reduced to first order in  $z = y'$  (from which  $y$  follows by integration). Give two examples of your own.
- (Reduction)** Show that  $F(y, y', y'') = 0$  can be reduced to a first-order ODE with  $y$  as the independent variable and  $y'' = (dz/dy)z$ , where  $z = y'$ ; derive this by the chain rule. Give two examples.

**17–22** Reduce to first order and solve (showing each step in detail).

- $y'' = ky'$
- $y'' = 1 + y'^2$
- $yy'' = 4y'^2$
- $xy'' + 2y' + xy = 0$ ,  $y_1 = x^{-1} \cos x$
- $y'' + y'^3 \sin y = 0$
- $(1 - x^2)y'' - 2xy' + 2y = 0$ ,  $y_1 = x$

**23. (Motion)** A small body moves on a straight line. Its velocity equals twice the reciprocal of its acceleration. If at  $t = 0$  the body has distance 1 m from the origin and velocity 2 m/sec, what are its distance and velocity after 3 sec?

**24. (Hanging cable)** It can be shown that the curve  $y(x)$  of an inextensible flexible homogeneous cable hanging between two fixed points is obtained by solving  $y'' = k\sqrt{1 + y'^2}$ , where the constant  $k$  depends on the weight. This curve is called a *catenary* (from Latin *catena* = the chain). Find and graph  $y(x)$ , assuming  $k = 1$  and those fixed points are  $(-1, 0)$  and  $(1, 0)$  in a vertical  $xy$ -plane.

**25. (Curves)** Find and sketch or graph the curves passing through the origin with slope 1 for which the second derivative is proportional to the first.

**26. WRITING PROJECT. General Properties of Solutions of Linear ODEs.** Write a short essay (with proofs and simple examples of your own) that includes the following.

(a) The superposition principle.

(b)  $y \equiv 0$  is a solution of the homogeneous equation (2) (called the **trivial solution**).

(c) The sum  $y = y_1 + y_2$  of a solution  $y_1$  of (1) and  $y_2$  of (2) is a solution of (1).

(d) Explore possibilities of making further general statements on solutions of (1) and (2) (sums, differences, multiples).

**27. CAS PROJECT. Linear Independence.** Write a program for testing linear independence and dependence. Try it out on some of the problems in this problem set and on examples of your own.

## 2.2 Homogeneous Linear ODEs with Constant Coefficients

We shall now consider second-order homogeneous linear ODEs whose coefficients  $a$  and  $b$  are constant,

$$(1) \quad y'' + ay' + by = 0.$$

These equations have important applications, especially in connection with mechanical and electrical vibrations, as we shall see in Secs. 2.4, 2.8, and 2.9.

How to solve (1)? We remember from Sec. 1.5 that the solution of the *first-order* linear ODE with a constant coefficient  $k$

$$y' + ky = 0$$

is an exponential function  $y = ce^{-kx}$ . This gives us the idea to try as a solution of (1) the function

$$(2) \quad y = e^{\lambda x}.$$

Substituting (2) and its derivatives

$$y' = \lambda e^{\lambda x} \quad \text{and} \quad y'' = \lambda^2 e^{\lambda x}$$

into our equation (1), we obtain

$$(\lambda^2 + a\lambda + b)e^{\lambda x} = 0.$$

Hence if  $\lambda$  is a solution of the important **characteristic equation** (or *auxiliary equation*)

$$(3) \quad \lambda^2 + a\lambda + b = 0$$

then the exponential function (2) is a solution of the ODE (1). Now from elementary algebra we recall that the roots of this quadratic equation (3) are

$$(4) \quad \lambda_1 = \frac{1}{2}(-a + \sqrt{a^2 - 4b}), \quad \lambda_2 = \frac{1}{2}(-a - \sqrt{a^2 - 4b}).$$

(3) and (4) will be basic because our derivation shows that the functions

$$(5) \quad y_1 = e^{\lambda_1 x} \quad \text{and} \quad y_2 = e^{\lambda_2 x}$$

are solutions of (1). Verify this by substituting (5) into (1).

From algebra we further know that the quadratic equation (3) may have three kinds of roots, depending on the sign of the discriminant  $a^2 - 4b$ , namely,

**(Case I)** Two real roots if  $a^2 - 4b > 0$ ,

**(Case II)** A real double root if  $a^2 - 4b = 0$ ,

**(Case III)** Complex conjugate roots if  $a^2 - 4b < 0$ .

## Case I. Two Distinct Real Roots $\lambda_1$ and $\lambda_2$

In this case, a basis of solutions of (1) on any interval is

$$y_1 = e^{\lambda_1 x} \quad \text{and} \quad y_2 = e^{\lambda_2 x}$$

because  $y_1$  and  $y_2$  are defined (and real) for all  $x$  and their quotient is not constant. The corresponding general solution is

$$(6) \quad y = c_1 e^{\lambda_1 x} + c_2 e^{\lambda_2 x}.$$

### EXAMPLE 1 General Solution in the Case of Distinct Real Roots

We can now solve  $y'' - y = 0$  in Example 6 of Sec. 2.1 systematically. The characteristic equation is  $\lambda^2 - 1 = 0$ . Its roots are  $\lambda_1 = 1$  and  $\lambda_2 = -1$ . Hence a basis of solutions is  $e^x$  and  $e^{-x}$  and gives the same general solution as before,

$$y = c_1 e^x + c_2 e^{-x}. \quad \blacksquare$$

### EXAMPLE 2 Initial Value Problem in the Case of Distinct Real Roots

Solve the initial value problem

$$y'' + y' - 2y = 0, \quad y(0) = 4, \quad y'(0) = -5.$$

**Solution.** *Step 1. General solution.* The characteristic equation is

$$\lambda^2 + \lambda - 2 = 0.$$

Its roots are

$$\lambda_1 = \frac{1}{2}(-1 + \sqrt{9}) = 1 \quad \text{and} \quad \lambda_2 = \frac{1}{2}(-1 - \sqrt{9}) = -2$$

so that we obtain the general solution

$$y = c_1 e^x + c_2 e^{-2x}.$$

*Step 2. Particular solution.* Since  $y'(x) = c_1 e^x - 2c_2 e^{-2x}$ , we obtain from the general solution and the initial conditions

$$y(0) = c_1 + c_2 = 4,$$

$$y'(0) = c_1 - 2c_2 = -5.$$

Hence  $c_1 = 1$  and  $c_2 = 3$ . This gives the *answer*  $y = e^x + 3e^{-2x}$ . Figure 29 shows that the curve begins at  $y = 4$  with a negative slope ( $-5$ , but note that the axes have different scales!), in agreement with the initial conditions.  $\blacksquare$

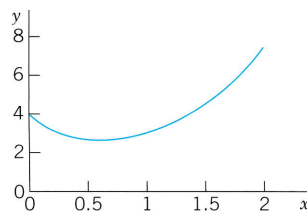


Fig. 29. Solution in Example 2

## Case II. Real Double Root $\lambda = -a/2$

If the discriminant  $a^2 - 4b$  is zero, we see directly from (4) that we get only one root,  $\lambda = \lambda_1 = \lambda_2 = -a/2$ , hence only one solution,

$$y_1 = e^{-(a/2)x}.$$

To obtain a second independent solution  $y_2$  (needed for a basis), we use the method of reduction of order discussed in the last section, setting  $y_2 = uy_1$ . Substituting this and its derivatives  $y_2' = u'y_1 + uy_1'$  and  $y_2''$  into (1), we first have

$$(u''y_1 + 2u'y_1' + uy_1'') + a(u'y_1 + uy_1') + buy_1 = 0.$$

Collecting terms in  $u''$ ,  $u'$ , and  $u$ , as in the last section, we obtain

$$u''y_1 + u'(2y_1' + ay_1) + u(y_1'' + ay_1' + by_1) = 0.$$

The expression in the last parentheses is zero, since  $y_1$  is a solution of (1). The expression in the first parentheses is zero, too, since

$$2y_1' = -ae^{-ax/2} = -ay_1.$$

We are thus left with  $u''y_1 = 0$ . Hence  $u'' = 0$ . By two integrations,  $u = c_1x + c_2$ . To get a second independent solution  $y_2 = uy_1$ , we can simply choose  $c_1 = 1$ ,  $c_2 = 0$  and take  $u = x$ . Then  $y_2 = xy_1$ . Since these solutions are not proportional, they form a basis. Hence in the case of a double root of (3) a basis of solutions of (1) on any interval is

$$e^{-ax/2}, \quad xe^{-ax/2}.$$

The corresponding general solution is

$$(7) \quad y = (c_1 + c_2x)e^{-ax/2}.$$

**Warning.** If  $\lambda$  is a *simple* root of (4), then  $(c_1 + c_2x)e^{\lambda x}$  with  $c_2 \neq 0$  is *not* a solution of (1).

### EXAMPLE 3 General Solution in the Case of a Double Root

The characteristic equation of the ODE  $y'' + 6y' + 9y = 0$  is  $\lambda^2 + 6\lambda + 9 = (\lambda + 3)^2 = 0$ . It has the double root  $\lambda = -3$ . Hence a basis is  $e^{-3x}$  and  $xe^{-3x}$ . The corresponding general solution is  $y = (c_1 + c_2x)e^{-3x}$ . ■

### EXAMPLE 4 Initial Value Problem in the Case of a Double Root

Solve the initial value problem

$$y'' + y' + 0.25y = 0, \quad y(0) = 3.0, \quad y'(0) = -3.5.$$

**Solution.** The characteristic equation is  $\lambda^2 + \lambda + 0.25 = (\lambda + 0.5)^2 = 0$ . It has the double root  $\lambda = -0.5$ . This gives the general solution

$$y = (c_1 + c_2x)e^{-0.5x}.$$

We need its derivative

$$y' = c_2e^{-0.5x} - 0.5(c_1 + c_2x)e^{-0.5x}.$$



From this and the initial conditions we obtain

$$y(0) = c_1 = 3.0, \quad y'(0) = c_2 - 0.5c_1 = -3.5; \quad \text{hence} \quad c_2 = -2.$$

The particular solution of the initial value problem is  $y = (3 - 2x)e^{-0.5x}$ . See Fig. 30. ■

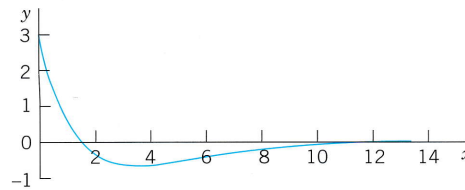


Fig. 30. Solution in Example 4

### Case III. Complex Roots $-\frac{1}{2}a + i\omega$ and $-\frac{1}{2}a - i\omega$

This case occurs if the discriminant  $a^2 - 4b$  of the characteristic equation (3) is negative. In this case, the roots of (3) and thus the solutions of the ODE (1) come at first out complex. However, we show that from them we can obtain a basis of *real* solutions

$$(8) \quad y_1 = e^{-ax/2} \cos \omega x, \quad y_2 = e^{-ax/2} \sin \omega x \quad (\omega > 0)$$

where  $\omega^2 = b - \frac{1}{4}a^2$ . It can be verified by substitution that these are solutions in the present case. We shall derive them systematically after the two examples by using the complex exponential function. They form a basis on any interval since their quotient  $\cot \omega x$  is not constant. Hence a real general solution in Case III is

$$(9) \quad y = e^{-ax/2} (A \cos \omega x + B \sin \omega x) \quad (A, B \text{ arbitrary}).$$

#### EXAMPLE 5 Complex Roots. Initial Value Problem

Solve the initial value problem

$$y'' + 0.4y' + 9.04y = 0, \quad y(0) = 0, \quad y'(0) = 3.$$

**Solution.** *Step 1. General solution.* The characteristic equation is  $\lambda^2 + 0.4\lambda + 9.04 = 0$ . It has the roots  $-0.2 \pm 3i$ . Hence  $\omega = 3$ , and a general solution (9) is

$$y = e^{-0.2x}(A \cos 3x + B \sin 3x).$$

*Step 2. Particular solution.* The first initial condition gives  $y(0) = A = 0$ . The remaining expression is  $y = Be^{-0.2x} \sin 3x$ . We need the derivative (chain rule!)

$$y' = B(-0.2e^{-0.2x} \sin 3x + 3e^{-0.2x} \cos 3x).$$

From this and the second initial condition we obtain  $y'(0) = 3B = 3$ . Hence  $B = 1$ . Our solution is

$$y = e^{-0.2x} \sin 3x.$$

Figure 31 shows  $y$  and the curves of  $e^{-0.2x}$  and  $-e^{-0.2x}$  (dashed), between which the curve of  $y$  oscillates. Such “damped vibrations” (with  $x = t$  being time) have important mechanical and electrical applications, as we shall soon see (in Sec. 2.4). ■

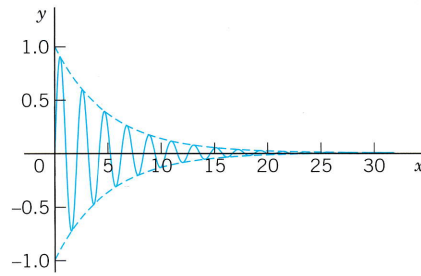


Fig. 31. Solution in Example 5

**EXAMPLE 6 Complex Roots**

A general solution of the ODE

$$y'' + \omega^2 y = 0 \quad (\omega \text{ constant, not zero})$$

is

$$y = A \cos \omega x + B \sin \omega x.$$

With  $\omega = 1$  this confirms Example 4 in Sec. 2.1. ■

**Summary of Cases I–III**

Case	Roots of (2)	Basis of (1)	General Solution of (1)
I	Distinct real $\lambda_1, \lambda_2$	$e^{\lambda_1 x}, e^{\lambda_2 x}$	$y = c_1 e^{\lambda_1 x} + c_2 e^{\lambda_2 x}$
II	Real double root $\lambda = -\frac{1}{2}a$	$e^{-ax/2}, xe^{-ax/2}$	$y = (c_1 + c_2 x)e^{-ax/2}$
III	Complex conjugate $\lambda_1 = -\frac{1}{2}a + i\omega,$ $\lambda_2 = -\frac{1}{2}a - i\omega$	$e^{-ax/2} \cos \omega x$ $e^{-ax/2} \sin \omega x$	$y = e^{-ax/2}(A \cos \omega x + B \sin \omega x)$

It is very interesting that in applications to mechanical systems or electrical circuits, these three cases correspond to three different forms of motion or flows of current, respectively. We shall discuss this basic relation between theory and practice in detail in Sec. 2.4 (and again in Sec. 2.8).

**Derivation in Case III. Complex Exponential Function**

If verification of the solutions in (8) satisfies you, skip the systematic derivation of these real solutions from the complex solutions by means of the complex exponential function  $e^z$  of a complex variable  $z = r + it$ . We write  $r + it$ , not  $x + iy$  because  $x$  and  $y$  occur in the ODE. The definition of  $e^z$  in terms of the real functions  $e^r$ ,  $\cos t$ , and  $\sin t$  is

(10) 
$$e^z = e^{r+it} = e^r e^{it} = e^r(\cos t + i \sin t).$$

This is motivated as follows. For real  $z = r$ , hence  $t = 0$ ,  $\cos 0 = 1$ ,  $\sin 0 = 0$ , we get the real exponential function  $e^r$ . It can be shown that  $e^{z_1+z_2} = e^{z_1}e^{z_2}$ , just as in real. (Proof in Sec. 13.5.) Finally, if we use the Maclaurin series of  $e^z$  with  $z = it$  as well as  $i^2 = -1$ ,  $i^3 = -i$ ,  $i^4 = 1$ , etc., and reorder the terms as shown (this is permissible, as can be proved), we obtain the series

$$\begin{aligned} e^{it} &= 1 + it + \frac{(it)^2}{2!} + \frac{(it)^3}{3!} + \frac{(it)^4}{4!} + \frac{(it)^5}{5!} + \cdots \\ &= 1 - \frac{t^2}{2!} + \frac{t^4}{4!} - \cdots + i\left(t - \frac{t^3}{3!} + \frac{t^5}{5!} - \cdots\right) \\ &= \cos t + i \sin t. \end{aligned}$$

(Look up these real series in your calculus book if necessary.) We see that we have obtained the formula

$$(11) \quad e^{it} = \cos t + i \sin t,$$

called the **Euler formula**. Multiplication by  $e^r$  gives (10).

For later use we note that  $e^{-it} = \cos(-t) + i \sin(-t) = \cos t - i \sin t$ , so that by addition and subtraction of this and (11),

$$(12) \quad \cos t = \frac{1}{2}(e^{it} + e^{-it}), \quad \sin t = \frac{1}{2i}(e^{it} - e^{-it}).$$

After these comments on the definition (10), let us now turn to Case III.

In Case III the radicand  $a^2 - 4b$  in (4) is negative. Hence  $4b - a^2$  is positive and, using  $\sqrt{-1} = i$ , we obtain in (4)

$$\frac{1}{2}\sqrt{a^2 - 4b} = \frac{1}{2}\sqrt{-(4b - a^2)} = \sqrt{-(b - \frac{1}{4}a^2)} = i\sqrt{b - \frac{1}{4}a^2} = i\omega$$

with  $\omega$  defined as in (8). Hence in (4),

$$\lambda_1 = \frac{1}{2}a + i\omega \quad \text{and, similarly,} \quad \lambda_2 = \frac{1}{2}a - i\omega.$$

Using (10) with  $r = -\frac{1}{2}ax$  and  $t = \omega x$ , we thus obtain

$$\begin{aligned} e^{\lambda_1 x} &= e^{-(a/2)x + i\omega x} = e^{-(a/2)x}(\cos \omega x + i \sin \omega x) \\ e^{\lambda_2 x} &= e^{-(a/2)x - i\omega x} = e^{-(a/2)x}(\cos \omega x - i \sin \omega x). \end{aligned}$$

We now add these two lines and multiply the result by  $\frac{1}{2}$ . This gives  $y_1$  as in (8). Then we subtract the second line from the first and multiply the result by  $1/(2i)$ . This gives  $y_2$  as in (8). These results obtained by addition and multiplication by constants are again solutions, as follows from the superposition principle in Sec. 2.1. This concludes the derivation of these real solutions in Case III.

## PROBLEM SET 2.2

### 1-14 GENERAL SOLUTION

Find a general solution. Check your answer by substitution.

1.  $y'' - 6y' - 7y = 0$
2.  $10y'' - 7y' + 1.2y = 0$
3.  $4y'' - 20y' + 25y = 0$
4.  $y'' + 4\pi y' + 4\pi^2 y = 0$
5.  $100y'' + 20y' - 99y = 0$
6.  $y'' + 2y' + 5y = 0$
7.  $y'' - y' + 2.5y = 0$
8.  $y'' + 2.6y' + 1.69y = 0$
9.  $y'' - 2y' - 5.25y = 0$
10.  $y'' - 2y = 0$
11.  $y'' + 9\pi^2 y = 0$
12.  $y'' + 2.4y' + 4.0y = 0$
13.  $y'' - 144y = 0$
14.  $y'' + y' - 0.96y = 0$

### 15-20 FIND ODE

Find an ODE  $y'' + ay' + by = 0$  for the given basis.

15.  $e^{2x}, e^x$
16.  $e^{0.5x}, e^{-3.5x}$
17.  $e^{x\sqrt{3}}, xe^{x\sqrt{3}}$
18.  $1, e^{-3x}$
19.  $e^{4x}, e^{-4x}$
20.  $e^{(-1+i)x}, e^{-(1+i)x}$

### 21-32 INITIAL VALUE PROBLEMS

Solve the initial value problem. Check that your answer satisfies the ODE as well as the initial conditions. (Show the details of your work.)

21.  $y'' - 2y' - 3y = 0, y(0) = 2, y'(0) = 14$
22.  $y'' + 2y' + y = 0, y(0) = 4, y'(0) = -6$
23.  $y'' + 4y' + 5y = 0, y(0) = 2, y'(0) = -5$
24.  $10y'' - 50y' + 65y = 0, y(0) = 1.5, y'(0) = 1.5$
25.  $y'' + \pi y' = 0, y(0) = 3, y'(0) = -\pi$
26.  $10y'' + 18y' + 5.6y = 0, y(0) = 4, y'(0) = -3.8$

27.  $10y'' + 5y' + 0.625y = 0, y(0) = 2, y'(0) = -4.5$

28.  $y'' - 9y = 0, y(0) = -2, y'(0) = -12$

29.  $20y'' + 4y' + y = 0, y(0) = 3.2, y'(0) = 0$

30.  $y'' + 2ky' + (k^2 + \omega^2)y = 0, y(0) = 1, y'(0) = -k$

31.  $y'' - 25y = 0, y(0) = 0, y'(0) = 40$

32.  $y'' - 2y' - 24y = 0, y(0) = 0, y'(0) = 20$

33. **(Instability)** Solve  $y'' - y = 0$  for the initial conditions  $y(0) = 1, y'(0) = -1$ . Then change the initial conditions to  $y(0) = 1.001, y'(0) = -0.999$  and explain why this small change of 0.001 at  $x = 0$  causes a large change later, e.g., 22 at  $x = 10$ .

### 34. TEAM PROJECT. General Properties of Solutions

**(A) Coefficient formulas.** Show how  $a$  and  $b$  in (1) can be expressed in terms of  $\lambda_1$  and  $\lambda_2$ . Explain how these formulas can be used in constructing equations for given bases.

**(B) Root zero.** Solve  $y'' + 4y' = 0$  (i) by the present method, and (ii) by reduction to first order. Can you explain why the result must be the same in both cases? Can you do the same for a general ODE  $y'' + ay' = 0$ ?

**(C) Double root.** Verify directly that  $xe^{\lambda x}$  with  $\lambda = -a/2$  is a solution of (1) in the case of a double root. Verify and explain why  $y = e^{-2x}$  is a solution of  $y'' - y' - 6y = 0$  but  $xe^{-2x}$  is not.

**(D) Limits.** Double roots should be limiting cases of distinct roots  $\lambda_1, \lambda_2$  as, say,  $\lambda_2 \rightarrow \lambda_1$ . Experiment with this idea. (Remember l'Hôpital's rule from calculus.) Can you arrive at  $xe^{\lambda_1 x}$ ? Give it a try.

35. **(Verification)** Show by substitution that  $y_1$  in (8) is a solution of (1).

## 2.3 Differential Operators. *Optional*

This short section can be omitted without interrupting the flow of ideas; it will not be used in the sequel (except for the notations  $Dy, D^2y$ , etc., for  $y', y''$ , etc.).

**Operational calculus** means the technique and application of operators. Here, an **operator** is a transformation that transforms a function into another function. Hence differential calculus involves an operator, the **differential operator**  $D$ , which transforms a (differentiable) function into its derivative. In operator notation we write

$$(1) \quad Dy = y' = \frac{dy}{dx}.$$

Similarly, for the higher derivatives we write  $D^2y = D(Dy) = y''$ , and so on. For example,  $D \sin = \cos$ ,  $D^2 \sin = -\sin$ , etc.

For a homogeneous linear ODE  $y'' + ay' + by = 0$  with constant coefficients we can now introduce the **second-order differential operator**

$$L = P(D) = D^2 + aD + bI,$$

where  $I$  is the **identity operator** defined by  $Iy = y$ . Then we can write that ODE as

$$(2) \quad Ly = P(D)y = (D^2 + aD + bI)y = 0.$$

$P$  suggests “polynomial.”  $L$  is a **linear operator**. By definition this means that if  $Ly$  and  $Lw$  exist (this is the case if  $y$  and  $w$  are twice differentiable), then  $L(cy + kw)$  exists for any constants  $c$  and  $k$ , and

$$L(cy + kw) = cLy + kLw.$$

Let us show that from (2) we reach agreement with the results in Sec. 2.2. Since  $(De^\lambda)(x) = \lambda e^{\lambda x}$  and  $(D^2e^\lambda)(x) = \lambda^2 e^{\lambda x}$ , we obtain

$$(3) \quad \begin{aligned} Le^\lambda(x) &= P(D)e^\lambda(x) = (D^2 + aD + bI)e^\lambda(x) \\ &= (\lambda^2 + a\lambda + b)e^{\lambda x} = P(\lambda)e^{\lambda x} = 0. \end{aligned}$$

This confirms our result of Sec. 2.2 that  $e^{\lambda x}$  is a solution of the ODE (2) if and only if  $\lambda$  is a solution of the characteristic equation  $P(\lambda) = 0$ .

$P(\lambda)$  is a polynomial in the usual sense of algebra. If we replace  $\lambda$  by the operator  $D$ , we obtain the “operator polynomial”  $P(D)$ . The point of this operational calculus is that  $P(D)$  can be treated just like an algebraic quantity. In particular, we can factor it.

### EXAMPLE 1 Factorization, Solution of an ODE

Factor  $P(D) = D^2 - 3D - 40I$  and solve  $P(D)y = 0$ .

**Solution.**  $D^2 - 3D - 40I = (D - 8I)(D + 5I)$  because  $I^2 = I$ . Now  $(D - 8I)y = y' - 8y = 0$  has the solution  $y_1 = e^{8x}$ . Similarly, the solution of  $(D + 5I)y = 0$  is  $y_2 = e^{-5x}$ . This is a basis of  $P(D)y = 0$  on any interval. From the factorization we obtain the ODE, as expected,

$$\begin{aligned} (D - 8I)(D + 5I)y &= (D - 8I)(y' + 5y) = D(y' + 5y) - 8(y' + 5y) \\ &= y'' + 5y' - 8y' - 40y = y'' - 3y' - 40y = 0. \end{aligned}$$

Verify that this agrees with the result of our method in Sec. 2.2. This is not unexpected because we factored  $P(D)$  in the same way as the characteristic polynomial  $P(\lambda) = \lambda^2 - 3\lambda - 40$ . ■

It was essential that  $L$  in (2) has *constant* coefficients. Extension of operator methods to variable-coefficient ODEs is more difficult and will not be considered here.

If operational methods were limited to the simple situations illustrated in this section, it would perhaps not be worth mentioning. Actually, the power of the operator approach appears in more complicated engineering problems, as we shall see in Chap. 6.

## PROBLEM SET 2.3

## 1–5 APPLICATION OF DIFFERENTIAL OPERATORS

Apply the given operator to the given functions. (Show all steps in detail.)

- $(D - I)^2$ ;  $e^x$ ,  $xe^x$ ,  $\sin x$
- $8D^2 + 2D - I$ ;  $\cosh \frac{1}{2}x$ ,  $\sinh \frac{1}{2}x$ ,  $e^{x/2}$
- $D - 0.4I$ ;  $2x^3 - 1$ ,  $e^{0.4x}$ ,  $xe^{0.4x}$
- $(D + 5I)(D - I)$ ;  $e^{-5x} \sin x$ ,  $e^{5x}$ ,  $x^2$
- $(D - 4I)(D + 3I)$ ;  $x^3 - x^2$ ,  $\sin 4x$ ,  $e^{-3x}$

## 6–13 GENERAL SOLUTION

Factor as in the text and solve. (Show the details.)

- $(D^2 - 5.5D + 6.66I)y = 0$
- $(D + 2I)^2y = 0$
- $(D^2 - 0.49I)y = 0$
- $(D^2 + 6D + 13I)y = 0$
- $(10D^2 + 2D + 1.7I)y = 0$

11.  $(D^2 + 4.1D + 3.1I)y = 0$

12.  $(4D^2 + 4\pi D + \pi^2 I)y = 0$

13.  $(D^2 + 17.64\omega^2 I)y = 0$

14. (**Double root**) If  $D^2 + aD + bI$  has distinct roots  $\mu$  and  $\lambda$ , show that a particular solution is  $y = (e^{\mu x} - e^{\lambda x})/(\mu - \lambda)$ . Obtain from this a solution  $xe^{\lambda x}$  by letting  $\mu \rightarrow \lambda$  and applying l'Hôpital's rule.

15. (**Linear operator**) Illustrate the linearity of  $L$  in (2) by taking  $c = 4$ ,  $k = -6$ ,  $y = e^{2x}$ , and  $w = \cos 2x$ . Prove that  $L$  is linear.

16. (**Definition of linearity**) Show that the definition of linearity in the text is equivalent to the following. If  $L[y]$  and  $L[w]$  exist, then  $L[y + w]$  exists and  $L[cy]$  and  $L[kw]$  exist for all constants  $c$  and  $k$ , and  $L[y + w] = L[y] + L[w]$  as well as  $L[cy] = cL[y]$  and  $L[kw] = kL[w]$ .

## 2.4 Modeling: Free Oscillations (Mass–Spring System)

Linear ODEs with constant coefficients have important applications in mechanics, as we show now (and in Sec. 2.8), and in electric circuits (to be shown in Sec. 2.9). In this section we consider a basic mechanical system, a mass on an elastic spring (“mass–spring system,” Fig. 32), which moves up and down. Its model will be a homogeneous linear ODE.

### Setting Up the Model

We take an ordinary spring that resists compression as well extension and suspend it vertically from a fixed support, as shown in Fig. 32. At the lower end of the spring we

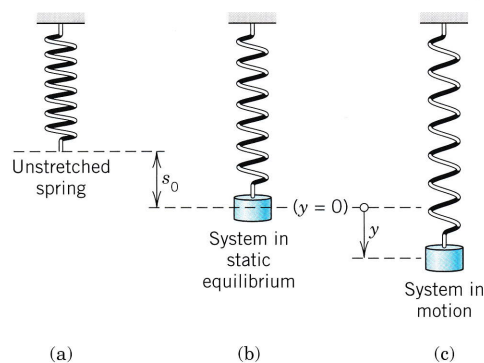


Fig. 32. Mechanical mass–spring system

attach a body of mass  $m$ . We assume  $m$  to be so large that we can neglect the mass of the spring. If we pull the body down a certain distance and then release it, it starts moving. We assume that it moves strictly vertically.

How can we obtain the motion of the body, say, the displacement  $y(t)$  as function of time  $t$ ? Now this motion is determined by **Newton's second law**

$$(1) \quad \text{Mass} \times \text{Acceleration} = my'' = \text{Force}$$

where  $y'' = d^2y/dt^2$  and "Force" is the resultant of all the forces acting on the body.

(For systems of units and conversion factors, see the inside of the front cover.)

We choose the **downward direction as the positive direction**, thus regarding downward forces as positive and upward forces as negative.

Consider Fig. 32. The spring is first unstretched. We now attach the body. This stretches the spring by an amount  $s_0$  shown in the figure. It causes an upward force  $F_0$  in the spring. Experiments show that  $F_0$  is proportional to the stretch  $s_0$ , say,

$$(2) \quad F_0 = -ks_0 \quad (\text{Hooke's law}^2).$$

$k$  ( $> 0$ ) is called the **spring constant** (or *spring modulus*). The minus sign indicates that  $F_0$  points upward, in our negative direction. Stiff springs have large  $k$ . (Explain!)

The extension  $s_0$  is such that  $F_0$  in the spring balances the weight  $W = mg$  of the body (where  $g = 980 \text{ cm/sec}^2 = 32.17 \text{ ft/sec}^2$  is the gravitational constant). Hence  $F_0 + W = -ks_0 + mg = 0$ . These forces will not affect the motion. Spring and body are again at rest. This is called the **static equilibrium** of the system (Fig. 32b). We measure the displacement  $y(t)$  of the body from this 'equilibrium point' as the origin  $y = 0$ , downward positive and upward negative.

From the position  $y = 0$  we pull the body downward. This further stretches the spring by some amount  $y > 0$  (the distance we pull it down). By Hooke's law this causes an (additional) upward force  $F_1$  in the spring,

$$F_1 = -ky.$$

$F_1$  is a **restoring force**. It has the tendency to *restore* the system, that is, to pull the body back to  $y = 0$ .

## Undamped System: ODE and Solution

Every system has damping—otherwise it would keep moving forever. But practically, the effect of damping may often be negligible, for example, for the motion of an iron ball on a spring during a few minutes. Then  $F_1$  is the only force in (1) causing the motion. Hence (1) gives the model  $my'' = -ky$  or

$$(3) \quad my'' + ky = 0.$$

<sup>2</sup>ROBERT HOOKE (1635–1703), English physicist, a forerunner of Newton with respect to the law of gravitation.

By the method in Sec. 2.2 (see Example 6) we obtain as a general solution

$$(4) \quad y(t) = A \cos \omega_0 t + B \sin \omega_0 t, \quad \omega_0 = \sqrt{\frac{k}{m}}.$$

The corresponding motion is called a **harmonic oscillation**.

Since the trigonometric functions in (4) have the period  $2\pi/\omega_0$ , the body executes  $\omega_0/2\pi$  cycles per second. This is the **frequency** of the oscillation, which is also called the **natural frequency** of the system. It is measured in cycles per second. Another name for cycles/sec is hertz (Hz).<sup>3</sup>

The sum in (4) can be combined into a phase-shifted cosine with amplitude  $C = \sqrt{A^2 + B^2}$  and phase angle  $\delta = \arctan(B/A)$ ,

$$(4^*) \quad y(t) = C \cos(\omega_0 t - \delta).$$

To verify this, apply the addition formula for the cosine [(6) in App. 3.1] to (4\*) and then compare with (4). Equation (4) is simpler in connection with initial value problems, whereas (4\*) is physically more informative because it exhibits the amplitude and phase of the oscillation.

Figure 33 shows typical forms of (4) and (4\*), all corresponding to some positive initial displacement  $y(0)$  [which determines  $A = y(0)$  in (4)] and different initial velocities  $y'(0)$  [which determine  $B = y'(0)/\omega_0$ ].

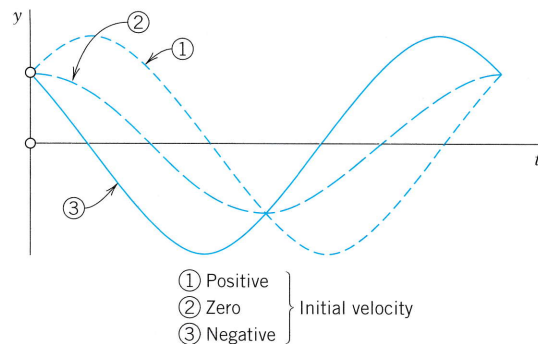


Fig. 33. Harmonic oscillations

### EXAMPLE 1 Undamped Motion. Harmonic Oscillation

If an iron ball of weight  $W = 98$  nt (about 22 lb) stretches a spring 1.09 m (about 43 in.), how many cycles per minute will this mass–spring system execute? What will its motion be if we pull down the weight an additional 16 cm (about 6 in.) and let it start with zero initial velocity?

**Solution.** Hooke's law (2) with  $W$  as the force and 1.09 meter as the stretch gives  $W = 1.09k$ ; thus  $k = W/1.09 = 98/1.09 = 90$  [kg/sec<sup>2</sup>] = 90 [nt/meter]. The mass is  $m = W/g = 98/9.8 = 10$  [kg]. This gives the frequency  $\omega_0/(2\pi) = \sqrt{k/m}/(2\pi) = 3/(2\pi) = 0.48$  [Hz] = 29 [cycles/min].

<sup>3</sup>HEINRICH HERTZ (1857–1894), German physicist, who discovered electromagnetic waves, as the basis of wireless communication developed by GUGLIELMO MARCONI (1874–1937), Italian physicist (Nobel prize in 1909).



From (4) and the initial conditions,  $y(0) = A = 0.16$  [meter] and  $y'(0) = \omega_0 B = 0$ . Hence the motion is

$$y(t) = 0.16 \cos 3t \text{ [meter]} \quad \text{or} \quad 0.52 \cos 3t \text{ [ft]} \quad (\text{Fig. 34}).$$

If you have a chance of experimenting with a mass–spring system, don't miss it. You will be surprised about the good agreement between theory and experiment, usually within a fraction of one percent if you measure carefully. ■

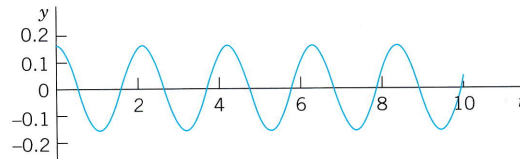


Fig. 34. Harmonic oscillation in Example 1

## Damped System: ODE and Solutions

We now add a **damping force**

$$F_2 = -cy'$$

to our model  $my'' = -ky$ , so that we have  $my'' = -ky - cy'$  or

$$(5) \quad my'' + cy' + ky = 0.$$

Physically this can be done by connecting the body to a dashpot; see Fig. 35. We assume this new force to be proportional to the velocity  $y' = dy/dt$ , as shown. This is generally a good approximation, at least for small velocities.

$c$  is called the **damping constant**. We show that  $c$  is positive. If at some instant,  $y'$  is positive, the body is moving downward (which is the positive direction). Hence the damping force  $F_2 = -cy'$ , always acting *against* the direction of motion, must be an upward force, which means that it must be negative,  $F_2 = -cy' < 0$ , so that  $-c < 0$  and  $c > 0$ . For an upward motion,  $y' < 0$  and we have a downward  $F_2 = -cy > 0$ ; hence  $-c < 0$  and  $c > 0$ , as before.

The ODE (5) is homogeneous linear and has constant coefficients. Hence we can solve it by the method in Sec. 2.2. The characteristic equation is (divide (5) by  $m$ )

$$\lambda^2 + \frac{c}{m} \lambda + \frac{k}{m} = 0.$$

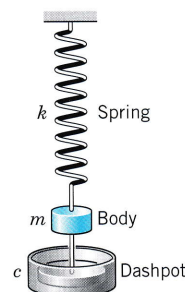


Fig. 35. Damped system

By the usual formula for the roots of a quadratic equation we obtain, as in Sec. 2.2,

$$(6) \quad \lambda_1 = -\alpha + \beta, \quad \lambda_2 = -\alpha - \beta, \quad \text{where} \quad \alpha = \frac{c}{2m} \quad \text{and} \quad \beta = \frac{1}{2m} \sqrt{c^2 - 4mk}.$$

It is now most interesting that depending on the amount of damping (much, medium, or little) there will be three types of motion corresponding to the three Cases I, II, III in Sec. 2.2:

- |                  |              |   |                           |
|------------------|--------------|---|---------------------------|
| <b>Case I.</b>   | $c^2 > 4mk.$ | <i>Distinct real roots <math>\lambda_1, \lambda_2.</math></i> | <b>(Overdamping)</b>      |
| <b>Case II.</b>  | $c^2 = 4mk.$ | <i>A real double root.</i>                                    | <b>(Critical damping)</b> |
| <b>Case III.</b> | $c^2 < 4mk.$ | <i>Complex conjugate roots.</i>                               | <b>(Underdamping)</b>     |

## Discussion of the Three Cases

### Case I. Overdamping

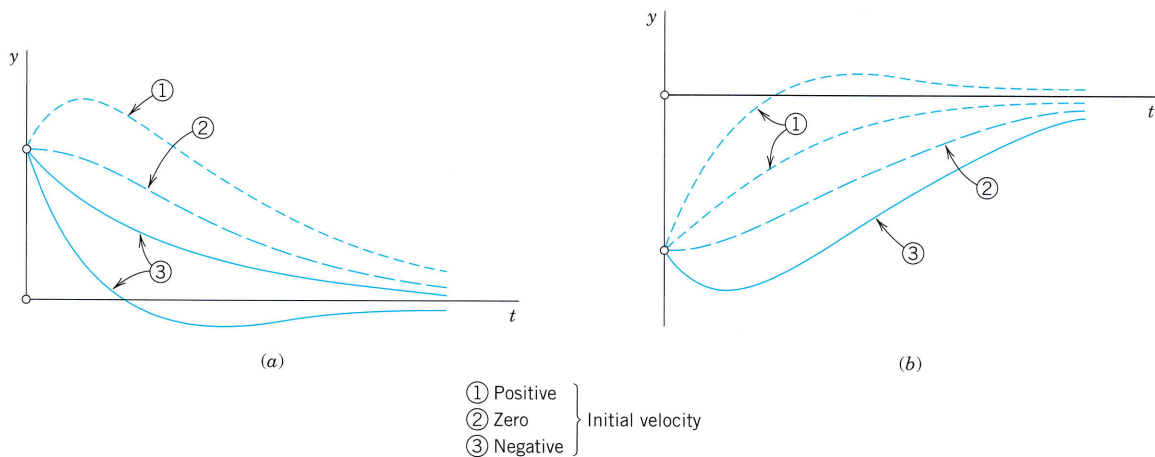
If the damping constant  $c$  is so large that  $c^2 > 4mk$ , then  $\lambda_1$  and  $\lambda_2$  are distinct real roots. In this case the corresponding general solution of (5) is

$$(7) \quad y(t) = c_1 e^{-(\alpha-\beta)t} + c_2 e^{-(\alpha+\beta)t}.$$

We see that in this case, damping takes out energy so quickly that the body does not oscillate. For  $t > 0$  both exponents in (7) are negative because  $\alpha > 0$ ,  $\beta > 0$ , and  $\beta^2 = \alpha^2 - k/m < \alpha^2$ . Hence both terms in (7) approach zero as  $t \rightarrow \infty$ . Practically speaking, after a sufficiently long time the mass will be at rest at the static equilibrium position ( $y = 0$ ). Figure 36 shows (7) for some typical initial conditions.

### Case II. Critical Damping

Critical damping is the border case between nonoscillatory motions (Case I) and oscillations (Case III). It occurs if the characteristic equation has a double root, that is, if  $c^2 = 4mk$ ,



**Fig. 36.** Typical motions (7) in the overdamped case  
 (a) Positive initial displacement  
 (b) Negative initial displacement

so that  $\beta = 0$ ,  $\lambda_1 = \lambda_2 = -\alpha$ . Then the corresponding general solution of (5) is

$$(8) \quad y(t) = (c_1 + c_2 t)e^{-\alpha t}.$$

This solution can pass through the equilibrium position  $y = 0$  at most once because  $e^{-\alpha t}$  is never zero and  $c_1 + c_2 t$  can have at most one positive zero. If both  $c_1$  and  $c_2$  are positive (or both negative), it has no positive zero, so that  $y$  does not pass through 0 at all. Figure 37 shows typical forms of (8). Note that they look almost like those in the previous figure.

### Case III. Underdamping

This is the most interesting case. It occurs if the damping constant  $c$  is so small that  $c^2 < 4mk$ . Then  $\beta$  in (6) is no longer real but pure imaginary, say,

$$(9) \quad \beta = i\omega^* \quad \text{where} \quad \omega^* = \frac{1}{2m} \sqrt{4mk - c^2} = \sqrt{\frac{k}{m} - \frac{c^2}{4m^2}} \quad (> 0).$$

(We write  $\omega^*$  to reserve  $\omega$  for driving and electromotive forces in Secs. 2.8 and 2.9.) The roots of the characteristic equation are now complex conjugate,

$$\lambda_1 = -\alpha + i\omega^*, \quad \lambda_2 = -\alpha - i\omega^*$$

with  $\alpha = c/(2m)$ , as given in (6). Hence the corresponding general solution is

$$(10) \quad y(t) = e^{-\alpha t}(A \cos \omega^* t + B \sin \omega^* t) = Ce^{-\alpha t} \cos(\omega^* t - \delta)$$

where  $C^2 = A^2 + B^2$  and  $\tan \delta = B/A$ , as in (4\*).

This represents **damped oscillations**. Their curve lies between the dashed curves  $y = Ce^{-\alpha t}$  and  $y = -Ce^{-\alpha t}$  in Fig. 38, touching them when  $\omega^* t - \delta$  is an integer multiple of  $\pi$  because these are the points at which  $\cos(\omega^* t - \delta)$  equals 1 or  $-1$ .

The frequency is  $\omega^*/(2\pi)$  Hz (hertz, cycles/sec). From (9) we see that the smaller  $c$  ( $> 0$ ) is, the larger is  $\omega^*$  and the more rapid the oscillations become. If  $c$  approaches 0, then  $\omega^*$  approaches  $\omega_0 = \sqrt{k/m}$ , giving the harmonic oscillation (4), whose frequency  $\omega_0/(2\pi)$  is the natural frequency of the system.

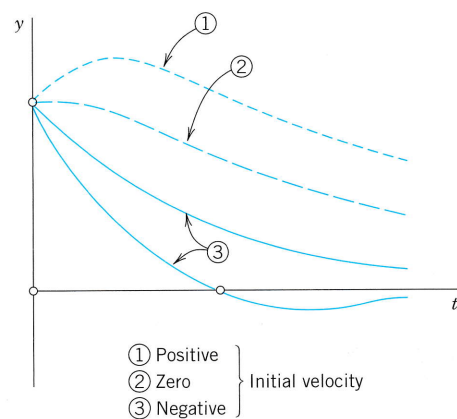


Fig. 37. Critical damping [see (8)]

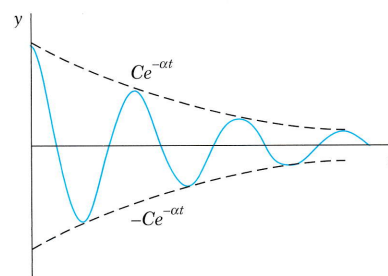


Fig. 38. Damped oscillation in Case III [see (10)]

**EXAMPLE 2 The Three Cases of Damped Motion**

How does the motion in Example 1 change if we change the damping constant  $c$  to one of the following three values, with  $y(0) = 0.16$  and  $y'(0) = 0$  as before?

$$(I) c = 100 \text{ kg/sec}, \quad (II) c = 60 \text{ kg/sec}, \quad (III) c = 10 \text{ kg/sec}.$$

**Solution.** It is interesting to see how the behavior of the system changes due to the effect of the damping, which takes energy from the system, so that the oscillations decrease in amplitude (Case III) or even disappear (Cases II and I).

(I) With  $m = 10$  and  $k = 90$ , as in Example 1, the model is the initial value problem

$$10y'' + 100y' + 90y = 0, \quad y(0) = 0.16 \text{ [meter]}, \quad y'(0) = 0.$$

The characteristic equation is  $10\lambda^2 + 100\lambda + 90 = 10(\lambda + 9)(\lambda + 1) = 0$ . It has the roots  $-9$  and  $-1$ . This gives the general solution

$$y = c_1 e^{-9t} + c_2 e^{-t}. \quad \text{We also need} \quad y' = -9c_1 e^{-9t} - c_2 e^{-t}.$$

The initial conditions give  $c_1 + c_2 = 0.16$ ,  $-9c_1 - c_2 = 0$ . The solution is  $c_1 = -0.02$ ,  $c_2 = 0.18$ . Hence in the overdamped case the solution is

$$y = -0.02e^{-9t} + 0.18e^{-t}.$$

It approaches 0 as  $t \rightarrow \infty$ . The approach is rapid; after a few seconds the solution is practically 0, that is, the iron ball is at rest.

(II) The model is as before, with  $c = 60$  instead of 100. The characteristic equation now has the form  $10\lambda^2 + 60\lambda + 90 = 10(\lambda + 3)^2 = 0$ . It has the double root  $-3$ . Hence the corresponding general solution is

$$y = (c_1 + c_2 t)e^{-3t}. \quad \text{We also need} \quad y' = (c_2 - 3c_1 - 3c_2 t)e^{-3t}.$$

The initial conditions give  $y(0) = c_1 = 0.16$ ,  $y'(0) = c_2 - 3c_1 = 0$ ,  $c_2 = 0.48$ . Hence in the critical case the solution is

$$y = (0.16 + 0.48t)e^{-3t}.$$

It is always positive and decreases to 0 in a monotone fashion.

(III) The model now is  $10y'' + 10y' + 90y = 0$ . Since  $c = 10$  is smaller than the critical  $c$ , we shall get oscillations. The characteristic equation is  $10\lambda^2 + 10\lambda + 90 = 10[(\lambda + \frac{1}{2})^2 + 9 - \frac{1}{4}] = 0$ . It has the complex roots [see (4) in Sec. 2.2 with  $a = 1$  and  $b = 9$ ]

$$\lambda = -0.5 \pm \sqrt{0.5^2 - 9} = -0.5 \pm 2.96i.$$

This gives the general solution

$$y = e^{-0.5t}(A \cos 2.96t + B \sin 2.96t).$$

Thus  $y(0) = A = 0.16$ . We also need the derivative

$$y' = e^{-0.5t}(-0.5A \cos 2.96t - 0.5B \sin 2.96t - 2.96A \sin 2.96t + 2.96B \cos 2.96t).$$

Hence  $y'(0) = -0.5A + 2.96B = 0$ ,  $B = 0.5A/2.96 = 0.027$ . This gives the solution

$$y = e^{-0.5t}(0.16 \cos 2.96t + 0.027 \sin 2.96t) = 0.162e^{-0.5t} \cos(2.96t - 0.17).$$

We see that these damped oscillations have a smaller frequency than the harmonic oscillations in Example 1 by about 1% (since 2.96 is smaller than 3.00 by about 1%). Their amplitude goes to zero. See Fig. 39. ■

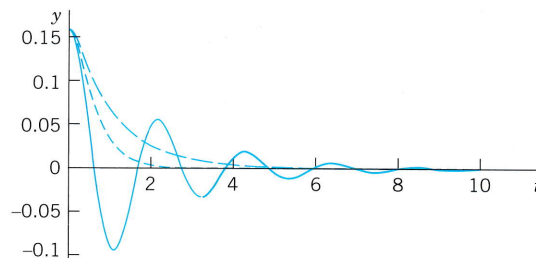


Fig. 39. The three solutions in Example 2

This section concerned *free motions* of mass-spring systems. Their models are *homogeneous* linear ODEs. *Nonhomogeneous* linear ODEs will arise as models of **forced motions**, that is, motions under the influence of a “driving force”. We shall study them in Sec. 2.8, after we have learned how to solve those ODEs.

## PROBLEM SET 2.4

### 1–8 MOTION WITHOUT DAMPING (HARMONIC OSCILLATIONS)

- (Initial value problem)** Find the harmonic motion (4) that starts from  $y_0$  with initial velocity  $v_0$ . Graph or sketch the solutions for  $\omega_0 = \pi$ ,  $y_0 = 1$ , and various  $v_0$  of your choice on common axes. At what  $t$ -values do all these curves intersect? Why?
- (Spring combinations)** Find the frequency of vibration of a ball of mass  $m = 3$  kg on a spring of modulus (i)  $k_1 = 27$  nt/m, (ii)  $k_2 = 75$  nt/m, (iii) on these springs in parallel (see Fig. 40), (iv) in series, that is, the ball hangs on one spring, which in turn hangs on the other spring.
- (Pendulum)** Find the frequency of oscillation of a pendulum of length  $L$  (Fig. 41), neglecting air resistance and the weight of the rod, and assuming  $\theta$  to be so small that  $\sin \theta$  practically equals  $\theta$ .
- (Frequency)** What is the frequency of a harmonic oscillation if the static equilibrium position of the ball is 10 cm lower than the lower end of the spring before the ball is attached?
- (Initial velocity)** Could you make a harmonic oscillation move faster by giving the body a greater initial push?
- (Archimedian principle)** This principle states that the buoyancy force equals the weight of the water displaced by the body (partly or totally submerged). The cylindrical buoy of diameter 60 cm in Fig. 42 is floating in water with its axis vertical. When depressed downward in the water and released, it vibrates with period 2 sec. What is its weight?



Fig. 40. Parallel springs (Problem 2)

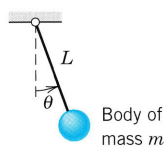


Fig. 41. Pendulum (Problem 3)

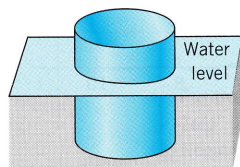


Fig. 42. Buoy (Problem 6)

- (Frequency)** How does the frequency of a harmonic motion change if we take (i) a spring of three times the modulus, (ii) a heavier ball?

- TEAM PROJECT. Harmonic Motions in Different Physical Systems.** Different physical or other systems may have the same or similar models, thus showing the *unifying power of mathematical methods*. Illustrate this for the systems in Figs. 43–45.

(a) **Flat spring** (Fig. 43). The spring is horizontally clamped at one end, and a body of weight 25 nt (about 5.6 lb) is attached at the other end. Find the motion of the system, assuming that its static equilibrium is 2 cm below the horizontal line, we let the system start from this position with initial velocity 15 cm/sec, and damping is negligible.

(b) **Torsional vibrations** (Fig. 44). Undamped torsional vibrations (rotations back and forth) of a wheel attached to an elastic thin rod are modeled by the ODE  $I_0\theta'' + K\theta = 0$ , where  $\theta$  is the angle measured from the state of equilibrium,  $I_0$  is the polar moment of inertia of the wheel about its center, and  $K$  is the torsional stiffness of the rod. Solve this ODE for  $K/I_0 = 17.64 \text{ sec}^{-2}$ , initial angle  $45^\circ$ , and initial angular velocity  $15^\circ \text{ sec}^{-1}$ .

(c) **Water in a tube** (Fig. 45). What is the frequency of vibration of 5 liters of water (about 1.3 gal) in a U-shaped tube of diameter 4 cm, neglecting friction?

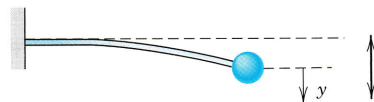


Fig. 43. Flat spring (Project 8a)

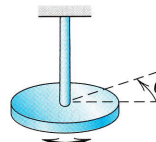


Fig. 44. Torsional vibrations (Project 8b)

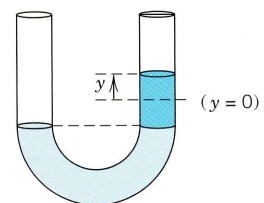


Fig. 45. Tube (Project 8c)

### 9–17 DAMPED MOTION

- (Frequency)** Find an approximation formula for  $\omega^*$  in terms of  $\omega_0$  by applying the binomial theorem in (9) and retaining only the first two terms. How good is the approximation in Example 2, III?

10. **(Extrema)** Find the location of the maxima and minima of  $y = e^{-2t} \cos t$  obtained approximately from a graph of  $y$  and compare it with the exact values obtained by calculation.
11. **(Maxima)** Show that the maxima of an underdamped motion occur at equidistant  $t$ -values and find the distance.
12. **(Logarithmic decrement)** Show that the ratio of two consecutive maximum amplitudes of a damped oscillation (10) is constant, and the natural logarithm of this ratio, called the *logarithmic decrement*, equals  $\Delta = 2\pi\alpha/\omega^*$ . Find  $\Delta$  for the solutions of  $y'' + 2y' + 5y = 0$ .
13. **(Shock absorber)** What is the smallest value of the damping constant of a shock absorber in the suspension of a wheel of a car (consisting of a spring and an absorber) that will provide (theoretically) an oscillation-free ride if the mass of the car is 2000 kg and the spring constant equals 4500 kg/sec<sup>2</sup>?
14. **(Damping constant)** Consider an underdamped motion of a body of mass  $m = 2$  kg. If the time between two consecutive maxima is 2 sec and the maximum amplitude decreases to  $\frac{1}{4}$  of its initial value after 15 cycles, what is the damping constant of the system?
15. **(Initial value problem)** Find the critical motion (8) that starts from  $y_0$  with initial velocity  $v_0$ . Graph solution curves for  $\alpha = 1$ ,  $y_0 = 1$  and several  $v_0$  such that (i) the curve does not intersect the  $t$ -axis, (ii) it intersects it at  $t = 1, 2, \dots, 5$ , respectively.
16. **(Initial value problem)** Find the overdamped motion (7) that starts from  $y_0$  with initial velocity  $v_0$ .
17. **(Overdamping)** Show that in the overdamped case, the body can pass through  $y = 0$  at most once.
18. **CAS PROJECT. Transition Between Cases I, II, III.** Study this transition in terms of graphs of typical solutions. (Cf. Fig. 46.)

(a) **Avoiding unnecessary generality is part of good modeling.** Decide that the initial value problems (A) and (B),

$$(A) \quad y'' + cy' + y = 0, \quad y(0) = 1, \quad y'(0) = 0$$

(B) the same with different  $c$  and  $y'(0) = -2$  (instead of 0), will give practically as much information as a problem with other  $m, k, y(0), y'(0)$ .

(b) **Consider (A).** Choose suitable values of  $c$ , perhaps better ones than in Fig. 46 for the transition from Case III to II and I. Guess  $c$  for the curves in the figure.

(c) **Time to go to rest.** Theoretically, this time is infinite (why?). Practically, the system is at rest when its motion has become very small, say, less than 0.1% of the initial displacement (this choice being up to us), that is in our case,

$$(11) \quad |y(t)| < 0.001 \quad \text{for all } t \text{ greater than some } t_1.$$

In engineering constructions, damping can often be varied without too much trouble. Experimenting with your graphs, find empirically a relation between  $t_1$  and  $c$ .

(d) **Solve (A) analytically.** Give a reason why the solution  $c$  of  $y(t_2) = -0.001$ , with  $t_2$  the solution of  $y'(t) = 0$ , will give you the best possible  $c$  satisfying (11).

(e) Consider (B) empirically as in (a) and (b). What is the main difference between (B) and (A)?

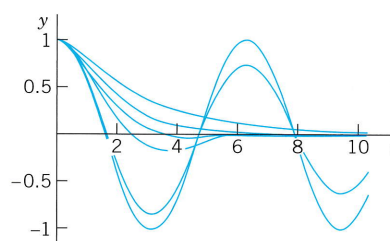


Fig. 46. CAS Project 18

## 2.5 Euler–Cauchy Equations

Euler–Cauchy equations<sup>4</sup> are ODEs of the form

$$(1) \quad x^2 y'' + axy' + by = 0$$

<sup>4</sup>LEONHARD EULER (1707–1783) was an enormously creative Swiss mathematician. He made fundamental contributions to almost all branches of mathematics and its application to physics. His important books on algebra and calculus contain numerous basic results of his own research. The great French mathematician AUGUSTIN LOUIS CAUCHY (1789–1857) is the father of modern analysis. He is the creator of complex analysis and had great influence on ODEs, PDEs, infinite series, elasticity theory, and optics.

with given constants  $a$  and  $b$  and unknown  $y(x)$ . We substitute

$$(2) \quad y = x^m$$

and its derivatives  $y' = mx^{m-1}$  and  $y'' = m(m-1)x^{m-2}$  into (1). This gives

$$x^2m(m-1)x^{m-2} + axmx^{m-1} + bx^m = 0.$$

We now see that (2) was a rather natural choice because we have obtained a common factor  $x^m$ . Dropping it, we have the auxiliary equation  $m(m-1) + am + b = 0$  or

$$(3) \quad m^2 + (a-1)m + b = 0. \quad (\text{Note: } a-1, \text{ not } a.)$$

Hence  $y = x^m$  is a solution of (1) if and only if  $m$  is a root of (3). The roots of (3) are

$$(4) \quad m_1 = \frac{1}{2}(1-a) + \sqrt{\frac{1}{4}(1-a)^2 - b}, \quad m_2 = \frac{1}{2}(1-a) - \sqrt{\frac{1}{4}(1-a)^2 - b}.$$

**Case I.** If the roots  $m_1$  and  $m_2$  are real and different, then solutions are

$$y_1(x) = x^{m_1} \quad \text{and} \quad y_2(x) = x^{m_2}$$

They are linearly independent since their quotient is not constant. Hence they constitute a basis of solutions of (1) for all  $x$  for which they are real. The corresponding general solution for all these  $x$  is

$$(5) \quad y = c_1x^{m_1} + c_2x^{m_2} \quad (c_1, c_2 \text{ arbitrary}).$$

### EXAMPLE 1 General Solution in the Case of Different Real Roots

The Euler–Cauchy equation

$$x^2y'' + 1.5xy' - 0.5y = 0$$

has the auxiliary equation

$$m^2 + 0.5m - 0.5 = 0. \quad (\text{Note: } 0.5, \text{ not } 1.5!)$$

The roots are 0.5 and  $-1$ . Hence a basis of solutions for all positive  $x$  is  $y_1 = x^{0.5}$  and  $y_2 = 1/x$  and gives the general solution

$$y = c_1\sqrt{x} + \frac{c_2}{x} \quad (x > 0). \quad \blacksquare$$

**Case II.** Equation (4) shows that the auxiliary equation (3) has a double root  $m_1 = \frac{1}{2}(1-a)$  if and only if  $(1-a)^2 - 4b = 0$ . The Euler–Cauchy equation (1) then has the form

$$(6) \quad x^2y'' + axy' + \frac{1}{4}(1-a)^2y = 0.$$

A solution is  $y_1 = x^{(1-a)/2}$ . To obtain a second linearly independent solution, we apply the method of reduction of order from Sec. 2.1 as follows. Starting from  $y_2 = uy_1$ , we obtain for  $u$  the expression (9), Sec. 2.1, namely,

$$u = \int U dx \quad \text{where} \quad U = \frac{1}{y_1^2} \exp\left(-\int p dx\right).$$

Here it is crucial that  $p$  is taken from the ODE written in standard form, in our case,

$$(6^*) \quad y'' + \frac{a}{x} y' + \frac{(1-a)^2}{4x^2} y = 0.$$

This shows that  $p = a/x$  (not  $ax$ ). Hence its integral is  $a \ln x = \ln(x^a)$ , the exponential function in  $U$  is  $1/x^a$ , and division by  $y_1^2 = x^{1-a}$  gives  $U = 1/x$ , and  $u = \ln x$  by integration.

Thus, in this “critical case,” a basis of solutions for positive  $x$  is  $y_1 = x^m$  and  $y_2 = x^m \ln x$ , where  $m = \frac{1}{2}(1-a)$ . Linear independence follows from the fact that the quotient of these solutions is not constant. Hence, for all  $x$  for which  $y_1$  and  $y_2$  are defined and real, a general solution is

$$(7) \quad y = (c_1 + c_2 \ln x)x^m, \quad m = \frac{1}{2}(1-a).$$

### EXAMPLE 2 General Solution in the Case of a Double Root

The Euler–Cauchy equation  $x^2 y'' - 5xy' + 9y = 0$  has the auxiliary equation  $m^2 - 6m + 9 = 0$ . It has the double root  $m = 3$ , so that a general solution for all positive  $x$  is

$$y = (c_1 + c_2 \ln x)x^3. \quad \blacksquare$$

**Case III.** The case of complex roots is of minor practical importance, and it suffices to present an example that explains the derivation of real solutions from complex ones.

### EXAMPLE 3 Real General Solution in the Case of Complex Roots

The Euler–Cauchy equation

$$x^2 y'' + 0.6xy' + 16.04y = 0$$

has the auxiliary equation  $m^2 - 0.4m + 16.04 = 0$ . The roots are complex conjugate,  $m_1 = 0.2 + 4i$  and  $m_2 = 0.2 - 4i$ , where  $i = \sqrt{-1}$ . (We know from algebra that if a polynomial with real coefficients has complex roots, these are always conjugate.) Now use the trick of writing  $x = e^{\ln x}$  and obtain

$$\begin{aligned} x^{m_1} &= x^{0.2+4i} = x^{0.2}(e^{\ln x})^{4i} = x^{0.2}e^{(4 \ln x)i}, \\ x^{m_2} &= x^{0.2-4i} = x^{0.2}(e^{\ln x})^{-4i} = x^{0.2}e^{-(4 \ln x)i}. \end{aligned}$$

Next apply Euler’s formula (11) in Sec. 2.2 with  $t = 4 \ln x$  to these two formulas. This gives

$$\begin{aligned} x^{m_1} &= x^{0.2}[\cos(4 \ln x) + i \sin(4 \ln x)], \\ x^{m_2} &= x^{0.2}[\cos(4 \ln x) - i \sin(4 \ln x)]. \end{aligned}$$

Add these two formulas, so that the sine drops out, and divide the result by 2. Then subtract the second formula from the first, so that the cosine drops out, and divide the result by  $2i$ . This yields

$$x^{0.2} \cos(4 \ln x) \quad \text{and} \quad x^{0.2} \sin(4 \ln x)$$

respectively. By the superposition principle in Sec. 2.2 these are solutions of the Euler–Cauchy equation (1). Since their quotient  $\cot(4 \ln x)$  is not constant, they are linearly independent. Hence they form a basis of solutions, and the corresponding real general solution for all positive  $x$  is

$$(8) \quad y = x^{0.2}[A \cos(4 \ln x) + B \sin(4 \ln x)].$$

Figure 47 shows typical solution curves in the three cases discussed, in particular the basis functions in Examples 1 and 3. \blacksquare



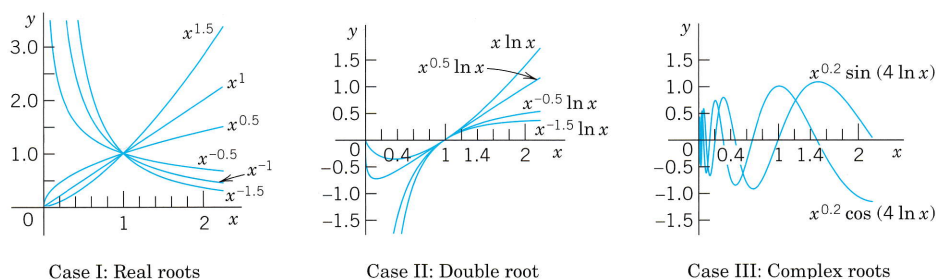


Fig. 47. Euler-Cauchy equations

**EXAMPLE 4** Boundary Value Problem. Electric Potential Field Between Two Concentric Spheres

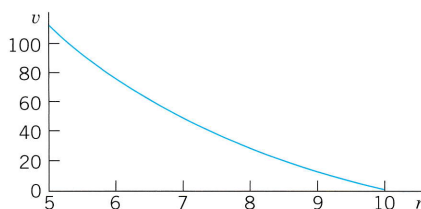
Find the electrostatic potential  $v = v(r)$  between two concentric spheres of radii  $r_1 = 5$  cm and  $r_2 = 10$  cm kept at potentials  $v_1 = 110$  V and  $v_2 = 0$ , respectively.

*Physical Information.*  $v(r)$  is a solution of the Euler-Cauchy equation  $rv'' + 2v' = 0$ , where  $v' = dv/dr$ .

**Solution.** The auxiliary equation is  $m^2 + m = 0$ . It has the roots 0 and  $-1$ . This gives the general solution  $v(r) = c_1 + c_2/r$ . From the "boundary conditions" (the potentials on the spheres) we obtain

$$v(5) = c_1 + \frac{c_2}{5} = 110, \quad v(10) = c_1 + \frac{c_2}{10} = 0.$$

By subtraction,  $c_2/10 = 110$ ,  $c_2 = 1100$ . From the second equation,  $c_1 = -c_2/10 = -110$ . *Answer:*  $v(r) = -110 + 1100/r$  V. Figure 48 shows that the potential is not a straight line, as it would be for a potential between two parallel plates. For example, on the sphere of radius 7.5 cm it is not  $110/2 = 55$  V, but considerably less. (What is it?) ■

Fig. 48. Potential  $v(r)$  in Example 4**PROBLEM SET 2.5****1-10** GENERAL SOLUTION

Find a real general solution, showing the details of your work.

- $x^2y'' - 6y = 0$
- $4x^2y'' + 4xy' - y = 0$
- $x^2y'' - 7xy' + 16y = 0$
- $x^2y'' + 3xy' + y = 0$
- $x^2y'' - xy' + 2y = 0$
- $2x^2y'' + 4xy' + 5y = 0$
- $(10x^2D^2 - 20xD + 22.4I)y = 0$
- $(4x^2D^2 + I)y = 0$
- $(100x^2D^2 + 9I)y = 0$
- $(10x^2D^2 + 6xD + 0.5I)y = 0$

**11-15** INITIAL VALUE PROBLEM

Solve and graph the solution, showing the details of your work.

- $x^2y'' - 4xy' + 6y = 0$ ,  $y(1) = 1$ ,  $y'(1) = 0$
- $x^2y'' + 3xy' + y = 0$ ,  $y(1) = 4$ ,  $y'(1) = -2$
- $(x^2D^2 + 2xD + 100.25I)y = 0$ ,  $y(1) = 2$ ,  $y'(1) = -11$
- $(x^2D^2 - 2xD + 2.25I)y = 0$ ,  $y(1) = 2.2$ ,  $y'(1) = 2.5$
- $(xD^2 + 4D)y = 0$ ,  $y(1) = 12$ ,  $y'(1) = -6$

**16. TEAM PROJECT. Double Root**

- (A) Derive a second linearly independent solution of (1) by reduction of order; but instead of using (9), Sec. 2.1, perform all steps directly for the present ODE (1).  
 (B) Obtain  $x^m \ln x$  by considering the solutions  $x^m$  and  $x^{m+s}$  of a suitable Euler–Cauchy equation and letting  $s \rightarrow 0$ .

(C) Verify by substitution that  $x^m \ln x$ ,  $m = (1 - a)/2$ , is a solution in the critical case.

(D) Transform the Euler–Cauchy equation (1) into an ODE with constant coefficients by setting  $x = e^t$  ( $x > 0$ ).

(E) Obtain a second linearly independent solution of the Euler–Cauchy equation in the “critical case” from that of a constant-coefficient ODE.

## 2.6 Existence and Uniqueness of Solutions. Wronskian

In this section we shall discuss the general theory of homogeneous linear ODEs

$$(1) \quad y'' + p(x)y' + q(x)y = 0$$

with continuous, but otherwise arbitrary *variable coefficients*  $p$  and  $q$ . This will concern the existence and form of a general solution of (1) as well as the uniqueness of the solution of initial value problems consisting of such an ODE and two initial conditions

$$(2) \quad y(x_0) = K_0, \quad y'(x_0) = K_1$$

with given  $x_0$ ,  $K_0$ , and  $K_1$ .

The two main results will be Theorem 1, stating that such an initial value problem always has a solution which is unique, and Theorem 4, stating that a general solution

$$(3) \quad y = c_1 y_1 + c_2 y_2 \quad (c_1, c_2 \text{ arbitrary})$$

includes all solutions. Hence *linear* ODEs with continuous coefficients have no “*singular solutions*” (solutions not obtainable from a general solution).

Clearly, no such theory was needed for constant-coefficient or Euler–Cauchy equations because everything resulted explicitly from our calculations.

Central to our present discussion is the following theorem.

**THEOREM 1****Existence and Uniqueness Theorem for Initial Value Problems**

*If  $p(x)$  and  $q(x)$  are continuous functions on some open interval  $I$  (see Sec. 1.1) and  $x_0$  is in  $I$ , then the initial value problem consisting of (1) and (2) has a unique solution  $y(x)$  on the interval  $I$ .*

The proof of existence uses the same prerequisites as the existence proof in Sec. 1.7 and will not be presented here; it can be found in Ref. [A11] listed in App. 1. Uniqueness proofs are usually simpler than existence proofs. But for Theorem 1, even the uniqueness proof is long, and we give it as an additional proof in App. 4.

## Linear Independence of Solutions

Remember from Sec. 2.1 that a general solution on an open interval  $I$  is made up from a **basis**  $y_1, y_2$  on  $I$ , that is, from a pair of linearly independent solutions on  $I$ . Here we call  $y_1, y_2$  **linearly independent** on  $I$  if the equation

$$(4) \quad k_1 y_1(x) + k_2 y_2(x) = 0 \quad \text{on } I \quad \text{implies} \quad k_1 = 0, \quad k_2 = 0.$$

We call  $y_1, y_2$  **linearly dependent** on  $I$  if this equation also holds for constants  $k_1, k_2$  not both 0. In this case, and only in this case,  $y_1$  and  $y_2$  are proportional on  $I$ , that is (see Sec. 2.1),

$$(5) \quad \text{(a) } y_1 = ky_2 \quad \text{or} \quad \text{(b) } y_2 = ly_1 \quad \text{for all } x \text{ on } I.$$

For our discussion the following criterion of linear independence and dependence of solutions will be helpful.

### THEOREM 2

#### Linear Dependence and Independence of Solutions

Let the ODE (1) have continuous coefficients  $p(x)$  and  $q(x)$  on an open interval  $I$ . Then two solutions  $y_1$  and  $y_2$  of (1) on  $I$  are linearly dependent on  $I$  if and only if their “Wronskian”

$$(6) \quad W(y_1, y_2) = y_1 y_2' - y_2 y_1'$$

is 0 at some  $x_0$  in  $I$ . Furthermore, if  $W = 0$  at an  $x = x_0$  in  $I$ , then  $W \equiv 0$  on  $I$ ; hence if there is an  $x_1$  in  $I$  at which  $W$  is not 0, then  $y_1, y_2$  are linearly independent on  $I$ .

**PROOF** (a) Let  $y_1$  and  $y_2$  be linearly dependent on  $I$ . Then (5a) or (5b) holds on  $I$ . If (5a) holds, then

$$W(y_1, y_2) = y_1 y_2' - y_2 y_1' = ky_2 y_2' - y_2 k y_2' = 0.$$

Similarly if (5b) holds.

(b) Conversely, we let  $W(y_1, y_2) = 0$  for some  $x = x_0$  and show that this implies linear dependence of  $y_1$  and  $y_2$  on  $I$ . We consider the linear system of equations in the unknowns  $k_1, k_2$

$$(7) \quad \begin{aligned} k_1 y_1(x_0) + k_2 y_2(x_0) &= 0 \\ k_1 y_1'(x_0) + k_2 y_2'(x_0) &= 0. \end{aligned}$$

To eliminate  $k_2$ , multiply the first equation by  $y_2'$  and the second by  $-y_2$  and add the resulting equations. This gives

$$k_1 y_1(x_0) y_2'(x_0) - k_1 y_1'(x_0) y_2(x_0) = k_1 W(y_1(x_0), y_2(x_0)) = 0.$$

Similarly, to eliminate  $k_1$ , multiply the first equation by  $-y_1'$  and the second by  $y_1$  and add the resulting equations. This gives

$$k_2 W(y_1(x_0), y_2(x_0)) = 0.$$

If  $W$  were not 0 at  $x_0$ , we could divide by  $W$  and conclude that  $k_1 = k_2 = 0$ . Since  $W$  is 0, division is not possible, and the system has a solution for which  $k_1$  and  $k_2$  are not both 0. Using *these numbers*  $k_1, k_2$ , we introduce the function

$$y(x) = k_1 y_1(x) + k_2 y_2(x).$$

Since (1) is homogeneous linear, Fundamental Theorem 1 in Sec. 2.1 (the superposition principle) implies that this function is a solution of (1) on  $I$ . From (7) we see that it satisfies the initial conditions  $y(x_0) = 0, y'(x_0) = 0$ . Now another solution of (1) satisfying the same initial conditions is  $y^* \equiv 0$ . Since the coefficients  $p$  and  $q$  of (1) are continuous, Theorem 1 applies and gives uniqueness, that is,  $y \equiv y^*$ , written out

$$k_1 y_1 + k_2 y_2 \equiv 0 \quad \text{on } I.$$

Now since  $k_1$  and  $k_2$  are not both zero, this means linear dependence of  $y_1, y_2$  on  $I$ .

(c) We prove the last statement of the theorem. If  $W(x_0) = 0$  at an  $x_0$  in  $I$ , we have linear dependence of  $y_1, y_2$  on  $I$  by part (b), hence  $W \equiv 0$  by part (a) of this proof. Hence in the case of linear dependence it cannot happen that  $W(x_1) \neq 0$  at an  $x_1$  in  $I$ . If it does happen, it thus implies linear independence as claimed. ■

**Remark. Determinants.** Students familiar with second-order determinants may have noticed that

$$W(y_1, y_2) = \begin{vmatrix} y_1 & y_2 \\ y_1' & y_2' \end{vmatrix} = y_1 y_2' - y_2 y_1'.$$

This determinant is called the *Wronski determinant*<sup>5</sup> or, briefly, the **Wronskian**, of two solutions  $y_1$  and  $y_2$  of (1), as has already been mentioned in (6). Note that its four entries occupy the same positions as in the linear system (7).

### EXAMPLE 1 Illustration of Theorem 2

The functions  $y_1 = \cos \omega x$  and  $y_2 = \sin \omega x$  are solutions of  $y'' + \omega^2 y = 0$ . Their Wronskian is

$$W(\cos \omega x, \sin \omega x) = \begin{vmatrix} \cos \omega x & \sin \omega x \\ -\omega \sin \omega x & \omega \cos \omega x \end{vmatrix} = y_1 y_2' - y_2 y_1' = \omega \cos^2 \omega x + \omega \sin^2 \omega x = \omega.$$

Theorem 2 shows that these solutions are linearly independent if and only if  $\omega \neq 0$ . Of course, we can see this directly from the quotient  $y_2/y_1 = \tan \omega x$ . For  $\omega = 0$  we have  $y_2 \equiv 0$ , which implies linear dependence (why?). ■

### EXAMPLE 2 Illustration of Theorem 2 for a Double Root

A general solution of  $y'' - 2y' + y = 0$  on any interval is  $y = (c_1 + c_2 x)e^x$ . (Verify!). The corresponding Wronskian is not 0, which shows linear independence of  $e^x$  and  $x e^x$  on any interval. Namely,

$$W(x, x e^x) = \begin{vmatrix} e^x & x e^x \\ e^x & (x+1)e^x \end{vmatrix} = (x+1)e^{2x} - x e^{2x} = e^{2x} \neq 0. \quad \blacksquare$$

<sup>5</sup>Introduced by WRONSKI (JOSEF MARIA HÖNE, 1776–1853), Polish mathematician.

## A General Solution of (1) Includes All Solutions

This will be our second main result, as announced at the beginning. Let us start with existence.

### THEOREM 3

#### Existence of a General Solution

If  $p(x)$  and  $q(x)$  are continuous on an open interval  $I$ , then (1) has a general solution on  $I$ .

**PROOF** By Theorem 1, the ODE (1) has a solution  $y_1(x)$  on  $I$  satisfying the initial conditions

$$y_1(x_0) = 1, \quad y_1'(x_0) = 0$$

and a solution  $y_2(x)$  on  $I$  satisfying the initial conditions

$$y_2(x_0) = 0, \quad y_2'(x_0) = 1.$$

The Wronskian of these two solutions has at  $x = x_0$  the value

$$W(y_1(x_0), y_2(x_0)) = y_1(x_0)y_2'(x_0) - y_2(x_0)y_1'(x_0) = 1.$$

Hence, by Theorem 2, these solutions are linearly independent on  $I$ . They form a basis of solutions of (1) on  $I$ , and  $y = c_1y_1 + c_2y_2$  with arbitrary  $c_1, c_2$  is a general solution of (1) on  $I$ , whose existence we wanted to prove. ■

We finally show that a general solution is as general as it can possibly be.

### THEOREM 4

#### A General Solution Includes All Solutions

If the ODE (1) has continuous coefficients  $p(x)$  and  $q(x)$  on some open interval  $I$ , then every solution  $y = Y(x)$  of (1) on  $I$  is of the form

$$(8) \quad Y(x) = C_1y_1(x) + C_2y_2(x)$$

where  $y_1, y_2$  is any basis of solutions of (1) on  $I$  and  $C_1, C_2$  are suitable constants.

Hence (1) does not have **singular solutions** (that is, solutions not obtainable from a general solution).

**PROOF** Let  $y = Y(x)$  be any solution of (1) on  $I$ . Now, by Theorem 3 the ODE (1) has a general solution

$$(9) \quad y(x) = c_1y_1(x) + c_2y_2(x)$$

on  $I$ . We have to find suitable values of  $c_1, c_2$  such that  $y(x) = Y(x)$  on  $I$ . We choose any  $x_0$  in  $I$  and show first that we can find values of  $c_1, c_2$  such that we reach agreement at  $x_0$ , that is,  $y(x_0) = Y(x_0)$  and  $y'(x_0) = Y'(x_0)$ . Written out in terms of (9), this becomes

$$(10) \quad \begin{aligned} (a) \quad c_1y_1(x_0) + c_2y_2(x_0) &= Y(x_0) \\ (b) \quad c_1y_1'(x_0) + c_2y_2'(x_0) &= Y'(x_0). \end{aligned}$$

We determine the unknowns  $c_1$  and  $c_2$ . To eliminate  $c_2$ , we multiply (10a) by  $y_2'(x_0)$  and (10b) by  $-y_2(x_0)$  and add the resulting equations. This gives an equation for  $c_1$ . Then we multiply (10a) by  $-y_1'(x_0)$  and (10b) by  $y_1(x_0)$  and add the resulting equations. This gives an equation for  $c_2$ . These new equations are as follows, where we take the values of  $y_1, y_1', y_2, y_2', Y, Y'$  at  $x_0$ ,

$$c_1(y_1 y_2' - y_2 y_1') = c_1 W(y_1, y_2) = Y y_2' - y_2 Y'$$

$$c_2(y_1 y_2' - y_2 y_1') = c_2 W(y_1, y_2) = y_1 Y' - Y y_1'$$

Since  $y_1, y_2$  is a basis, the Wronskian  $W$  in these equations is not 0, and we can solve for  $c_1$  and  $c_2$ . We call the (unique) solution  $c_1 = C_1, c_2 = C_2$ . By substituting it into (9) we obtain from (9) the particular solution

$$y^*(x) = C_1 y_1(x) + C_2 y_2(x).$$

Now since  $C_1, C_2$  is a solution of (10), we see from (10) that

$$y^*(x_0) = Y(x_0), \quad y^{*'}(x_0) = Y'(x_0).$$

From the uniqueness stated in Theorem 1 this implies that  $y^*$  and  $Y$  must be equal everywhere on  $I$ , and the proof is complete. ■

Looking back at the content of this section, we see that homogeneous linear ODEs with continuous variable coefficients have a conceptually and structurally rather transparent existence and uniqueness theory of solutions. Important in itself, this theory will also provide the foundation of an investigation of nonhomogeneous linear ODEs, whose theory and engineering applications we shall study in the remaining four sections of this chapter.

## PROBLEM SET 2.6

### 1-17 BASES OF SOLUTIONS. CORRESPONDING ODEs. WRONSKIANS

Find an ODE (1) for which the given functions are solutions. Show linear independence (a) by considering quotients, (b) by Theorem 2.

1.  $e^{0.5x}, e^{-0.5x}$
2.  $\cos \pi x, \sin \pi x$
3.  $e^{kx}, x e^{kx}$
4.  $x^3, x^{-2}$
5.  $x^{0.25}, x^{0.25} \ln x$
6.  $e^{3.4x}, e^{-2.5x}$
7.  $\cos(2 \ln x), \sin(2 \ln x)$
8.  $e^{-2x}, x e^{-2x}$
9.  $x^{1.5}, x^{-0.5}$
10.  $x^{-3}, x^{-3} \ln x$
11.  $\cosh 2.5x, \sinh 2.5x$
12.  $e^{-2x} \cos \omega x, e^{-2x} \sin \omega x$
13.  $e^{-x} \cos 0.8x, e^{-x} \sin 0.8x$
14.  $x^{-1} \cos(\ln x), x^{-1} \sin(\ln x)$
15.  $e^{-2.5x} \cos 0.3x, e^{-2.5x} \sin 0.3x$
16.  $e^{-kx} \cos \pi x, e^{-kx} \sin \pi x$
17.  $e^{-3.8\pi x}, x e^{-3.8\pi x}$

### 18. TEAM PROJECT. Consequences of the Present Theory.

This concerns some noteworthy general properties of solutions. Assume that the coefficients  $p$  and  $q$  of the ODE (1) are continuous on some open interval  $I$ , to which the subsequent statements refer.

(A) Solve  $y'' - y = 0$  (a) by exponential functions, (b) by hyperbolic functions. How are the constants in the corresponding general solutions related?

(B) Prove that the solutions of a basis cannot be 0 at the same point.

(C) Prove that the solutions of a basis cannot have a maximum or minimum at the same point.

(D) Express  $(y_2/y_1)'$  by a formula involving the Wronskian  $W$ . Why is it likely that such a formula should exist? Use it to find  $W$  in Prob. 10.

(E) Sketch  $y_1(x) = x^3$  if  $x \geq 0$  and 0 if  $x < 0$ ,  $y_2(x) = 0$  if  $x \geq 0$  and  $x^3$  if  $x < 0$ . Show linear independence on  $-1 < x < 1$ . What is their Wronskian? What Euler-Cauchy equation do  $y_1, y_2$  satisfy? Is there a contradiction to Theorem 2?

(F) Prove **Abel's formula**<sup>6</sup>

$$W(y_1(x), y_2(x)) = c \exp \left[ - \int_{x_0}^x p(t) dt \right]$$

where  $c = W(y_1(x_0), y_2(x_0))$ . Apply it to Prob. 12. *Hint:* Write (1) for  $y_1$  and for  $y_2$ . Eliminate  $q$  algebraically from these two ODEs, obtaining a first-order linear ODE. Solve it.

## 2.7 Nonhomogeneous ODEs

### Method of Undetermined Coefficients

*In this section we proceed from homogeneous to nonhomogeneous linear ODEs*

$$(1) \quad y'' + p(x)y' + q(x)y = r(x)$$

where  $r(x) \neq 0$ . We shall see that a “general solution” of (1) is the sum of a general solution of the corresponding homogeneous ODE

$$(2) \quad y'' + p(x)y' + q(x)y = 0$$

and a “particular solution” of (1). These two new terms “general solution of (1)” and “particular solution of (1)” are defined as follows.

#### DEFINITION

##### General Solution, Particular Solution

A **general solution** of the nonhomogeneous ODE (1) on an open interval  $I$  is a solution of the form

$$(3) \quad y(x) = y_h(x) + y_p(x);$$

here,  $y_h = c_1y_1 + c_2y_2$  is a general solution of the homogeneous ODE (2) on  $I$  and  $y_p$  is any solution of (1) on  $I$  containing no arbitrary constants.

A **particular solution** of (1) on  $I$  is a solution obtained from (3) by assigning specific values to the arbitrary constants  $c_1$  and  $c_2$  in  $y_h$ .

Our task is now twofold, first to justify these definitions and then to develop a method for finding a solution  $y_p$  of (1).

Accordingly, we first show that a general solution as just defined satisfies (1) and that the solutions of (1) and (2) are related in a very simple way.

#### THEOREM 1

##### Relations of Solutions of (1) to Those of (2)

- (a) *The sum of a solution  $y$  of (1) on some open interval  $I$  and a solution  $\tilde{y}$  of (2) on  $I$  is a solution of (1) on  $I$ . In particular, (3) is a solution of (1) on  $I$ .*
- (b) *The difference of two solutions of (1) on  $I$  is a solution of (2) on  $I$ .*

<sup>6</sup>NIELS HENRIK ABEL (1802–1829), Norwegian mathematician.

**PROOF** (a) Let  $L[y]$  denote the left side of (1). Then for any solutions  $y$  of (1) and  $\tilde{y}$  of (2) on  $I$ ,

$$L[y + \tilde{y}] = L[y] + L[\tilde{y}] = r + 0 = r.$$

(b) For any solutions  $y$  and  $y^*$  of (1) on  $I$  we have  $L[y - y^*] = L[y] - L[y^*] = r - r = 0$ . ■

Now for *homogeneous ODEs* (2) we know that general solutions include all solutions. We show that the same is true for nonhomogeneous ODEs (1).

### THEOREM 2

#### A General Solution of a Nonhomogeneous ODE Includes All Solutions

If the coefficients  $p(x)$ ,  $q(x)$ , and the function  $r(x)$  in (1) are continuous on some open interval  $I$ , then every solution of (1) on  $I$  is obtained by assigning suitable values to the arbitrary constants  $c_1$  and  $c_2$  in a general solution (3) of (1) on  $I$ .

**PROOF** Let  $y^*$  be any solution of (1) on  $I$  and  $x_0$  any  $x$  in  $I$ . Let (3) be any general solution of (1) on  $I$ . This solution exists. Indeed,  $y_h = c_1 y_1 + c_2 y_2$  exists by Theorem 3 in Sec. 2.6 because of the continuity assumption, and  $y_p$  exists according to a construction to be shown in Sec. 2.10. Now, by Theorem 1(b) just proved, the difference  $Y = y^* - y_p$  is a solution of (2) on  $I$ . At  $x_0$  we have

$$Y(x_0) = y^*(x_0) - y_p(x_0), \quad Y'(x_0) = y^{*'}(x_0) - y_p'(x_0).$$

Theorem 1 in Sec. 2.6 implies that for these conditions, as for any other initial conditions in  $I$ , there exists a unique particular solution of (2) obtained by assigning suitable values to  $c_1, c_2$  in  $y_h$ . From this and  $y^* = Y + y_p$  the statement follows. ■

## Method of Undetermined Coefficients

Our discussion suggests the following. *To solve the nonhomogeneous ODE (1) or an initial value problem for (1), we have to solve the homogeneous ODE (2) and find any solution  $y_p$  of (1), so that we obtain a general solution (3) of (1).*

How can we find a solution  $y_p$  of (1)? One method is the so-called **method of undetermined coefficients**. It is much simpler than another, more general method (to be discussed in Sec. 2.10). Since it applies to models of vibrational systems and electric circuits to be shown in the next two sections, it is frequently used in engineering.

More precisely, the method of undetermined coefficients is suitable for linear ODEs with *constant coefficients  $a$  and  $b$*

$$(4) \quad y'' + ay' + by = r(x)$$

when  $r(x)$  is an exponential function, a power of  $x$ , a cosine or sine, or sums or products of such functions. These functions have derivatives similar to  $r(x)$  itself. This gives the idea. We choose a form for  $y_p$  similar to  $r(x)$ , but with unknown coefficients to be determined by substituting that  $y_p$  and its derivatives into the ODE. Table 2.1 on p. 80 shows the choice of  $y_p$  for practically important forms of  $r(x)$ . Corresponding rules are as follows.



### Choice Rules for the Method of Undetermined Coefficients

- (a) **Basic Rule.** If  $r(x)$  in (4) is one of the functions in the first column in Table 2.1, choose  $y_p$  in the same line and determine its undetermined coefficients by substituting  $y_p$  and its derivatives into (4).
- (b) **Modification Rule.** If a term in your choice for  $y_p$  happens to be a solution of the homogeneous ODE corresponding to (4), multiply your choice of  $y_p$  by  $x$  (or by  $x^2$  if this solution corresponds to a double root of the characteristic equation of the homogeneous ODE).
- (c) **Sum Rule.** If  $r(x)$  is a sum of functions in the first column of Table 2.1, choose for  $y_p$  the sum of the functions in the corresponding lines of the second column.

The Basic Rule applies when  $r(x)$  is a single term. The Modification Rule helps in the indicated case, and to recognize such a case, we have to solve the homogeneous ODE first. The Sum Rule follows by noting that the sum of two solutions of (1) with  $r = r_1$  and  $r = r_2$  (and the same left side!) is a solution of (1) with  $r = r_1 + r_2$ . (Verify!)

The method is self-correcting. A false choice for  $y_p$  or one with too few terms will lead to a contradiction. A choice with too many terms will give a correct result, with superfluous coefficients coming out zero.

Let us illustrate Rules (a)–(c) by the typical Examples 1–3.

**Table 2.1** Method of Undetermined Coefficients

Term in $r(x)$	Choice for $y_p(x)$
$ke^{\gamma x}$	$Ce^{\gamma x}$
$kx^n$ ( $n = 0, 1, \dots$ )	$K_n x^n + K_{n-1} x^{n-1} + \dots + K_1 x + K_0$
$k \cos \omega x$	} $K \cos \omega x + M \sin \omega x$
$k \sin \omega x$	
$ke^{\alpha x} \cos \omega x$	} $e^{\alpha x}(K \cos \omega x + M \sin \omega x)$
$ke^{\alpha x} \sin \omega x$	

#### EXAMPLE 1 Application of the Basic Rule (a)

Solve the initial value problem

$$(5) \quad y'' + y = 0.001x^2, \quad y(0) = 0, \quad y'(0) = 1.5.$$

**Solution.** *Step 1. General solution of the homogeneous ODE.* The ODE  $y'' + y = 0$  has the general solution

$$y_h = A \cos x + B \sin x.$$

*Step 2. Solution  $y_p$  of the nonhomogeneous ODE.* We first try  $y_p = Kx^2$ . Then  $y_p'' = 2K$ . By substitution,  $2K + Kx^2 = 0.001x^2$ . For this to hold for all  $x$ , the coefficient of each power of  $x$  ( $x^2$  and  $x^0$ ) must be the same on both sides; thus  $K = 0.001$  and  $2K = 0$ , a contradiction.

The second line in Table 2.1 suggests the choice

$$y_p = K_2 x^2 + K_1 x + K_0. \quad \text{Then} \quad y_p'' + y_p = 2K_2 + K_2 x^2 + K_1 x + K_0 = 0.001x^2.$$

Equating the coefficients of  $x^2$ ,  $x$ ,  $x^0$  on both sides, we have  $K_2 = 0.001$ ,  $K_1 = 0$ ,  $2K_2 + K_0 = 0$ . Hence  $K_0 = -2K_2 = -0.002$ . This gives  $y_p = 0.001x^2 - 0.002$ , and

$$y = y_h + y_p = A \cos x + B \sin x + 0.001x^2 - 0.002.$$

**Step 3. Solution of the initial value problem.** Setting  $x = 0$  and using the first initial condition gives  $y(0) = A - 0.002 = 0$ , hence  $A = 0.002$ . By differentiation and from the second initial condition,

$$y' = y'_h + y'_p = -A \sin x + B \cos x + 0.002x \quad \text{and} \quad y'(0) = B = 1.5.$$

This gives the answer (Fig. 49)

$$y = 0.002 \cos x + 1.5 \sin x + 0.001x^2 - 0.002.$$

Figure 49 shows  $y$  as well as the quadratic parabola  $y_p$  about which  $y$  is oscillating, practically like a sine curve since the cosine term is smaller by a factor of about  $1/1000$ . ■

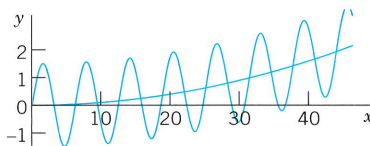


Fig. 49. Solution in Example 1

### EXAMPLE 2 Application of the Modification Rule (b)

Solve the initial value problem

$$(6) \quad y'' + 3y' + 2.25y = -10e^{-1.5x}, \quad y(0) = 1, \quad y'(0) = 0.$$

**Solution.** **Step 1. General solution of the homogeneous ODE.** The characteristic equation of the homogeneous ODE is  $\lambda^2 + 3\lambda + 2.25 = (\lambda + 1.5)^2 = 0$ . Hence the homogeneous ODE has the general solution

$$y_h = (c_1 + c_2x)e^{-1.5x}.$$

**Step 2. Solution  $y_p$  of the nonhomogeneous ODE.** The function  $e^{-1.5x}$  on the right would normally require the choice  $Ce^{-1.5x}$ . But we see from  $y_h$  that this function is a solution of the homogeneous ODE, which corresponds to a *double root* of the characteristic equation. Hence, according to the Modification Rule we have to multiply our choice function by  $x^2$ . That is, we choose

$$y_p = Cx^2e^{-1.5x}. \quad \text{Then} \quad y'_p = C(2x - 1.5x^2)e^{-1.5x}, \quad y''_p = C(2 - 3x - 3x + 2.25x^2)e^{-1.5x}.$$

We substitute these expressions into the given ODE and omit the factor  $e^{-1.5x}$ . This yields

$$C(2 - 6x + 2.25x^2) + 3C(2x - 1.5x^2) + 2.25Cx^2 = -10.$$

Comparing the coefficients of  $x^2$ ,  $x$ ,  $x^0$  gives  $0 = 0$ ,  $0 = 0$ ,  $2C = -10$ , hence  $C = -5$ . This gives the solution  $y_p = -5x^2e^{-1.5x}$ . Hence the given ODE has the general solution

$$y = y_h + y_p = (c_1 + c_2x)e^{-1.5x} - 5x^2e^{-1.5x}.$$

**Step 3. Solution of the initial value problem.** Setting  $x = 0$  in  $y$  and using the first initial condition, we obtain  $y(0) = c_1 = 1$ . Differentiation of  $y$  gives

$$y' = (c_2 - 1.5c_1 - 1.5c_2x)e^{-1.5x} - 10xe^{-1.5x} + 7.5x^2e^{-1.5x}.$$

From this and the second initial condition we have  $y'(0) = c_2 - 1.5c_1 = 0$ . Hence  $c_2 = 1.5c_1 = 1.5$ . This gives the answer (Fig. 50)

$$y = (1 + 1.5x)e^{-1.5x} - 5x^2e^{-1.5x} = (1 + 1.5x - 5x^2)e^{-1.5x}.$$

The curve begins with a horizontal tangent, crosses the  $x$ -axis at  $x = 0.6217$  (where  $1 + 1.5x - 5x^2 = 0$ ) and approaches the axis from below as  $x$  increases. ■

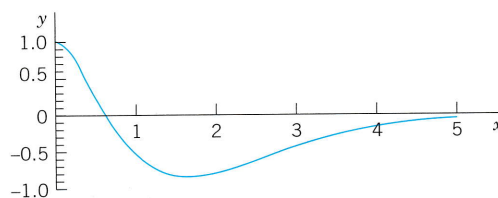


Fig. 50. Solution in Example 2

**EXAMPLE 3 Application of the Sum Rule (c)**

Solve the initial value problem

$$(7) \quad y'' + 2y' + 5y = e^{0.5x} + 40 \cos 10x - 190 \sin 10x, \quad y(0) = 0.16, \quad y'(0) = 40.08.$$

**Solution.** *Step 1. General solution of the homogeneous ODE.* The characteristic equation

$$\lambda^2 + 2\lambda + 5 = (\lambda + 1 + 2i)(\lambda + 1 - 2i) = 0$$

shows that a real general solution of the homogeneous ODE is

$$y_h = e^{-x} (A \cos 2x + B \sin 2x).$$

*Step 2. Solution of the nonhomogeneous ODE.* We write  $y_p = y_{p1} + y_{p2}$ , where  $y_{p1}$  corresponds to the exponential term and  $y_{p2}$  to the sum of the other two terms. We set

$$y_{p1} = Ce^{0.5x}. \quad \text{Then} \quad y'_{p1} = 0.5Ce^{0.5x} \quad \text{and} \quad y''_{p1} = 0.25Ce^{0.5x}.$$

Substitution into the given ODE and omission of the exponential factor gives  $(0.25 + 2 \cdot 0.5 + 5)C = 1$ , hence  $C = 1/6.25 = 0.16$ , and  $y_{p1} = 0.16e^{0.5x}$ .We now set  $y_{p2} = K \cos 10x + M \sin 10x$ , as in Table 2.1, and obtain

$$y'_{p2} = -10K \sin 10x + 10M \cos 10x, \quad y''_{p2} = -100K \cos 10x - 100M \sin 10x.$$

Substitution into the given ODE gives for the cosine terms and for the sine terms

$$-100K + 2 \cdot 10M + 5K = 40, \quad -100M - 2 \cdot 10K + 5M = -190$$

or, by simplification,

$$-95K + 20M = 40, \quad -20K - 95M = -190.$$

The solution is  $K = 0$ ,  $M = 2$ . Hence  $y_{p2} = 2 \sin 10x$ . Together,

$$y = y_h + y_{p1} + y_{p2} = e^{-x} (A \cos 2x + B \sin 2x) + 0.16e^{0.5x} + 2 \sin 10x.$$

*Step 3. Solution of the initial value problem.* From  $y$  and the first initial condition,  $y(0) = A + 0.16 = 0.16$ , hence  $A = 0$ . Differentiation gives

$$y' = e^{-x}(-A \cos 2x - B \sin 2x - 2A \sin 2x + 2B \cos 2x) + 0.08e^{0.5x} + 20 \cos 10x.$$

From this and the second initial condition we have  $y'(0) = -A + 2B + 0.08 + 20 = 40.08$ , hence  $B = 10$ . This gives the solution (Fig. 51)

$$y = 10e^{-x} \sin 2x + 0.16e^{0.5x} + 2 \sin 10x.$$

The first term goes to 0 relatively fast. When  $x = 4$ , it is practically 0, as the dashed curves  $\pm 10e^{-x} + 0.16e^{0.5x}$  show. From then on, the last term,  $2 \sin 10x$ , gives an oscillation about  $0.16e^{0.5x}$ , the monotone increasing dashed curve. ■

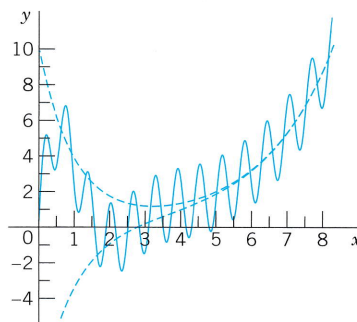


Fig. 51. Solution in Example 3

**Stability.** The following is important. If (and only if) all the roots of the characteristic equation of the homogeneous ODE  $y'' + ay' + by = 0$  in (4) are negative, or have a negative real part, then a general solution  $y_h$  of this ODE goes to 0 as  $x \rightarrow \infty$ , so that the “**transient solution**”  $y = y_h + y_p$  of (4) approaches the “**steady-state solution**”  $y_p$ . In this case the nonhomogeneous ODE and the physical or other system modeled by the ODE are called **stable**; otherwise they are called **unstable**. For instance, the ODE in Example 1 is unstable.

Basic applications follow in the next two sections.

## PROBLEM SET 2.7

### 1–14 GENERAL SOLUTIONS OF NONHOMOGENEOUS ODES

Find a (real) general solution. Which rule are you using? (Show each step of your calculation.)

1.  $y'' + 3y' + 2y = 30e^{2x}$
2.  $y'' + 4y' + 3.75y = 109 \cos 5x$
3.  $y'' - 16y = 19.2e^{4x} + 60e^x$
4.  $y'' + 9y = \cos x + \frac{1}{3} \cos 3x$
5.  $y'' + y' - 6y = 6x^3 - 3x^2 + 12x$
6.  $y'' + 4y' + 4y = e^{-2x} \sin 2x$
7.  $y'' + 6y' + 73y = 80e^x \cos 4x$
8.  $y'' + 10y' + 25y = 100 \sinh 5x$
9.  $y'' - 0.16y = 32 \cosh 0.4x$
10.  $y'' + 4y' + 6.25y = 3.125(x + 1)^2$
11.  $y'' + 1.44y = 24 \cos 1.2x$
12.  $y'' + 9y = 18x + 36 \sin 3x$
13.  $y'' + 4y' + 5y = 25x^2 + 13 \sin 2x$
14.  $y'' + 2y' + y = 2x \sin x$

### 15–20 INITIAL VALUE PROBLEMS FOR NONHOMOGENEOUS ODES

Solve the initial value problem. State which rules you are using. Show each step of your calculation in detail.

15.  $y'' + 4y = 16 \cos 2x, \quad y(0) = 0, \quad y'(0) = 0$

16.  $y'' - 3y' + 2.25y = 27(x^2 - x),$   
 $y(0) = 20, \quad y'(0) = 30$
17.  $y'' + 0.2y' + 0.26y = 1.22e^{0.5x},$   
 $y(0) = 3.5, \quad y'(0) = 0.35$
18.  $y'' - 2y' = 12e^{2x} - 8e^{-2x},$   
 $y(0) = -2, \quad y'(0) = 12$
19.  $y'' - y' - 12y = 144x^3 + 12.5,$   
 $y(0) = 5, \quad y'(0) = -0.5$
20.  $y'' + 2y' + 10y = 17 \sin x - 37 \sin 3x,$   
 $y(0) = 6.6, \quad y'(0) = -2.2$

21. **WRITING PROJECT. Initial Value Problem.** Write out all the details of Example 3 in your own words. Discuss Fig. 51 in more detail. Why is it that some of the “half-waves” do not reach the dashed curves, whereas others preceding them (and, of course, all later ones) exceed the dashed curves?

22. **TEAM PROJECT. Extensions of the Method of Undetermined Coefficients.** (a) Extend the method to products of the function in Table 2.1. (b) Extend the method to Euler–Cauchy equations. Comment on the practical significance of such extensions.

23. **CAS PROJECT. Structure of Solutions of Initial Value Problems.** Using the present method, find, graph, and discuss the solutions  $y$  of initial value problems of your own choice. Explore effects on solutions caused by

changes of initial conditions. Graph  $y_p$ ,  $y$ ,  $y - y_p$  separately, to see the separate effects. Find a problem in which (a) the part of  $y$  resulting from  $y_h$  decreases to zero, (b) increases, (c) is not present in the answer  $y$ . Study a

problem with  $y(0) = 0$ ,  $y'(0) = 0$ . Consider a problem in which you need the Modification Rule (a) for a simple root, (b) for a double root. Make sure that your problems cover all three Cases I, II, III (see Sec. 2.2).

## 2.8 Modeling: Forced Oscillations. Resonance

In Sec. 2.4 we considered vertical motions of a mass-spring system (vibration of a mass  $m$  on an elastic spring, as in Figs. 32 and 52) and modeled it by the *homogeneous* linear ODE

$$(1) \quad my'' + cy' + ky = 0.$$

Here  $y(t)$  as a function of time  $t$  is the displacement of the body of mass  $m$  from rest. These were **free motions**, that is, motions in the absence of *external forces* (outside forces) caused solely by *internal forces*, forces within the system. These are the force of inertia  $my''$ , the damping force  $cy'$  (if  $c > 0$ ), and the spring force  $ky$  acting as a restoring force.

We now extend our model by including an external force, call it  $r(t)$ , on the right. Then we have

$$(2^*) \quad my'' + cy' + ky = r(t).$$

Mechanically this means that at each instant  $t$  the resultant of the internal forces is in equilibrium with  $r(t)$ . The resulting motion is called a **forced motion** with **forcing function**  $r(t)$ , which is also known as **input** or **driving force**, and the solution  $y(t)$  to be obtained is called the **output** or the **response of the system to the driving force**.

Of special interest are periodic external forces, and we shall consider a driving force of the form

$$r(t) = F_0 \cos \omega t \quad (F_0 > 0, \omega > 0).$$

Then we have the nonhomogeneous ODE

$$(2) \quad my'' + cy' + ky = F_0 \cos \omega t.$$

Its solution will familiarize us with further interesting facts fundamental in engineering mathematics, in particular with resonance.

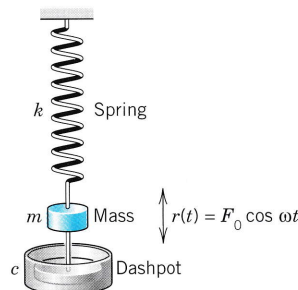


Fig. 52. Mass on a spring

## Solving the Nonhomogeneous ODE (2)

From Sec. 2.7 we know that a general solution of (2) is the sum of a general solution  $y_h$  of the homogeneous ODE (1) plus any solution  $y_p$  of (2). To find  $y_p$ , we use the method of undetermined coefficients (Sec. 2.7), starting from

$$(3) \quad y_p(t) = a \cos \omega t + b \sin \omega t.$$

By differentiating this function (chain rule!) we obtain

$$\begin{aligned} y_p' &= -\omega a \sin \omega t + \omega b \cos \omega t, \\ y_p'' &= -\omega^2 a \cos \omega t - \omega^2 b \sin \omega t. \end{aligned}$$

Substituting  $y_p$ ,  $y_p'$ , and  $y_p''$  into (2) and collecting the cosine and the sine terms, we get

$$[(k - m\omega^2)a + \omega cb] \cos \omega t + [-\omega ca + (k - m\omega^2)b] \sin \omega t = F_0 \cos \omega t.$$

The cosine terms on both sides must be equal, and the coefficient of the sine term on the left must be zero since there is no sine term on the right. This gives the two equations

$$(4) \quad \begin{aligned} (k - m\omega^2)a + \omega cb &= F_0 \\ -\omega ca + (k - m\omega^2)b &= 0 \end{aligned}$$

for determining the unknown coefficients  $a$  and  $b$ . This is a linear system. We can solve it by elimination. To eliminate  $b$ , multiply the first equation by  $k - m\omega^2$  and the second by  $-\omega c$  and add the results, obtaining

$$(k - m\omega^2)^2 a + \omega^2 c^2 a = F_0(k - m\omega^2).$$

Similarly, to eliminate  $a$ , multiply the first equation by  $\omega c$  and the second by  $k - m\omega^2$  and add to get

$$\omega^2 c^2 b + (k - m\omega^2)^2 b = F_0 \omega c.$$

If the factor  $(k - m\omega^2)^2 + \omega^2 c^2$  is not zero, we can divide by this factor and solve for  $a$  and  $b$ ,

$$a = F_0 \frac{k - m\omega^2}{(k - m\omega^2)^2 + \omega^2 c^2}, \quad b = F_0 \frac{\omega c}{(k - m\omega^2)^2 + \omega^2 c^2}.$$

If we set  $\sqrt{k/m} = \omega_0 (> 0)$  as in Sec. 2.4, then  $k = m\omega_0^2$  and we obtain

$$(5) \quad a = F_0 \frac{m(\omega_0^2 - \omega^2)}{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2}, \quad b = F_0 \frac{\omega c}{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2}.$$

We thus obtain the general solution of the nonhomogeneous ODE (2) in the form

$$(6) \quad y(t) = y_h(t) + y_p(t).$$

Here  $y_h$  is a general solution of the homogeneous ODE (1) and  $y_p$  is given by (3) with coefficients (5).

We shall now discuss the behavior of the mechanical system, distinguishing between the two cases  $c = 0$  (no damping) and  $c > 0$  (damping). These cases will correspond to two basically different types of output.

### Case 1. Undamped Forced Oscillations. Resonance

If the damping of the physical system is so small that its effect can be neglected over the time interval considered, we can set  $c = 0$ . Then (5) reduces to  $a = F_0/[m(\omega_0^2 - \omega^2)]$  and  $b = 0$ . Hence (3) becomes (use  $\omega_0^2 = k/m$ )

$$(7) \quad y_p(t) = \frac{F_0}{m(\omega_0^2 - \omega^2)} \cos \omega t = \frac{F_0}{k[1 - (\omega/\omega_0)^2]} \cos \omega t.$$

Here we must assume that  $\omega^2 \neq \omega_0^2$ ; physically, the frequency  $\omega/(2\pi)$  [cycles/sec] of the driving force is different from the *natural frequency*  $\omega_0/(2\pi)$  of the system, which is the frequency of the free undamped motion [see (4) in Sec. 2.4]. From (7) and from (4\*) in Sec. 2.4 we have the general solution of the “undamped system”

$$(8) \quad y(t) = C \cos(\omega_0 t - \delta) + \frac{F_0}{m(\omega_0^2 - \omega^2)} \cos \omega t.$$

We see that this output is a *superposition of two harmonic oscillations* of the frequencies just mentioned.

**Resonance.** We discuss (7). We see that the maximum amplitude of  $y_p$  is (put  $\cos \omega t = 1$ )

$$(9) \quad a_0 = \frac{F_0}{k} \rho \quad \text{where} \quad \rho = \frac{1}{1 - (\omega/\omega_0)^2}.$$

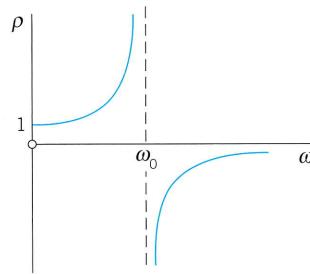
$a_0$  depends on  $\omega$  and  $\omega_0$ . If  $\omega \rightarrow \omega_0$ , then  $\rho$  and  $a_0$  tend to infinity. This excitation of large oscillations by matching input and natural frequencies ( $\omega = \omega_0$ ) is called **resonance**.  $\rho$  is called the **resonance factor** (Fig. 53), and from (9) we see that  $\rho/k = a_0/F_0$  is the ratio of the amplitudes of the particular solution  $y_p$  and of the input  $F_0 \cos \omega t$ . We shall see later in this section that resonance is of basic importance in the study of vibrating systems.

In the case of resonance the nonhomogeneous ODE (2) becomes

$$(10) \quad y'' + \omega_0^2 y = \frac{F_0}{m} \cos \omega_0 t.$$

Then (7) is no longer valid, and from the Modification Rule in Sec. 2.7 we conclude that a particular solution of (10) is of the form

$$y_p(t) = t(a \cos \omega_0 t + b \sin \omega_0 t).$$

Fig. 53. Resonance factor  $\rho(\omega)$ 

By substituting this into (10) we find  $a = 0$  and  $b = F_0/(2m\omega_0)$ . Hence (Fig. 54)

$$(11) \quad y_p(t) = \frac{F_0}{2m\omega_0} t \sin \omega_0 t.$$

We see that because of the factor  $t$  the amplitude of the vibration becomes larger and larger. Practically speaking, systems with very little damping may undergo large vibrations that can destroy the system. We shall return to this practical aspect of resonance later in this section.

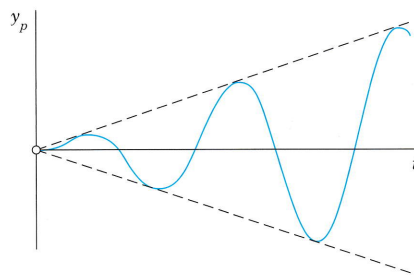


Fig. 54. Particular solution in the case of resonance

**Beats.** Another interesting and highly important type of oscillation is obtained if  $\omega$  is close to  $\omega_0$ . Take, for example, the particular solution [see (8)]

$$(12) \quad y(t) = \frac{F_0}{m(\omega_0^2 - \omega^2)} (\cos \omega t - \cos \omega_0 t) \quad (\omega \neq \omega_0).$$

Using (12) in App. 3.1, we may write this as

$$y(t) = \frac{2F_0}{m(\omega_0^2 - \omega^2)} \sin \left( \frac{\omega_0 + \omega}{2} t \right) \sin \left( \frac{\omega_0 - \omega}{2} t \right).$$

Since  $\omega$  is close to  $\omega_0$ , the difference  $\omega_0 - \omega$  is small. Hence the period of the last sine function is large, and we obtain an oscillation of the type shown in Fig. 55, the dashed curve resulting from the first sine factor. This is what musicians are listening to when they *tune* their instruments.



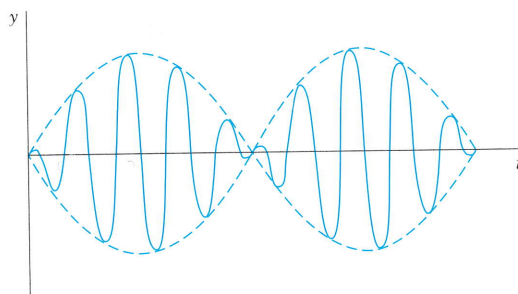


Fig. 55. Forced undamped oscillation when the difference of the input and natural frequencies is small (“beats”)

## Case 2. Damped Forced Oscillations

If the damping of the mass-spring system is not negligibly small, we have  $c > 0$  and a damping term  $cy'$  in (1) and (2). Then the general solution  $y_h$  of the homogeneous ODE (1) approaches zero as  $t$  goes to infinity, as we know from Sec. 2.4. Practically, it is zero after a sufficiently long time. Hence the “**transient solution**” (6) of (2), given by  $y = y_h + y_p$ , approaches the “**steady-state solution**”  $y_p$ . This proves the following.

### THEOREM 1

#### Steady-State Solution

After a sufficiently long time the output of a damped vibrating system under a purely sinusoidal driving force [see (2)] will practically be a harmonic oscillation whose frequency is that of the input.

#### Amplitude of the Steady-State Solution. Practical Resonance

Whereas in the undamped case the amplitude of  $y_p$  approaches infinity as  $\omega$  approaches  $\omega_0$ , this will not happen in the damped case. In this case the amplitude will always be finite. But it may have a maximum for some  $\omega$  depending on the damping constant  $c$ . This may be called **practical resonance**. It is of great importance because if  $c$  is not too large, then some input may excite oscillations large enough to damage or even destroy the system. Such cases happened, in particular in earlier times when less was known about resonance. Machines, cars, ships, airplanes, bridges, and high-rising buildings are vibrating mechanical systems, and it is sometimes rather difficult to find constructions that are completely free of undesired resonance effects, caused, for instance, by an engine or by strong winds.

To study the amplitude of  $y_p$  as a function of  $\omega$ , we write (3) in the form

$$(13) \quad y_p(t) = C^* \cos(\omega t - \eta).$$

$C^*$  is called the **amplitude** of  $y_p$  and  $\eta$  the **phase angle** or **phase lag** because it measures the lag of the output behind the input. According to (5), these quantities are

$$(14) \quad C^*(\omega) = \sqrt{a^2 + b^2} = \frac{F_0}{\sqrt{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2}},$$

$$\tan \eta(\omega) = \frac{b}{a} = \frac{\omega c}{m(\omega_0^2 - \omega^2)}.$$

Let us see whether  $C^*(\omega)$  has a maximum and, if so, find its location and then its size. We denote the radicand in the second root in  $C^*$  by  $R$ . Equating the derivative of  $C^*$  to zero, we obtain

$$\frac{dC^*}{d\omega} = F_0 \left( -\frac{1}{2} R^{-3/2} \right) [2m^2(\omega_0^2 - \omega^2)(-2\omega) + 2\omega c^2].$$

The expression in the brackets [...] is zero if

$$(15) \quad c^2 = 2m^2(\omega_0^2 - \omega^2) \quad (\omega_0^2 = k/m).$$

By reshuffling terms we have

$$2m^2\omega^2 = 2m^2\omega_0^2 - c^2 = 2mk - c^2.$$

The right side of this equation becomes negative if  $c^2 > 2mk$ , so that then (15) has no real solution and  $C^*$  decreases monotone as  $\omega$  increases, as the lowest curve in Fig. 56 on p. 90 shows. If  $c$  is smaller,  $c^2 < 2mk$ , then (15) has a real solution  $\omega = \omega_{\max}$ , where

$$(15^*) \quad \omega_{\max}^2 = \omega_0^2 - \frac{c^2}{2m^2}.$$

From (15\*) we see that this solution increases as  $c$  decreases and approaches  $\omega_0$  as  $c$  approaches zero. See also Fig. 56.

The size of  $C^*(\omega_{\max})$  is obtained from (14), with  $\omega^2 = \omega_{\max}^2$  given by (15\*). For this  $\omega^2$  we obtain in the second radicand in (14) from (15\*)

$$m^2(\omega_0^2 - \omega_{\max}^2)^2 = \frac{c^4}{4m^2} \quad \text{and} \quad \omega_{\max}^2 c^2 = \left( \omega_0^2 - \frac{c^2}{2m^2} \right) c^2.$$

The sum of the right sides of these two formulas is

$$(c^4 + 4m^2\omega_0^2 c^2 - 2c^4)/(4m^2) = c^2(4m^2\omega_0^2 - c^2)/(4m^2).$$

Substitution into (14) gives

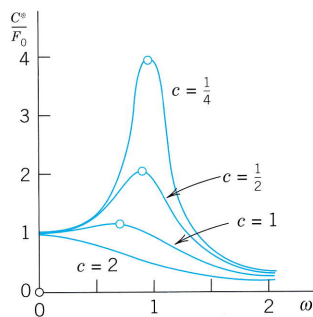
$$(16) \quad C^*(\omega_{\max}) = \frac{2mF_0}{c\sqrt{4m^2\omega_0^2 - c^2}}.$$

We see that  $C^*(\omega_{\max})$  is always finite when  $c > 0$ . Furthermore, since the expression

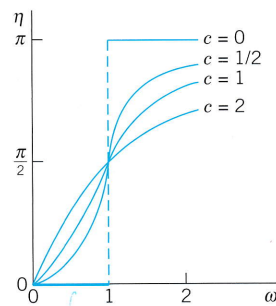
$$c^2 4m^2\omega_0^2 - c^4 = c^2(4mk - c^2)$$

in the denominator of (16) decreases monotone to zero as  $c^2 (< 2mk)$  goes to zero, the maximum amplitude (16) increases monotone to infinity, in agreement with our result in Case 1. Figure 56 shows the **amplification**  $C^*/F_0$  (ratio of the amplitudes of output and input) as a function of  $\omega$  for  $m = 1$ ,  $k = 1$ , hence  $\omega_0 = 1$ , and various values of the damping constant  $c$ .

Figure 57 shows the phase angle (the lag of the output behind the input), which is less than  $\pi/2$  when  $\omega < \omega_0$ , and greater than  $\pi/2$  for  $\omega > \omega_0$ .



**Fig. 56.** Amplification  $C^*/F_0$  as a function of  $\omega$  for  $m = 1$ ,  $k = 1$ , and various values of the damping constant  $c$



**Fig. 57.** Phase lag  $\eta$  as a function of  $\omega$  for  $m = 1$ ,  $k = 1$ , thus  $\omega_0 = 1$ , and various values of the damping constant  $c$

## PROBLEM SET 2.8

### 1–8 STEADY-STATE SOLUTIONS

Find the steady-state oscillation of the mass–spring system modeled by the given ODE. Show the details of your calculations.

- $y'' + 6y' + 8y = 130 \cos 3t$
- $4y'' + 8y' + 13y = 8 \sin 1.5t$
- $y'' + y' + 4.25y = 221 \cos 4.5t$
- $y'' + 4y' + 5y = \cos t - \sin t$
- $(D^2 + 2D + I)y = -\sin 2t$
- $(D^2 + 4D + 3I)y = \cos t + \frac{1}{3} \cos 3t$
- $(D^2 + 6D + 18I)y = \cos 3t - 3 \sin 3t$
- $(D^2 + 2D + 10I)y = -25 \sin 4t$

### 9–14 TRANSIENT SOLUTIONS

Find the transient motion of the mass–spring system modeled by the given ODE. (Show the details of your work.)

- $y'' + 2y' + 0.75y = 13 \sin t$
- $y'' + 4y' + 4y = \cos 4t$
- $4y'' + 12y' + 9y = 75 \sin 3t$
- $(D^2 + 5D + 4I)y = \sin 2t$
- $(D^2 + 3D + 3.25I)y = 13 - 39 \cos 2t$
- $(D^2 + 2D + 5I)y = 1 + \sin t$

### 15–20 INITIAL VALUE PROBLEMS

Find the motion of the mass–spring system modeled by the ODE and initial conditions. Sketch or graph the solution curve. In addition, sketch or graph the curve of

$y - y_p$  to see when the system practically reaches the steady state.

- $y'' + 2y' + 26y = 13 \cos 3t$ ,  
 $y(0) = 1$ ,  $y'(0) = 0.4$
- $y'' + 64y = \cos t$ ,  $y(0) = 0$ ,  $y'(0) = 1$
- $y'' + 6y' + 8y = 4 \sin 2t$ ,  $y(0) = 0.7$ ,  
 $y'(0) = -11.8$
- $(D^2 + 2D + I)y = 75(\sin t - \frac{1}{2} \sin 2t + \frac{1}{3} \sin 3t)$ ,  
 $y(0) = 0$ ,  $y'(0) = 1$
- $(4D^2 + 12D + 13I)y = 12 \cos t - 6 \sin t$ ,  
 $y(0) = 1$ ,  $y'(0) = -1$
- $y'' + 25y = 99 \cos 4.9t$ ,  $y(0) = 2$ ,  $y'(0) = 0$
- (Beats)** Derive the formula after (12) from (12). Can there be beats if the system has damping?
- (Beats)** How does the graph of the solution in Prob. 20 change if you change (a)  $y(0)$ , (b) the frequency of the driving force?
- WRITING PROJECT. Free and Forced Vibrations.** Write a condensed report of 2–3 pages on the most important facts about free and forced vibrations.
- CAS EXPERIMENT. Undamped Vibrations.** (a) Solve the initial value problem  $y'' + y = \cos \omega t$ ,  $\omega^2 \neq 1$ ,  $y(0) = 0$ ,  $y'(0) = 0$ . Show that the solution can be written

$$(17) \quad y(t) = \frac{2}{1 - \omega^2} \sin \left[ \frac{1}{2} (1 + \omega)t \right] \times \sin \left[ \frac{1}{2} (1 - \omega)t \right].$$

(b) Experiment with (17) by changing  $\omega$  to see the change of the curves from those for small  $\omega$  ( $> 0$ ) to beats, to resonance and to large values of  $\omega$  (see Fig. 58).

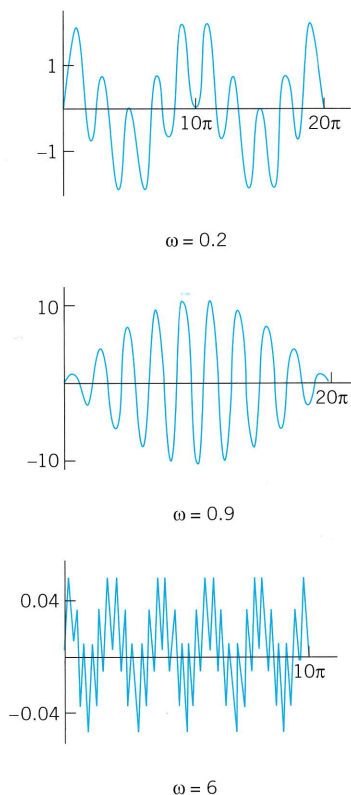


Fig. 58. Typical solution curves in CAS Experiment 24

25. **TEAM PROJECT. Practical Resonance.** (a) Give a detailed derivation of the crucial formula (16).  
 (b) By considering  $dC^*/dc$  show that  $C^*(\omega_{\max})$  increases as  $c$  ( $\leq \sqrt{2mk}$ ) decreases.  
 (c) Illustrate practical resonance with an ODE of your own in which you vary  $c$ , and sketch or graph corresponding curves as in Fig. 56.  
 (d) Take your ODE with  $c$  fixed and an input of two terms, one with frequency close to the practical resonance frequency and the other not. Discuss and sketch or graph the output.  
 (e) Give other applications (not in the book) in which resonance is important.

26. **(Gun barrel)** Solve

$$y'' + y = \begin{cases} 1 - t^2/\pi^2 & \text{if } 0 \leq t \leq \pi \\ 0 & \text{if } t > \pi, \end{cases} \quad y(0) = y'(\pi) = 0.$$

This models an undamped system on which a force  $F$  acts during some interval of time (see Fig. 59), for instance, the force on a gun barrel when a shell is fired, the barrel being braked by heavy springs (and then damped by a dashpot, which we disregard for simplicity). *Hint.* At  $\pi$  both  $y$  and  $y'$  must be continuous.

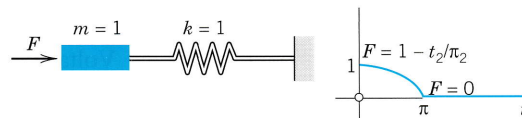


Fig. 59. Problem 26

## 2.9 Modeling: Electric Circuits

Designing good models is a task the computer cannot do. Hence setting up models has become an important task in modern applied mathematics. The best way to gain experience is to consider models from various fields. Accordingly, modeling electric circuits to be discussed will be *profitable for all students*, not just for electrical engineers and computer scientists.

We have just seen that linear ODEs have important applications in mechanics (see also Sec. 2.4). Similarly, they are models of electric circuits, as they occur as portions of large networks in computers and elsewhere. The circuits we shall consider here are basic building blocks of such networks. They contain three kinds of components, namely, resistors, inductors, and capacitors. Figure 60 on p. 92 shows such an **RLC-circuit**, as they are called. In it a resistor of resistance  $R \Omega$  (ohms), an inductor of inductance  $L$  H (henrys), and a capacitor of capacitance  $C$  F (farads) are wired in series as shown, and connected to an electromotive force  $E(t)$  V (volts) (a generator, for instance), sinusoidal as in Fig. 60, or of some other kind.  $R$ ,  $L$ ,  $C$ , and  $E$  are given and we want to find the current  $I(t)$  A (amperes) in the circuit.

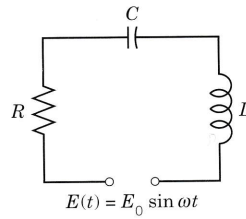


Fig. 60. RLC-circuit

An ODE for the current  $I(t)$  in the  $RLC$ -circuit in Fig. 60 is obtained from the following law (which is the analog of Newton's second law, as we shall see later).

**Kirchhoff's Voltage Law (KVL).**<sup>7</sup> *The voltage (the electromotive force) impressed on a closed loop is equal to the sum of the voltage drops across the other elements of the loop.*

In Fig. 60 the circuit is a closed loop, and the impressed voltage  $E(t)$  equals the sum of the voltage drops across the three elements  $R$ ,  $L$ ,  $C$  of the loop.

**Voltage Drops.** Experiments show that a current  $I$  flowing through a resistor, inductor or capacitor causes a voltage drop (voltage difference, measured in volts) at the two ends; these drops are

$RI$  (Ohm's law) Voltage drop for a resistor of resistance  $R$  ohms ( $\Omega$ ),

$LI' = L \frac{dI}{dt}$  Voltage drop for an inductor of inductance  $L$  henrys (H),

$\frac{Q}{C}$  Voltage drop for a capacitor of capacitance  $C$  farads (F).

Here  $Q$  coulombs is the charge on the capacitor, related to the current by

$$I(t) = \frac{dQ}{dt}, \quad \text{equivalently,} \quad Q(t) = \int I(t) dt.$$

This is summarized in Fig. 61.

According to KVL we thus have in Fig. 60 for an  $RLC$ -circuit with electromotive force  $E(t) = E_0 \sin \omega t$  ( $E_0$  constant) as a model the "**integro-differential equation**"

$$(1') \quad LI' + RI + \frac{1}{C} \int I dt = E(t) = E_0 \sin \omega t.$$

<sup>7</sup>GUSTAV ROBERT KIRCHHOFF (1824–1887), German physicist. Later we shall also need **Kirchhoff's current law (KCL)**:

*At any point of a circuit, the sum of the inflowing currents is equal to the sum of the outflowing currents.*

The units of measurement of electrical quantities are named after ANDRÉ MARIE AMPÈRE (1775–1836), French physicist, CHARLES AUGUSTIN DE COULOMB (1736–1806), French physicist and engineer, MICHAEL FARADAY (1791–1867), English physicist, JOSEPH HENRY (1797–1878), American physicist, GEORG SIMON OHM (1789–1854), German physicist, and ALESSANDRO VOLTA (1745–1827), Italian physicist.




Name	Symbol	Notation	Unit	Voltage Drop
Ohm's resistor		$R$ Ohm's resistance	ohms ( $\Omega$ )	$RI$
Inductor		$L$ Inductance	henrys (H)	$L \frac{dI}{dt}$
Capacitor		$C$ Capacitance	farads (F)	$Q/C$

Fig. 61. Elements in an  $RLC$ -circuit

To get rid of the integral, we differentiate (1') with respect to  $t$ , obtaining

$$(1) \quad LI'' + RI' + \frac{1}{C} I = E'(t) = E_0\omega \cos \omega t.$$

This shows that the current in an  $RLC$ -circuit is obtained as the solution of this nonhomogeneous second-order ODE (1) with constant coefficients.

From (1'), using  $I = Q'$ , hence  $I' = Q''$ , we also have directly

$$(1'') \quad LQ'' + RQ' + \frac{1}{C} Q = E_0 \sin \omega t.$$

But in most practical problems the current  $I(t)$  is more important than the charge  $Q(t)$ , and for this reason we shall concentrate on (1) rather than on (1'').

## Solving the ODE (1) for the Current.

### Discussion of Solution

A general solution of (1) is the sum  $I = I_h + I_p$ , where  $I_h$  is a general solution of the homogeneous ODE corresponding to (1) and  $I_p$  is a particular solution of (1). We first determine  $I_p$  by the method of undetermined coefficients, proceeding as in the previous section. We substitute

$$(2) \quad \begin{aligned} I_p &= a \cos \omega t + b \sin \omega t \\ I_p' &= \omega(-a \sin \omega t + b \cos \omega t) \\ I_p'' &= \omega^2(-a \cos \omega t - b \sin \omega t) \end{aligned}$$

into (1). Then we collect the cosine terms and equate them to  $E_0\omega \cos \omega t$  on the right, and we equate the sine terms to zero because there is no sine term on the right,

$$L\omega^2(-a) + R\omega b + a/C = E_0\omega \quad (\text{Cosine terms})$$

$$L\omega^2(-b) + R\omega(-a) + b/C = 0 \quad (\text{Sine terms}).$$

To solve this system for  $a$  and  $b$ , we first introduce a combination of  $L$  and  $C$ , called the **reactance**

$$(3) \quad S = \omega L - \frac{1}{\omega C}.$$

Dividing the previous two equations by  $\omega$ , ordering them, and substituting  $S$  gives

$$\begin{aligned} -Sa + Rb &= E_0 \\ -Ra - Sb &= 0. \end{aligned}$$

We now eliminate  $b$  by multiplying the first equation by  $S$  and the second by  $R$ , and adding. Then we eliminate  $a$  by multiplying the first equation by  $R$  and the second by  $-S$ , and adding. This gives

$$-(S^2 + R^2)a = E_0S, \quad (R^2 + S^2)b = E_0R.$$

In any practical case the resistance  $R$  is different from zero, so that we can solve for  $a$  and  $b$ ,

$$(4) \quad a = \frac{-E_0S}{R^2 + S^2}, \quad b = \frac{E_0R}{R^2 + S^2}.$$

Equation (2) with coefficients  $a$  and  $b$  given by (4) is the desired particular solution  $I_p$  of the nonhomogeneous ODE (1) governing the current  $I$  in an  $RLC$ -circuit with sinusoidal electromotive force.

Using (4), we can write  $I_p$  in terms of “physically visible” quantities, namely, amplitude  $I_0$  and phase lag  $\theta$  of the current behind the electromotive force, that is,

$$(5) \quad I_p(t) = I_0 \sin(\omega t - \theta)$$

where [see (14) in App. A3.1]

$$I_0 = \sqrt{a^2 + b^2} = \frac{E_0}{\sqrt{R^2 + S^2}}, \quad \tan \theta = -\frac{a}{b} = \frac{S}{R}.$$

The quantity  $\sqrt{R^2 + S^2}$  is called the **impedance**. Our formula shows that the impedance equals the ratio  $E_0/I_0$ . This is somewhat analogous to  $E/I = R$  (Ohm’s law).

A general solution of the homogeneous equation corresponding to (1) is

$$I_h = c_1 e^{\lambda_1 t} + c_2 e^{\lambda_2 t}$$

where  $\lambda_1$  and  $\lambda_2$  are the roots of the characteristic equation

$$\lambda^2 + \frac{R}{L}\lambda + \frac{1}{LC} = 0.$$

We can write these roots in the form  $\lambda_1 = -\alpha + \beta$  and  $\lambda_2 = -\alpha - \beta$ , where

$$\alpha = \frac{R}{2L}, \quad \beta = \sqrt{\frac{R^2}{4L^2} - \frac{1}{LC}} = \frac{1}{2L} \sqrt{R^2 - \frac{4L}{C}}.$$

Now in an actual circuit,  $R$  is never zero (hence  $R > 0$ ). From this it follows that  $I_h$  approaches zero, theoretically as  $t \rightarrow \infty$ , but practically after a relatively short time. (This is as for the motion in the previous section.) Hence the transient current  $I = I_h + I_p$  tends

to the steady-state current  $I_p$ , and after some time the output will practically be a harmonic oscillation, which is given by (5) and whose frequency is that of the input (of the electromotive force).

### EXAMPLE 1 RLC-Circuit

Find the current  $I(t)$  in an  $RLC$ -circuit with  $R = 11 \Omega$  (ohms),  $L = 0.1$  H (henry),  $C = 10^{-2}$  F (farad), which is connected to a source of voltage  $E(t) = 100 \sin 400t$  (hence  $63\frac{2}{3}$  Hz =  $63\frac{2}{3}$  cycles/sec, because  $400 = 63\frac{2}{3} \cdot 2\pi$ ). Assume that current and charge are zero when  $t = 0$ .

**Solution.** *Step 1. General solution of the homogeneous ODE.* Substituting  $R, L, C$ , and the derivative  $E'(t)$  into (1), we obtain

$$0.1I'' + 11I' + 100I = 100 \cdot 400 \cos 400t.$$

Hence the homogeneous ODE is  $0.1I'' + 11I' + 100I = 0$ . Its characteristic equation is

$$0.1\lambda^2 + 11\lambda + 100 = 0.$$

The roots are  $\lambda_1 = -10$  and  $\lambda_2 = -100$ . The corresponding general solution of the homogeneous ODE is

$$I_h(t) = c_1 e^{-10t} + c_2 e^{-100t}.$$

*Step 2. Particular solution  $I_p$  of (1).* We calculate the reactance  $S = 40 - 1/4 = 39.75$  and the steady-state current

$$I_p(t) = a \cos 400t + b \sin 400t$$

with coefficients obtained from (4)

$$a = \frac{-100 \cdot 39.75}{11^2 + 39.75^2} = -2.3368, \quad b = \frac{100 \cdot 11}{11^2 + 39.75^2} = 0.6467.$$

Hence in our present case, a general solution of the nonhomogeneous ODE (1) is

$$(6) \quad I(t) = c_1 e^{-10t} + c_2 e^{-100t} - 2.3368 \cos 400t + 0.6467 \sin 400t.$$

*Step 3. Particular solution satisfying the initial conditions. How to use  $Q(0) = 0$ ?* We finally determine  $c_1$  and  $c_2$  from the initial conditions  $I(0) = 0$  and  $Q(0) = 0$ . From the first condition and (6) we have

$$(7) \quad I(0) = c_1 + c_2 - 2.3368 = 0, \quad \text{hence} \quad c_2 = 2.3368 - c_1.$$

Furthermore, using (1') with  $t = 0$  and noting that the integral equals  $Q(t)$  (see the formula before (1')), we obtain

$$LI'(0) + R \cdot 0 + \frac{1}{C} \cdot 0 = 0, \quad \text{hence} \quad I'(0) = 0.$$

Differentiating (6) and setting  $t = 0$ , we thus obtain

$$I'(0) = -10c_1 - 100c_2 + 0 + 0.6467 \cdot 400 = 0, \quad \text{hence} \quad -10c_1 = 100(2.3368 - c_1) - 258.68.$$

The solution of this and (7) is  $c_1 = -0.2776$ ,  $c_2 = 2.6144$ . Hence the answer is

$$I(t) = -0.2776e^{-10t} + 2.6144e^{-100t} - 2.3368 \cos 400t + 0.6467 \sin 400t.$$

Figure 62 on p. 96 shows  $I(t)$  as well as  $I_p(t)$ , which practically coincide, except for a very short time near  $t = 0$  because the exponential terms go to zero very rapidly. Thus after a very short time the current will practically execute harmonic oscillations of the input frequency  $63\frac{2}{3}$  Hz =  $63\frac{2}{3}$  cycles/sec. Its maximum amplitude and phase lag can be seen from (5), which here takes the form

$$I_p(t) = 2.4246 \sin(400t - 1.3008). \quad \blacksquare$$



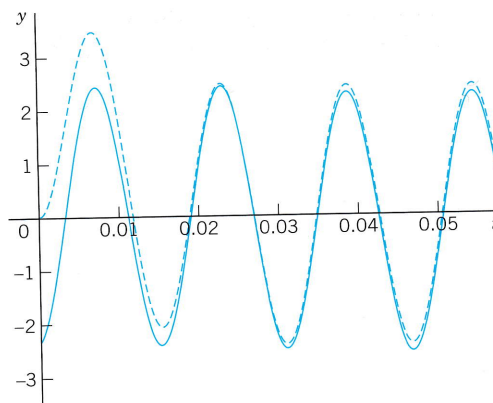


Fig. 62. Transient and steady-state currents in Example 1

## Analogy of Electrical and Mechanical Quantities

*Entirely different physical or other systems may have the same mathematical model.* For instance, we have seen this from the various applications of the ODE  $y'' = ky$  in Chap. 1. Another impressive demonstration of this *unifying power of mathematics* is given by the ODE (1) for an electric *RLC*-circuit and the ODE (2) in the last section for a mass–spring system. Both equations

$$LI'' + RI' + \frac{1}{C}I = E_0\omega \cos \omega t \quad \text{and} \quad my'' + cy' + ky = F_0 \cos \omega t$$

are of the same form. Table 2.2 shows the analogy between the various quantities involved. The inductance  $L$  corresponds to the mass  $m$  and, indeed, an inductor opposes a change in current, having an “inertia effect” similar to that of a mass. The resistance  $R$  corresponds to the damping constant  $c$ , and a resistor causes loss of energy, just as a damping dashpot does. And so on.

This analogy is *strictly quantitative* in the sense that to a given mechanical system we can construct an electric circuit whose current will give the exact values of the displacement in the mechanical system when suitable scale factors are introduced.

The *practical importance* of this analogy is almost obvious. The analogy may be used for constructing an “electrical model” of a given mechanical model, resulting in substantial savings of time and money because electric circuits are easy to assemble, and electric quantities can be measured much more quickly and accurately than mechanical ones.

Table 2.2 Analogy of Electrical and Mechanical Quantities

Electrical System	Mechanical System
Inductance $L$	Mass $m$
Resistance $R$	Damping constant $c$
Reciprocal $1/C$ of capacitance	Spring modulus $k$
Derivative $E_0\omega \cos \omega t$ of } electromotive force }	Driving force $F_0 \cos \omega t$
Current $I(t)$	Displacement $y(t)$

**PROBLEM SET 2.9**

- (RL-circuit)** Model the  $RL$ -circuit in Fig. 63. Find the general solution when  $R, L, E$  are any constants. Graph or sketch solutions when  $L = 0.1$  H,  $R = 5 \Omega$ ,  $E = 12$  V.
- (RL-circuit)** Solve Prob. 1 when  $E = E_0 \sin \omega t$  and  $R, L, E_0, \omega$  are arbitrary. Sketch a typical solution.
- (RC-circuit)** Model the  $RC$ -circuit in Fig. 66. Find the current due to a constant  $E$ .
- (RC-circuit)** Find the current in the  $RC$ -circuit in Fig. 66 with  $E = E_0 \sin \omega t$  and arbitrary  $R, C, E_0$ , and  $\omega$ .

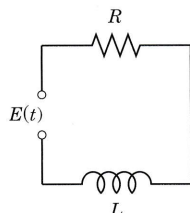


Fig. 63.  $RL$ -circuit

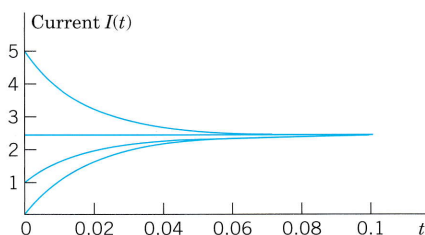


Fig. 64. Currents in Problem 1

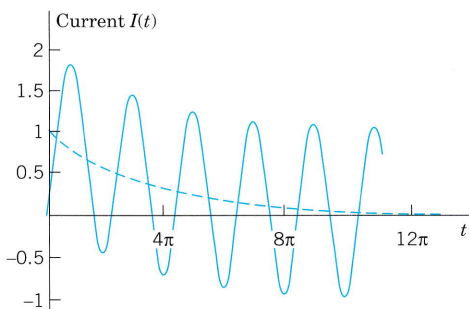


Fig. 65. Typical current  $I = e^{-0.1t} + \sin(t - \frac{1}{4}\pi)$  in Problem 2

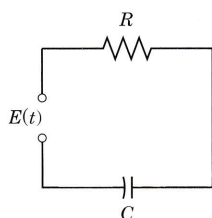


Fig. 66.  $RC$ -circuit

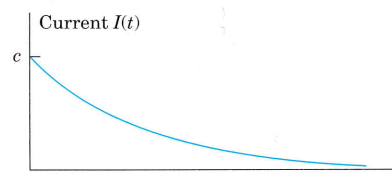


Fig. 67. Current  $I$  in Problem 3

- (LC-circuit)** This is an  $RLC$ -circuit with negligibly small  $R$  (analog of an undamped mass-spring system). Find the current when  $L = 0.2$  H,  $C = 0.05$  F, and  $E = \sin t$  V, assuming zero initial current and charge.
- (LC-circuit)** Find the current when  $L = 0.5$  H,  $C = 8 \cdot 10^{-4}$  F,  $E = t^2$  V and initial current and charge zero.

**7-9 RLC-CIRCUITS (FIG. 60, P. 92)**

- (Tuning)** In tuning a stereo system to a radio station, we adjust the tuning control (turn a knob) that changes  $C$  (or perhaps  $L$ ) in an  $RLC$ -circuit so that the amplitude of the steady-state current (5) becomes maximum. For what  $C$  will this happen?
- (Transient current)** Prove the claim in the text that if  $R \neq 0$  (hence  $R > 0$ ), then the transient current approaches  $I_p$  as  $t \rightarrow \infty$ .
- (Cases of damping)** What are the conditions for an  $RLC$ -circuit to be (I) overdamped, (II) critically damped, (III) underdamped? What is the critical resistance  $R_{crit}$  (the analog of the critical damping constant  $2\sqrt{mk}$ )?

**10-12** Find the **steady-state current** in the  $RLC$ -circuit in Fig. 60 on p. 92 for the given data. (Show the details of your work.)

- $R = 8 \Omega, L = 0.5$  H,  $C = 0.1$  F,  $E = 100 \sin 2t$  V
- $R = 1 \Omega, L = 0.25$  H,  $C = 5 \cdot 10^{-5}$  F,  $E = 110$  V
- $R = 2 \Omega, L = 1$  H,  $C = 0.05$  F,  $E = \frac{157}{9} \sin 3t$  V

**13-15** Find the **transient current** (a general solution) in the  $RLC$ -circuit in Fig. 60 for the given data. (Show the details of your work.)

- $R = 6 \Omega, L = 0.2$  H,  $C = 0.025$  F,  $E = 110 \sin 10t$  V
- $R = 0.2 \Omega, L = 0.1$  H,  $C = 2$  F,  $E = 754 \sin 0.5t$  V
- $R = 1/10 \Omega, L = 1/2$  H,  $C = 100/13$  F,  $E = e^{-4t}(1.932 \cos \frac{1}{2}t + 0.246 \sin \frac{1}{2}t)$  V

**16-18** Solve the **initial value problem** for the  $RLC$ -circuit in Fig. 60 with the given data, assuming zero initial current and charge. Graph or sketch the solution. (Show the details of your work.)

16.  $R = 4 \Omega$ ,  $L = 0.1 \text{ H}$ ,  $C = 0.025 \text{ F}$ ,  $E = 10 \sin 10t \text{ V}$   
 17.  $R = 6 \Omega$ ,  $L = 1 \text{ H}$ ,  $C = 0.04 \text{ F}$ ,  
 $E = 600(\cos t + 4 \sin t) \text{ V}$   
 18.  $R = 3.6 \Omega$ ,  $L = 0.2 \text{ H}$ ,  $C = 0.0625 \text{ F}$ ,  
 $E = 164 \cos 10t \text{ V}$

19. **WRITING PROJECT. Analogy of RLC-Circuits and Damped Mass-Spring Systems.** (a) Write an essay of 2–3 pages based on Table 2.2. Describe the analogy in more detail and indicate its practical significance.

(b) What RLC-circuit with  $L = 1 \text{ H}$  is the analog of the mass-spring system with mass 5 kg, damping constant 10 kg/sec, spring constant 60 kg/sec<sup>2</sup>, and driving force  $220 \cos 10t$ ?

(c) Illustrate the analogy with another example of your own choice.

20. **TEAM PROJECT. Complex Method for Particular Solutions.** (a) Find a particular solution of the complex ODE

$$(8) \quad L\tilde{I}'' + R\tilde{I}' + \frac{1}{C}\tilde{I} = E_0\omega e^{i\omega t} \quad (i = \sqrt{-1})$$

by substituting  $\tilde{I}_p = Ke^{i\omega t}$  ( $K$  unknown) and its derivatives into (8), and then take the real part  $I_p$  of  $\tilde{I}_p$ , showing that  $I_p$  agrees with (2), (4). *Hint.* Use the Euler formula  $e^{i\omega t} = \cos \omega t + i \sin \omega t$  [(11) in Sec. 2.2 with  $\omega t$  instead of  $t$ ]. Note that  $E_0\omega \cos \omega t$  in (1) is the real part of  $E_0\omega e^{i\omega t}$  in (8). Use  $i^2 = -1$ .

(b) The complex impedance  $Z$  is defined by

$$Z = R + iS = R + i\left(\omega L - \frac{1}{\omega C}\right).$$

Show that  $K$  obtained in (a) can be written as

$$K = \frac{E_0}{iZ}.$$

Note that the real part of  $Z$  is  $R$ , the imaginary part is the reactance  $S$ , and the absolute value is the impedance  $|Z| = \sqrt{R^2 + S^2}$  as defined before. See Fig. 68.

(c) Find the steady-state solution of the ODE  $I'' + 2I' + 3I = 20 \cos t$ , first by the real method and then by the complex method, and compare. (Show the details of your work.)

(d) Apply the complex method to an RLC-circuit of your choice.

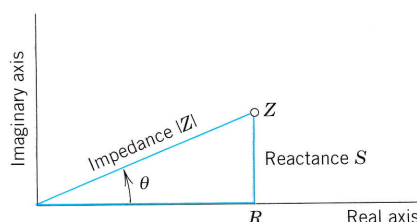


Fig. 68. Complex impedance  $Z$

## 2.10 Solution by Variation of Parameters

We continue our discussion of nonhomogeneous linear ODEs

$$(1) \quad y'' + p(x)y' + q(x)y = r(x).$$

In Sec. 2.6 we have seen that a general solution of (1) is the sum of a general solution  $y_h$  of the corresponding homogeneous ODE and any particular solution  $y_p$  of (1). To obtain  $y_p$  when  $r(x)$  is not too complicated, we can often use the *method of undetermined coefficients*, as we have shown in Sec. 2.7 and applied to basic engineering models in Secs. 2.8 and 2.9.

However, since this method is restricted to functions  $r(x)$  whose derivatives are of a form similar to  $r(x)$  itself (powers, exponential functions, etc.), it is desirable to have a method valid for more general ODEs (1), which we shall now develop. It is called the **method of variation of parameters** and is credited to Lagrange (Sec. 2.1). Here  $p$ ,  $q$ ,  $r$  in (1) may be variable (given functions of  $x$ ), but we assume that they are continuous on some open interval  $I$ .

Lagrange's method gives a particular solution  $y_p$  of (1) on  $I$  in the form

$$(2) \quad y_p(x) = -y_1 \int \frac{y_2 r}{W} dx + y_2 \int \frac{y_1 r}{W} dx$$

where  $y_1, y_2$  form a basis of solutions of the corresponding homogeneous ODE

$$(3) \quad y'' + p(x)y' + q(x)y = 0$$

on  $I$ , and  $W$  is the Wronskian of  $y_1, y_2$ ,

$$(4) \quad W = y_1y_2' - y_2y_1' \quad (\text{see Sec. 2.6}).$$

**CAUTION!** The solution formula (2) is obtained under the assumption that the ODE is written in standard form, with  $y''$  as the first term as shown in (1). If it starts with  $f(x)y''$ , divide first by  $f(x)$ .

The integration in (2) may often cause difficulties, and so may the determination of  $y_1, y_2$  if (1) has variable coefficients. If you have a choice, use the previous method. It is simpler. Before deriving (2) let us work an example for which you *do need* the new method. (Try otherwise.)

**EXAMPLE 1 Method of Variation of Parameters**

Solve the nonhomogeneous ODE

$$y'' + y = \sec x = \frac{1}{\cos x}.$$

**Solution.** A basis of solutions of the homogeneous ODE on any interval is  $y_1 = \cos x, y_2 = \sin x$ . This gives the Wronskian

$$W(y_1, y_2) = \cos x \cos x - \sin x (-\sin x) = 1.$$

From (2), choosing zero constants of integration, we get the particular solution of the given ODE

$$\begin{aligned} y_p &= -\cos x \int \sin x \sec x \, dx + \sin x \int \cos x \sec x \, dx \\ &= \cos x \ln |\cos x| + x \sin x \end{aligned} \quad (\text{Fig. 69}).$$

Figure 69 shows  $y_p$  and its first term, which is small, so that  $x \sin x$  essentially determines the shape of the curve of  $y_p$ . (Recall from Sec. 2.8 that we have seen  $x \sin x$  in connection with resonance, except for notation.) From  $y_p$  and the general solution  $y_h = c_1y_1 + c_2y_2$  of the homogeneous ODE we obtain the *answer*

$$y = y_h + y_p = (c_1 + \ln |\cos x|) \cos x + (c_2 + x) \sin x.$$

Had we included integration constants  $-c_1, c_2$  in (2), then (2) would have given the additional  $c_1 \cos x + c_2 \sin x = c_1y_1 + c_2y_2$ , that is, a general solution of the given ODE directly from (2). This will always be the case. ■

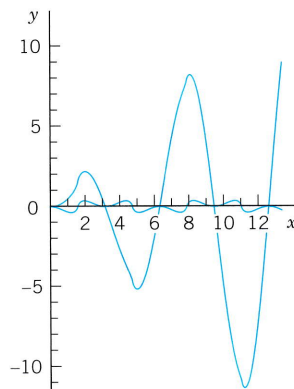


Fig. 69. Particular solution  $y_p$  and its first term in Example 1

## Idea of the Method. Derivation of (2)

What idea did Lagrange have? What gave the method the name? Where do we use the continuity assumptions?

The idea is to start from a general solution

$$y_h(x) = c_1 y_1(x) + c_2 y_2(x)$$

of the homogeneous ODE (3) on an open interval  $I$  and to replace the constants (“the parameters”)  $c_1$  and  $c_2$  by functions  $u(x)$  and  $v(x)$ ; this suggests the name of the method. We shall determine  $u$  and  $v$  so that the resulting function

$$(5) \quad y_p(x) = u(x)y_1(x) + v(x)y_2(x)$$

is a particular solution of the nonhomogeneous ODE (1). Note that  $y_h$  exists by Theorem 3 in Sec. 2.6 because of the continuity of  $p$  and  $q$  on  $I$ . (The continuity of  $r$  will be used later.)

We determine  $u$  and  $v$  by substituting (5) and its derivatives into (1). Differentiating (5), we obtain

$$y_p' = u'y_1 + uy_1' + v'y_2 + vy_2'$$

Now  $y_p$  must satisfy (1). This is *one* condition for *two* functions  $u$  and  $v$ . It seems plausible that we may impose a *second* condition. Indeed, our calculation will show that we can determine  $u$  and  $v$  such that  $y_p$  satisfies (1) and  $u$  and  $v$  satisfy as a second condition the equation

$$(6) \quad u'y_1 + v'y_2 = 0.$$

This reduces the first derivative  $y_p'$  to the simpler form

$$(7) \quad y_p' = uy_1' + vy_2'$$

Differentiating (7), we obtain

$$(8) \quad y_p'' = u'y_1' + uy_1'' + v'y_2' + vy_2''$$

We now substitute  $y_p$  and its derivatives according to (5), (7), (8) into (1). Collecting terms in  $u$  and terms in  $v$ , we obtain

$$u(y_1'' + py_1' + qy_1) + v(y_2'' + py_2' + qy_2) + u'y_1' + v'y_2' = r.$$

Since  $y_1$  and  $y_2$  are solutions of the homogeneous ODE (3), this reduces to

$$(9a) \quad u'y_1' + v'y_2' = r.$$

Equation (6) is

$$(9b) \quad u'y_1 + v'y_2 = 0.$$

This is a linear system of two algebraic equations for the unknown functions  $u'$  and  $v'$ . We can solve it by elimination as follows (or by Cramer's rule in Sec. 7.6). To eliminate  $v'$ , we multiply (9a) by  $-y_2$  and (9b) by  $y_2'$  and add, obtaining

$$u'(y_1y_2' - y_2y_1') = -y_2r, \quad \text{thus} \quad u'W = -y_2r.$$

Here,  $W$  is the Wronskian (4) of  $y_1, y_2$ . To eliminate  $u'$  we multiply (9a) by  $y_1$ , and (9b) by  $-y_1'$  and add, obtaining

$$v'(y_1y_2' - y_2y_1') = y_1r, \quad \text{thus} \quad v'W = y_1r.$$

Since  $y_1, y_2$  form a basis, we have  $W \neq 0$  (by Theorem 2 in Sec. 2.6) and can divide by  $W$ ,

$$(10) \quad u' = -\frac{y_2r}{W}, \quad v' = \frac{y_1r}{W}.$$

By integration,

$$u = -\int \frac{y_2r}{W} dx, \quad v = \int \frac{y_1r}{W} dx.$$

These integrals exist because  $r(x)$  is continuous. Inserting them into (5) gives (2) and completes the derivation. ■

## PROBLEM SET 2.10

### 1-17 GENERAL SOLUTION

Solve the given nonhomogeneous ODE by variation of parameters or undetermined coefficients. Give a general solution. (Show the details of your work.)

1.  $y'' + y = \csc x$
2.  $y'' - 4y' + 4y = x^2e^x$
3.  $x^2y'' - 2xy' + 2y = x^3 \cos x$
4.  $y'' - 2y' + y = e^x \sin x$
5.  $y'' + y = \tan x$
6.  $x^2y'' - xy' + y = x \ln |x|$
7.  $y'' + y = \cos x + \sec x$
8.  $y'' - 4y' + 4y = 12e^{2x}/x^4$
9.  $(D^2 - 2D + I)y = x^2 + x^{-2}e^x$
10.  $(D^2 - I)y = 1/\cosh x$
11.  $(D^2 + 4I)y = \cosh 2x$
12.  $(x^2D^2 + xD - \frac{1}{4}I)y = 3x^{-1} + 3x$
13.  $(x^2D^2 - 2xD + 2I)y = x^3 \sin x$

14.  $(x^2D^2 + xD - 4I)y = 1/x^2$
15.  $(D^2 + I)y = \sec x - 10 \sin 5x$
16.  $(x^2D^2 + xD + (x^2 - \frac{1}{4})I)y = x^{3/2} \cos x$ .  
*Hint.* To find  $y_1, y_2$  set  $y = ux^{-1/2}$ .
17.  $(x^2D^2 + xD + (x^2 - \frac{1}{4})I)y = x^{3/2} \sin x$ .  
*Hint:* As in Prob. 16.

18. **TEAM PROJECT. Comparison of Methods.** The undetermined-coefficient method should be used whenever possible because it is simpler. Compare it with the present method as follows.

- (a) Solve  $y'' + 2y' - 15y = 17 \sin 5x$  by both methods, showing all details, and compare.
- (b) Solve  $y'' + 9y = r_1 + r_2$ ,  $r_1 = \sec 3x$ ,  $r_2 = \sin 3x$  by applying each method to a suitable function on the right.
- (c) Invent an undetermined-coefficient method for nonhomogeneous Euler–Cauchy equations by experimenting.

## CHAPTER 2 REVIEW QUESTIONS AND PROBLEMS

1. What general properties make *linear* ODEs particularly attractive?
2. What is a general solution of a linear ODE? A basis of solutions?
3. How would you obtain a general solution of a nonhomogeneous linear ODE if you knew a general solution of the corresponding homogeneous ODE?
4. What does an initial value problem for a second-order ODE look like?
5. What is a particular solution and why is it more common than a general solution as the answer to practical problems?
6. Why are second-order ODEs more important in modeling than ODEs of higher order?
7. Describe the applications of ODEs in mechanical vibrating systems. What are the electrical analogs of those systems?
8. If a construction, such as a bridge, shows undesirable resonance, what could you do?

### 9–18 GENERAL SOLUTION

Find a general solution. Indicate the method you are using and show the details of your calculation.

9.  $y'' - 2y' - 8y = 52 \cos 6x$
10.  $y'' + 6y' + 9y = e^{-3x} - 27x^2$
11.  $y'' + 8y' + 25y = 26 \sin 3x$
12.  $yy'' = 2y'^2$
13.  $(x^2D^2 + 2xD - 12I)y = 1/x^3$
14.  $(x^2D^2 + 6xD + 6I)y = x^2$
15.  $(D^2 - 2D + I)y = x^{-3}e^x$
16.  $(D^2 - 4D + 5I)y = e^{2x} \csc x$
17.  $(D^2 - 2D + 2I)y = e^x \csc x$
18.  $(4x^2D^2 - 24xD + 49I)y = 36x^5$

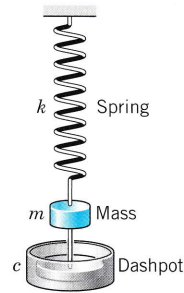
### 19–25 INITIAL VALUE PROBLEMS

Solve the following initial value problems. Sketch or graph the solution. (Show the details of your work.)

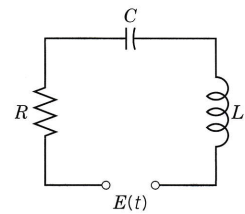
19.  $y'' + 5y' - 14y = 0$ ,  $y(0) = 6$ ,  $y'(0) = -6$
20.  $y'' + 6y' + 18y = 0$ ,  $y(0) = 5$ ,  $y'(0) = -21$
21.  $x^2y'' - xy' - 24y = 0$ ,  $y(1) = 15$ ,  $y'(1) = 0$
22.  $x^2y'' + 15xy' + 49y = 0$ ,  $y(1) = 2$ ,  $y'(1) = -11$
23.  $y'' + 5y' + 6y = 108x^2$ ,  $y(0) = 18$ ,  $y'(0) = -26$
24.  $y'' + y' + 2.5y = 13 \cos x$ ,  $y(0) = 8.0$ ,  $y'(0) = 4.5$
25.  $(x^2D^2 + xD - 4I)y = x^3$ ,  $y(1) = -4/5$ ,  $y'(1) = 93/5$

### 26–34 APPLICATIONS

26. Find the steady-state solution of the system in Fig. 70 when  $m = 4$ ,  $c = 4$ ,  $k = 17$  and the driving force is  $202 \cos 3t$ .
27. Find the motion of the system in Fig. 70 with mass 0.25 kg, no damping, spring constant 1 kg/sec<sup>2</sup>, and driving force  $15 \cos 0.5t - 7 \sin 1.5t$  nt, assuming zero initial displacement and velocity. For what frequency of the driving force would you get resonance?
28. In Prob. 26 find the solution corresponding to initial displacement 10 and initial velocity 0.
29. Show that the system in Fig. 70 with  $m = 4$ ,  $c = 0$ ,  $k = 36$ , and driving force  $61 \cos 3.1t$  exhibits beats. *Hint:* Choose zero initial conditions.
30. In Fig. 70 let  $m = 2$ ,  $c = 6$ ,  $k = 27$ , and  $r(t) = 10 \cos \omega t$ . For what  $\omega$  will you obtain the steady-state vibration of maximum possible amplitude? Determine this amplitude. Then use this  $\omega$  and the undetermined-coefficient method to see whether you obtain the same amplitude.
31. Find an electrical analog of the mass–spring system in Fig. 70 with mass 0.5 kg, spring constant 40 kg/sec<sup>2</sup>, damping constant 9 kg/sec, and driving force  $102 \cos 6t$  nt. Solve the analog, assuming zero initial current and charge.
32. Find the current in the *RLC*-circuit in Fig. 71 when  $L = 0.1$  H,  $R = 20 \Omega$ ,  $C = 2 \cdot 10^{-4}$  F, and  $E(t) = 110 \sin 415t$  V (66 cycles/sec).
33. Find the current in the *RLC*-circuit when  $L = 0.4$  H,  $R = 40 \Omega$ ,  $C = 10^{-4}$  F, and  $E(t) = 220 \sin 314t$  V (50 cycles/sec).
34. Find a particular solution in Prob. 33 by the complex method. (See Team Project 20 in Sec. 2.9.)



**Fig. 70.** Mass–spring system



**Fig. 71.** *RLC*-circuit

## SUMMARY OF CHAPTER 2

## Second-Order Linear ODEs

Second-order linear ODEs are particularly important in applications, for instance, in mechanics (Secs. 2.4, 2.8) and electrical engineering (Sec. 2.9). A second-order ODE is called **linear** if it can be written

$$(1) \quad y'' + p(x)y' + q(x)y = r(x) \quad (\text{Sec. 2.1}).$$

(If the first term is, say,  $f(x)y''$ , divide by  $f(x)$  to get the “**standard form**” (1) with  $y''$  as the first term.) Equation (1) is called **homogeneous** if  $r(x)$  is zero for all  $x$  considered, usually in some open interval; this is written  $r(x) \equiv 0$ . Then

$$(2) \quad y'' + p(x)y' + q(x)y = 0.$$

Equation (1) is called **nonhomogeneous** if  $r(x) \neq 0$  (meaning  $r(x)$  is not zero for some  $x$  considered).

For the homogeneous ODE (2) we have the important **superposition principle** (Sec. 2.1) that a linear combination  $y = ky_1 + ly_2$  of two solutions  $y_1, y_2$  is again a solution.

Two *linearly independent* solutions  $y_1, y_2$  of (2) on an open interval  $I$  form a **basis** (or **fundamental system**) of solutions on  $I$ , and  $y = c_1y_1 + c_2y_2$  with arbitrary constants  $c_1, c_2$  is a **general solution** of (2) on  $I$ . From it we obtain a **particular solution** if we specify numeric values (numbers) for  $c_1$  and  $c_2$ , usually by prescribing two **initial conditions**

$$(3) \quad y(x_0) = K_0, \quad y'(x_0) = K_1 \quad (x_0, K_0, K_1 \text{ given numbers; Sec. 2.1}).$$

(2) and (3) together form an **initial value problem**. Similarly for (1) and (3).

For a nonhomogeneous ODE (1) a **general solution** is of the form

$$(4) \quad y = y_h + y_p \quad (\text{Sec. 2.7}).$$

Here  $y_h$  is a general solution of (2) and  $y_p$  is a particular solution of (1). Such a  $y_p$  can be determined by a general method (**variation of parameters**, Sec. 2.10) or in many practical cases by the **method of undetermined coefficients**. The latter applies when (1) has constant coefficients  $p$  and  $q$ , and  $r(x)$  is a power of  $x$ , sine, cosine, etc. (Sec. 2.7). Then we write (1) as

$$(5) \quad y'' + ay' + by = r(x) \quad (\text{Sec. 2.7}).$$

The corresponding homogeneous ODE  $y'' + ay' + by = 0$  has solutions  $y = e^{\lambda x}$ , where  $\lambda$  is a root of

$$(6) \quad \lambda^2 + a\lambda + b = 0.$$



Hence there are three cases (Sec. 2.2):

Case	Type of Roots	General Solution
I	Distinct real $\lambda_1, \lambda_2$	$y = c_1 e^{\lambda_1 x} + c_2 e^{\lambda_2 x}$
II	Double $-\frac{1}{2}a$	$y = (c_1 + c_2 x) e^{-ax/2}$
III	Complex $-\frac{1}{2}a \pm i\omega^*$	$y = e^{-ax/2}(A \cos \omega^* x + B \sin \omega^* x)$

Important applications of (5) in mechanical and electrical engineering in connection with **vibrations** and **resonance** are discussed in Secs. 2.4, 2.7, and 2.8.

Another large class of ODEs solvable “algebraically” consists of the **Euler–Cauchy equations**

$$(7) \quad x^2 y'' + axy' + by = 0 \quad (\text{Sec. 2.5}).$$

These have solutions of the form  $y = x^m$ , where  $m$  is a solution of the auxiliary equation

$$(8) \quad m^2 + (a - 1)m + b = 0.$$

**Existence and uniqueness** of solutions of (1) and (2) is discussed in Secs. 2.6 and 2.7, and **reduction of order** in Sec. 2.1.

## Higher Order Linear ODEs

In this chapter we extend the concepts and methods of Chap. 2 for linear ODEs from order  $n = 2$  to arbitrary order  $n$ . This will be straightforward and needs no new ideas. However, the formulas become more involved, the variety of roots of the characteristic equation (in Sec. 3.2) becomes much larger with increasing  $n$ , and the Wronskian plays a more prominent role.

*Prerequisite:* Secs. 2.1, 2.2, 2.6, 2.7, 2.10.

*References and Answers to Problems:* App. 1 Part A, and App. 2.

## 3.1 Homogeneous Linear ODEs

Recall from Sec. 1.1 that an ODE is of  **$n$ th order** if the  $n$ th derivative  $y^{(n)} = d^n y/dx^n$  of the unknown function  $y(x)$  is the highest occurring derivative. Thus the ODE is of the form

$$F(x, y, y', \dots, y^{(n)}) = 0 \quad \left( y^{(n)} = \frac{d^n y}{dx^n} \right)$$

where lower order derivatives and  $y$  itself may or may not occur. Such an ODE is called **linear** if it can be written

$$(1) \quad y^{(n)} + p_{n-1}(x)y^{(n-1)} + \dots + p_1(x)y' + p_0(x)y = r(x).$$

(For  $n = 2$  this is (1) in Sec. 2.1 with  $p_1 = p$  and  $p_0 = q$ ). The **coefficients**  $p_0, \dots, p_{n-1}$  and the function  $r$  on the right are any given functions of  $x$ , and  $y$  is unknown.  $y^{(n)}$  has coefficient 1. This is practical. We call this the **standard form**. (If you have  $p_n(x)y^{(n)}$ , divide by  $p_n(x)$  to get this form.) An  $n$ th-order ODE that cannot be written in the form (1) is called **nonlinear**.

If  $r(x)$  is identically zero,  $r(x) \equiv 0$  (zero for all  $x$  considered, usually in some open interval  $I$ ), then (1) becomes

$$(2) \quad y^{(n)} + p_{n-1}(x)y^{(n-1)} + \dots + p_1(x)y' + p_0(x)y = 0$$

and is called **homogeneous**. If  $r(x)$  is not identically zero, then the ODE is called **nonhomogeneous**. This is as in Sec. 2.1.

A **solution** of an  $n$ th-order (linear or nonlinear) ODE on some open interval  $I$  is a function  $y = h(x)$  that is defined and  $n$  times differentiable on  $I$  and is such that the ODE becomes an identity if we replace the unknown function  $y$  and its derivatives by  $h$  and its corresponding derivatives.

## Homogeneous Linear ODE: Superposition Principle, General Solution

Sections 3.1–3.2 will be devoted to homogeneous linear ODEs and Sec. 3.3 to nonhomogeneous linear ODEs. The basic **superposition or linearity principle** in Sec. 2.1 extends to  $n$ th order homogeneous linear ODEs as follows.

### THEOREM 1

#### Fundamental Theorem for the Homogeneous Linear ODE (2)

For a homogeneous linear ODE (2), sums and constant multiples of solutions on some open interval  $I$  are again solutions on  $I$ . (This does **not** hold for a nonhomogeneous or nonlinear ODE!)

The proof is a simple generalization of that in Sec. 2.1 and we leave it to the student.

Our further discussion parallels and extends that for second-order ODEs in Sec. 2.1. So we define next a general solution of (2), which will require an extension of linear independence from 2 to  $n$  functions.

### DEFINITION

#### General Solution, Basis, Particular Solution

A **general solution** of (2) on an open interval  $I$  is a solution of (2) on  $I$  of the form

$$(3) \quad y(x) = c_1 y_1(x) + \cdots + c_n y_n(x) \quad (c_1, \cdots, c_n \text{ arbitrary})$$

where  $y_1, \cdots, y_n$  is a **basis** (or **fundamental system**) of solutions of (2) on  $I$ ; that is, these solutions are linearly independent on  $I$ , as defined below.

A **particular solution** of (2) on  $I$  is obtained if we assign specific values to the  $n$  constants  $c_1, \cdots, c_n$  in (3).

### DEFINITION

#### Linear Independence and Dependence

$n$  functions  $y_1(x), \cdots, y_n(x)$  are called **linearly independent** on some interval  $I$  where they are defined if the equation

$$(4) \quad k_1 y_1(x) + \cdots + k_n y_n(x) = 0 \quad \text{on } I$$

implies that all  $k_1, \cdots, k_n$  are zero. These functions are called **linearly dependent** on  $I$  if this equation also holds on  $I$  for some  $k_1, \cdots, k_n$  not all zero.

(As in Secs. 1.1 and 2.1, the arbitrary constants  $c_1, \cdots, c_n$  must sometimes be restricted to some interval.)

If and only if  $y_1, \cdots, y_n$  are linearly dependent on  $I$ , we can express (at least) one of these functions on  $I$  as a “**linear combination**” of the other  $n - 1$  functions, that is, as a sum of those functions, each multiplied by a constant (zero or not). This motivates the term “linearly dependent.” For instance, if (4) holds with  $k_1 \neq 0$ , we can divide by  $k_1$  and express  $y_1$  as the linear combination

$$y_1 = -\frac{1}{k_1}(k_2 y_2 + \cdots + k_n y_n).$$

Note that when  $n = 2$ , these concepts reduce to those defined in Sec. 2.1.

### EXAMPLE 1 Linear Dependence

Show that the functions  $y_1 = x^2$ ,  $y_2 = 5x$ ,  $y_3 = 2x$  are linearly dependent on any interval.

**Solution.**  $y_2 = 0y_1 + 2.5y_3$ . This proves linear dependence on any interval. ■

### EXAMPLE 2 Linear Independence

Show that  $y_1 = x$ ,  $y_2 = x^2$ ,  $y_3 = x^3$  are linearly independent on any interval, for instance, on  $-1 \leq x \leq 2$ .

**Solution.** Equation (4) is  $k_1 x + k_2 x^2 + k_3 x^3 = 0$ . Taking (a)  $x = -1$ , (b)  $x = 1$ , (c)  $x = 2$ , we get

$$(a) -k_1 + k_2 - k_3 = 0, \quad (b) k_1 + k_2 + k_3 = 0, \quad (c) 2k_1 + 4k_2 + 8k_3 = 0.$$

$k_2 = 0$  from (a) + (b). Then  $k_3 = 0$  from (c) - 2(b). Then  $k_1 = 0$  from (b). This proves linear independence.

A better method for testing linear independence of solutions of ODEs will soon be explained. ■

### EXAMPLE 3 General Solution. Basis

Solve the fourth-order ODE

$$y^{iv} - 5y'' + 4y = 0 \quad (\text{where } y^{iv} = d^4y/dx^4).$$

**Solution.** As in Sec. 2.2 we try and substitute  $y = e^{\lambda x}$ . Omitting the common factor  $e^{\lambda x}$ , we obtain the characteristic equation

$$\lambda^4 - 5\lambda^2 + 4 = 0.$$

This is a quadratic equation in  $\mu = \lambda^2$ , namely,

$$\mu^2 - 5\mu + 4 = (\mu - 1)(\mu - 4) = 0.$$

The roots are  $\mu = 1$  and  $4$ . Hence  $\lambda = -2, -1, 1, 2$ . This gives four solutions. A general solution on any interval is

$$y = c_1 e^{-2x} + c_2 e^{-x} + c_3 e^x + c_4 e^{2x}$$

provided those four solutions are linearly independent. This is true but will be shown later. ■

## Initial Value Problem. Existence and Uniqueness

An **initial value problem** for the ODE (2) consists of (2) and  $n$  **initial conditions**

$$(5) \quad y(x_0) = K_0, \quad y'(x_0) = K_1, \quad \cdots, \quad y^{(n-1)}(x_0) = K_{n-1}$$

with given  $x_0$  in the open interval  $I$  considered, and given  $K_0, \cdots, K_{n-1}$ .

In extension of the existence and uniqueness theorem in Sec. 2.6 we now have the following.

### THEOREM 2

#### Existence and Uniqueness Theorem for Initial Value Problems

If the coefficients  $p_0(x), \cdots, p_{n-1}(x)$  of (2) are continuous on some open interval  $I$  and  $x_0$  is in  $I$ , then the initial value problem (2), (5) has a unique solution  $y(x)$  on  $I$ .

Existence is proved in Ref. [A11] in App. 1. Uniqueness can be proved by a slight generalization of the uniqueness proof at the beginning of App. 4.

**EXAMPLE 4** Initial Value Problem for a Third-Order Euler–Cauchy Equation

Solve the following initial value problem on any open interval  $I$  on the positive  $x$ -axis containing  $x = 1$ .

$$x^3 y''' - 3x^2 y'' + 6xy' - 6y = 0, \quad y(1) = 2, \quad y'(1) = 1, \quad y''(1) = -4.$$

**Solution.** *Step 1. General solution.* As in Sec. 2.5 we try  $y = x^m$ . By differentiation and substitution,

$$m(m-1)(m-2)x^m - 3m(m-1)x^m + 6mx^m - 6x^m = 0.$$

Dropping  $x^m$  and ordering gives  $m^3 - 6m^2 + 11m - 6 = 0$ . If we can guess the root  $m = 1$ , we can divide by  $m - 1$  and find the other roots 2 and 3, thus obtaining the solutions  $x, x^2, x^3$ , which are linearly independent on  $I$  (see Example 2). [In general one shall need a root-finding method, such as Newton's (Sec. 19.2), also available in a CAS (Computer Algebra System).] Hence a general solution is

$$y = c_1 x + c_2 x^2 + c_3 x^3$$

valid on any interval  $I$ , even when it includes  $x = 0$  where the coefficients of the ODE divided by  $x^3$  (to have the standard form) are not continuous.

*Step 2. Particular solution.* The derivatives are  $y' = c_1 + 2c_2 x + 3c_3 x^2$  and  $y'' = 2c_2 + 6c_3 x$ . From this and  $y$  and the initial conditions we get by setting  $x = 1$

$$(a) \quad y(1) = c_1 + c_2 + c_3 = 2$$

$$(b) \quad y'(1) = c_1 + 2c_2 + 3c_3 = 1$$

$$(c) \quad y''(1) = 2c_2 + 6c_3 = -4.$$

This is solved by Cramer's rule (Sec. 7.6), or by elimination, which is simple, as follows. (b) - (a) gives (d)  $c_2 + 2c_3 = -1$ . Then (c) - 2(d) gives  $c_3 = -1$ . Then (c) gives  $c_2 = 1$ . Finally  $c_1 = 2$  from (a).  
*Answer:*  $y = 2x + x^2 - x^3$ . ■

## Linear Independence of Solutions. Wronskian

Linear independence of solutions is crucial for obtaining general solutions. Although it can often be seen by inspection, it would be good to have a criterion for it. Now Theorem 2 in Sec. 2.6 extends from order  $n = 2$  to any  $n$ . This extended criterion uses the **Wronskian**  $W$  of  $n$  solutions  $y_1, \dots, y_n$  defined as the  $n$ th order determinant

$$(6) \quad W(y_1, \dots, y_n) = \begin{vmatrix} y_1 & y_2 & \cdots & y_n \\ y_1' & y_2' & \cdots & y_n' \\ \cdot & \cdot & \cdots & \cdot \\ y_1^{(n-1)} & y_2^{(n-1)} & \cdots & y_n^{(n-1)} \end{vmatrix}.$$

Note that  $W$  depends on  $x$  since  $y_1, \dots, y_n$  does. The criterion states that these solutions form a basis if and only if  $W$  is not zero; more precisely:

### THEOREM 3

#### Linear Dependence and Independence of Solutions

Let the ODE (2) have continuous coefficients  $p_0(x), \dots, p_{n-1}(x)$  on an open interval  $I$ . Then  $n$  solutions  $y_1, \dots, y_n$  of (2) on  $I$  are linearly dependent on  $I$  if and only if their Wronskian is zero for some  $x = x_0$  in  $I$ . Furthermore, if  $W$  is zero for  $x = x_0$ , then  $W$  is identically zero on  $I$ . Hence if there is an  $x_1$  in  $I$  at which  $W$  is not zero, then  $y_1, \dots, y_n$  are linearly independent on  $I$ , so that they form a basis of solutions of (2) on  $I$ .

**PROOF** (a) Let  $y_1, \dots, y_n$  be linearly dependent solutions of (2) on  $I$ . Then, by definition, there are constants  $k_1, \dots, k_n$  not all zero, such that for all  $x$  in  $I$ ,

$$(7) \quad k_1 y_1 + \dots + k_n y_n = 0.$$

By  $n - 1$  differentiations of (7) we obtain for all  $x$  in  $I$

$$(8) \quad \begin{aligned} k_1 y_1' + \dots + k_n y_n' &= 0 \\ &\vdots \\ k_1 y_1^{(n-1)} + \dots + k_n y_n^{(n-1)} &= 0. \end{aligned}$$

(7), (8) is a homogeneous linear system of algebraic equations with a nontrivial solution  $k_1, \dots, k_n$ . Hence its coefficient determinant must be zero for every  $x$  on  $I$ , by Cramer's theorem (Sec. 7.7). But that determinant is the Wronskian  $W$ , as we see from (6). Hence  $W$  is zero for every  $x$  on  $I$ .

(b) Conversely, if  $W$  is zero at an  $x_0$  in  $I$ , then the system (7), (8) with  $x = x_0$  has a solution  $k_1^*, \dots, k_n^*$ , not all zero, by the same theorem. With these constants we define the solution  $y^* = k_1^* y_1 + \dots + k_n^* y_n$  of (2) on  $I$ . By (7), (8) this solution satisfies the initial conditions  $y^*(x_0) = 0, \dots, y^{*(n-1)}(x_0) = 0$ . But another solution satisfying the same conditions is  $y \equiv 0$ . Hence  $y^* \equiv y$  by Theorem 2, which applies since the coefficients of (2) are continuous. Together,  $y^* = k_1^* y_1 + \dots + k_n^* y_n \equiv 0$  on  $I$ . This means linear dependence of  $y_1, \dots, y_n$  on  $I$ .

(c) If  $W$  is zero at an  $x_0$  in  $I$ , we have linear dependence by (b) and then  $W \equiv 0$  by (a). Hence if  $W$  is not zero at an  $x_1$  in  $I$ , the solutions  $y_1, \dots, y_n$  must be linearly independent on  $I$ . ■

**EXAMPLE 5** Basis, Wronskian

We can now prove that in Example 3 we do have a basis. In evaluating  $W$ , pull out the exponential functions columnwise. In the result, subtract Column 1 from Columns 2, 3, 4 (without changing Column 1). Then expand by Row 1. In the resulting third-order determinant, subtract Column 1 from Column 2 and expand the result by Row 2:

$$W = \begin{vmatrix} e^{-2x} & e^{-x} & e^x & e^{2x} \\ -2e^{-2x} & -e^{-x} & e^x & 2e^{2x} \\ 4e^{-2x} & e^{-x} & e^x & 4e^{2x} \\ -8e^{-2x} & -e^{-x} & e^x & 8e^{2x} \end{vmatrix} = \begin{vmatrix} 1 & 1 & 1 & 1 \\ -2 & -1 & 1 & 2 \\ 4 & 1 & 1 & 4 \\ -8 & -1 & 1 & 8 \end{vmatrix} = \begin{vmatrix} 1 & 3 & 4 \\ -3 & -3 & 0 \\ 7 & 9 & 16 \end{vmatrix} = 72. \quad \blacksquare$$

**A General Solution of (2) Includes All Solutions**

Let us first show that general solutions always exist. Indeed, Theorem 3 in Sec. 2.6 extends as follows.

**THEOREM 4**

**Existence of a General Solution**

If the coefficients  $p_0(x), \dots, p_{n-1}(x)$  of (2) are continuous on some open interval  $I$ , then (2) has a general solution on  $I$ .

**PROOF** We choose any fixed  $x_0$  in  $I$ . By Theorem 2 the ODE (2) has  $n$  solutions  $y_1, \dots, y_n$ , where  $y_j$  satisfies initial conditions (5) with  $K_{j-1} = 1$  and all other  $K$ 's equal to zero. Their Wronskian at  $x_0$  equals 1. For instance, when  $n = 3$ , then  $y_1(x_0) = 1$ ,  $y_2'(x_0) = 1$ ,  $y_3''(x_0) = 1$ , and the other initial values are zero. Thus, as claimed,

$$W(y_1(x_0), y_2(x_0), y_3(x_0)) = \begin{vmatrix} y_1(x_0) & y_2(x_0) & y_3(x_0) \\ y_1'(x_0) & y_2'(x_0) & y_3'(x_0) \\ y_1''(x_0) & y_2''(x_0) & y_3''(x_0) \end{vmatrix} = \begin{vmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{vmatrix} = 1.$$

Hence for any  $n$  those solutions  $y_1, \dots, y_n$  are linearly independent on  $I$ , by Theorem 3. They form a basis on  $I$ , and  $y = c_1y_1 + \dots + c_ny_n$  is a general solution of (2) on  $I$ . ■

We can now prove the basic property that from a general solution of (2) every solution of (2) can be obtained by choosing suitable values of the arbitrary constants. Hence an  $n$ th order **linear** ODE has no **singular solutions**, that is, solutions that cannot be obtained from a general solution.

### THEOREM 5

#### General Solution Includes All Solutions

If the ODE (2) has continuous coefficients  $p_0(x), \dots, p_{n-1}(x)$  on some open interval  $I$ , then every solution  $y = Y(x)$  of (2) on  $I$  is of the form

$$(9) \quad Y(x) = C_1y_1(x) + \dots + C_ny_n(x)$$

where  $y_1, \dots, y_n$  is a basis of solutions of (2) on  $I$  and  $C_1, \dots, C_n$  are suitable constants.

**PROOF** Let  $Y$  be a given solution and  $y = c_1y_1 + \dots + c_ny_n$  a general solution of (2) on  $I$ . We choose any fixed  $x_0$  in  $I$  and show that we can find constants  $c_1, \dots, c_n$  for which  $y$  and its first  $n - 1$  derivatives agree with  $Y$  and its corresponding derivatives at  $x_0$ . That is, we should have at  $x = x_0$

$$(10) \quad \begin{aligned} c_1y_1 + \dots + c_ny_n &= Y \\ c_1y_1' + \dots + c_ny_n' &= Y' \\ &\vdots \\ c_1y_1^{(n-1)} + \dots + c_ny_n^{(n-1)} &= Y^{(n-1)}. \end{aligned}$$

But this is a linear system of equations in the unknowns  $c_1, \dots, c_n$ . Its coefficient determinant is the Wronskian  $W$  of  $y_1, \dots, y_n$  at  $x_0$ . Since  $y_1, \dots, y_n$  form a basis, they are linearly independent, so that  $W$  is not zero by Theorem 3. Hence (10) has a unique solution  $c_1 = C_1, \dots, c_n = C_n$  (by Cramer's theorem in Sec. 7.7). With these values we obtain the particular solution

$$y^*(x) = C_1y_1(x) + \dots + C_ny_n(x)$$

on  $I$ . Equation (10) shows that  $y^*$  and its first  $n - 1$  derivatives agree at  $x_0$  with  $Y$  and its corresponding derivatives. That is,  $y^*$  and  $Y$  satisfy at  $x_0$  the same initial conditions.

The uniqueness theorem (Theorem 2) now implies that  $y^* \equiv Y$  on  $I$ . This proves the theorem. ■

This completes our theory of the homogeneous linear ODE (2). Note that for  $n = 2$  it is identical with that in Sec. 2.6. This had to be expected.

### PROBLEM SET 3.1

#### 1-5 TYPICAL EXAMPLES OF BASES

To get a feel for higher order ODEs, show that the given functions are solutions and form a basis on any interval. Use Wronskians. (In Prob. 2,  $x > 0$ .)

1.  $1, x, x^2, x^3, y^{iv} = 0$
2.  $1, x^2, x^4, x^2 y''' - 3xy'' + 3y' = 0$
3.  $e^x, xe^x, x^2 e^x, y''' - 3y'' + 3y' - y = 0$
4.  $e^{2x} \cos x, e^{2x} \sin x, e^{-2x} \cos x, e^{-2x} \sin x, y^{iv} - 6y''' + 25y'' = 0$
5.  $1, x, \cos 3x, \sin 3x, y^{iv} + 9y'' = 0$

6. **TEAM PROJECT. General Properties of Solutions of Linear ODEs.** These properties are important in obtaining new solutions from given ones. Therefore extend Team Project 34 in Sec. 2.2 to  $n$ th-order ODEs. Explore statements on sums and multiples of solutions of (1) and (2) systematically and with proofs. Recognize clearly that no new ideas are needed in this extension from  $n = 2$  to general  $n$ .

#### 7-19 LINEAR INDEPENDENCE AND DEPENDENCE

Are the given functions linearly independent or dependent on the positive  $x$ -axis? (Give a reason.)

7.  $1, e^x, e^{-x}$
8.  $x + 1, x + 2, x$
9.  $\ln x, \ln x^2, (\ln x)^2$
10.  $e^x, e^{-x}, \sinh 2x$

11.  $x^2, x|x|, x$
12.  $x, 1/x, 0$
13.  $\sin 2x, \sin x, \cos x$
14.  $\cos^2 x, \sin^2 x, \cos 2x$
15.  $\tan x, \cot x, 1$
16.  $(x - 1)^2, (x + 1)^2, x$
17.  $\sin x, \sin \frac{1}{2}x$
18.  $\cosh x, \sinh x, \cosh^2 x$
19.  $\cos^2 x, \sin^2 x, 2\pi$

20. **TEAM PROJECT. Linear Independence and Dependence.** (a) Investigate the given question about a set  $S$  of functions on an interval  $I$ . Give an example. Prove your answer.

(1) If  $S$  contains the zero function, can  $S$  be linearly independent?

(2) If  $S$  is linearly independent on a subinterval  $J$  of  $I$ , is it linearly independent on  $I$ ?

(3) If  $S$  is linearly dependent on a subinterval  $J$  of  $I$ , is it linearly dependent on  $I$ ?

(4) If  $S$  is linearly independent on  $I$ , is it linearly independent on a subinterval  $J$ ?

(5) If  $S$  is linearly dependent on  $I$ , is it linearly dependent on a subinterval  $J$ ?

(6) If  $S$  is linearly dependent on  $I$ , and if  $T$  contains  $S$ , is  $T$  linearly dependent on  $I$ ?

(b) In what cases can you use the Wronskian for testing linear independence? By what other means can you perform such a test?

## 3.2 Homogeneous Linear ODEs with Constant Coefficients

In this section we consider  $n$ th-order homogeneous linear ODEs with constant coefficients, which we write in the form

$$(1) \quad y^{(n)} + a_{n-1}y^{(n-1)} + \cdots + a_1y' + a_0y = 0$$

where  $y^{(n)} = d^n y/dx^n$ , etc. We shall see that this extends the case  $n = 2$  discussed in Sec. 2.2. Substituting  $y = e^{\lambda x}$  (as in Sec. 2.2), we obtain the characteristic equation

$$(2) \quad \lambda^n + a_{n-1}\lambda^{(n-1)} + \cdots + a_1\lambda + a_0 = 0$$



of (1). If  $\lambda$  is a root of (2), then  $y = e^{\lambda x}$  is a solution of (1). To find these roots, you may need a numeric method, such as Newton's in Sec. 19.2, also available on the usual CASs. For general  $n$  there are more cases than for  $n = 2$ . We shall discuss all of them and illustrate them with typical examples.

## Distinct Real Roots

If all the  $n$  roots  $\lambda_1, \dots, \lambda_n$  of (2) are real and different, then the  $n$  solutions

$$(3) \quad y_1 = e^{\lambda_1 x}, \quad \dots, \quad y_n = e^{\lambda_n x}$$

constitute a basis for all  $x$ . The corresponding general solution of (1) is

$$(4) \quad y = c_1 e^{\lambda_1 x} + \dots + c_n e^{\lambda_n x}.$$

Indeed, the solutions in (3) are linearly independent, as we shall see after the example.

### EXAMPLE 1 Distinct Real Roots

Solve the ODE  $y''' - 2y'' - y' + 2y = 0$ .

**Solution.** The characteristic equation is  $\lambda^3 - 2\lambda^2 - \lambda + 2 = 0$ . It has the roots  $-1, 1, 2$ ; if you find one of them by inspection, you can obtain the other two roots by solving a quadratic equation (explain!). The corresponding general solution (4) is  $y = c_1 e^{-x} + c_2 e^x + c_3 e^{2x}$ . ■

**Linear Independence of (3).** Students familiar with  $n$ th-order determinants may verify that by pulling out all exponential functions from the columns and denoting their product by  $E$ , thus  $E = \exp[(\lambda_1 + \dots + \lambda_n)x]$ , the Wronskian of the solutions in (3) becomes

$$(5) \quad W = \begin{vmatrix} e^{\lambda_1 x} & e^{\lambda_2 x} & \dots & e^{\lambda_n x} \\ \lambda_1 e^{\lambda_1 x} & \lambda_2 e^{\lambda_2 x} & \dots & \lambda_n e^{\lambda_n x} \\ \lambda_1^2 e^{\lambda_1 x} & \lambda_2^2 e^{\lambda_2 x} & \dots & \lambda_n^2 e^{\lambda_n x} \\ \cdot & \cdot & \dots & \cdot \\ \lambda_1^{n-1} e^{\lambda_1 x} & \lambda_2^{n-1} e^{\lambda_2 x} & \dots & \lambda_n^{n-1} e^{\lambda_n x} \end{vmatrix}$$

$$= E \begin{vmatrix} 1 & 1 & \dots & 1 \\ \lambda_1 & \lambda_2 & \dots & \lambda_n \\ \lambda_1^2 & \lambda_2^2 & \dots & \lambda_n^2 \\ \cdot & \cdot & \dots & \cdot \\ \lambda_1^{n-1} & \lambda_2^{n-1} & \dots & \lambda_n^{n-1} \end{vmatrix}.$$

The exponential function  $E$  is never zero. Hence  $W = 0$  if and only if the determinant on the right is zero. This is a so-called **Vandermonde** or **Cauchy determinant**<sup>1</sup>. It can be shown that it equals

<sup>1</sup>ALEXANDRE THÉOPHILE VANDERMONDE (1735–1796), French mathematician, who worked on solution of equations by determinants. For CAUCHY see footnote 4, in Sec. 2.5.

$$(6) \quad (-1)^{n(n-1)/2} V$$

where  $V$  is the product of all factors  $\lambda_j - \lambda_k$  with  $j < k$  ( $\leq n$ ); for instance, when  $n = 3$  we get  $-V = -(\lambda_1 - \lambda_2)(\lambda_1 - \lambda_3)(\lambda_2 - \lambda_3)$ . This shows that the Wronskian is not zero if and only if all the  $n$  roots of (2) are different and thus gives the following.

**THEOREM 1****Basis**

Solutions  $y_1 = e^{\lambda_1 x}, \dots, y_n = e^{\lambda_n x}$  of (1) (with any real or complex  $\lambda_j$ 's) form a basis of solutions of (1) on any open interval if and only if all  $n$  roots of (2) are different.

Actually, Theorem 1 is an important special case of our more general result obtained from (5) and (6):

**THEOREM 2****Linear Independence**

Any number of solutions of (1) of the form  $e^{\lambda x}$  are linearly independent on an open interval  $I$  if and only if the corresponding  $\lambda$  are all different.

## Simple Complex Roots

If complex roots occur, they must occur in conjugate pairs since the coefficients of (1) are real. Thus, if  $\lambda = \gamma + i\omega$  is a simple root of (2), so is the conjugate  $\bar{\lambda} = \gamma - i\omega$ , and two corresponding linearly independent solutions are (as in Sec. 2.2, except for notation)

$$y_1 = e^{\gamma x} \cos \omega x, \quad y_2 = e^{\gamma x} \sin \omega x.$$

**EXAMPLE 2****Simple Complex Roots. Initial Value Problem**

Solve the initial value problem

$$y''' - y'' + 100y' - 100y = 0, \quad y(0) = 4, \quad y'(0) = 11, \quad y''(0) = -299.$$

**Solution.** The characteristic equation is  $\lambda^3 - \lambda^2 + 100\lambda - 100 = 0$ . It has the root 1, as can perhaps be seen by inspection. Then division by  $\lambda - 1$  shows that the other roots are  $\pm 10i$ . Hence a general solution and its derivatives (obtained by differentiation) are

$$\begin{aligned} y &= c_1 e^x + A \cos 10x + B \sin 10x, \\ y' &= c_1 e^x - 10A \sin 10x + 10B \cos 10x, \\ y'' &= c_1 e^x - 100A \cos 10x - 100B \sin 10x. \end{aligned}$$

From this and the initial conditions we obtain by setting  $x = 0$

$$(a) \quad c_1 + A = 4, \quad (b) \quad c_1 + 10B = 11, \quad (c) \quad c_1 - 100A = -299.$$

We solve this system for the unknowns  $A, B, c_1$ . Equation (a) minus Equation (c) gives  $101A = 303$ ,  $A = 3$ . Then  $c_1 = 1$  from (a) and  $B = 1$  from (b). The solution is (Fig. 72)

$$y = e^x + 3 \cos 10x + \sin 10x.$$

This gives the solution curve, which oscillates about  $e^x$  (dashed in Fig. 72 on p. 114). ■

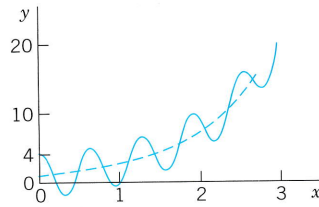


Fig. 72. Solution in Example 2

## Multiple Real Roots

If a real double root occurs, say,  $\lambda_1 = \lambda_2$ , then  $y_1 = y_2$  in (3), and we take  $y_1$  and  $xy_1$  as corresponding linearly independent solutions. This is as in Sec. 2.2.

More generally, if  $\lambda$  is a real root of order  $m$ , then  $m$  corresponding linearly independent solutions are

$$(7) \quad e^{\lambda x}, \quad xe^{\lambda x}, \quad x^2e^{\lambda x}, \quad \dots, \quad x^{m-1}e^{\lambda x}.$$

We derive these solutions after the next example and indicate how to prove their linear independence.

### EXAMPLE 3 Real Double and Triple Roots

Solve the ODE  $y^{(5)} - 3y^{(4)} + 3y''' - y'' = 0$ .

**Solution.** The characteristic equation  $\lambda^5 - 3\lambda^4 + 3\lambda^3 - \lambda^2 = 0$  has the roots  $\lambda_1 = \lambda_2 = 0$  and  $\lambda_3 = \lambda_4 = \lambda_5 = 1$ , and the answer is

$$(8) \quad y = c_1 + c_2x + (c_3 + c_4x + c_5x^2)e^x. \quad \blacksquare$$

**Derivation of (7).** We write the left side of (1) as

$$L[y] = y^{(n)} + a_{n-1}y^{(n-1)} + \dots + a_0y.$$

Let  $y = e^{\lambda x}$ . Then by performing the differentiations we have

$$L[e^{\lambda x}] = (\lambda^n + a_{n-1}\lambda^{n-1} + \dots + a_0)e^{\lambda x}.$$

Now let  $\lambda_1$  be a root of  $m$ th order of the polynomial on the right, where  $m \leq n$ . For  $m < n$  let  $\lambda_{m+1}, \dots, \lambda_n$  be the other roots, all different from  $\lambda_1$ . Writing the polynomial in product form, we then have

$$L[e^{\lambda x}] = (\lambda - \lambda_1)^m h(\lambda) e^{\lambda x}$$

with  $h(\lambda) = 1$  if  $m = n$ , and  $h(\lambda) = (\lambda - \lambda_{m+1}) \cdots (\lambda - \lambda_n)$  if  $m < n$ . Now comes the key idea: We differentiate on both sides with respect to  $\lambda$ ,

$$(9) \quad \frac{\partial}{\partial \lambda} L[e^{\lambda x}] = m(\lambda - \lambda_1)^{m-1} h(\lambda) e^{\lambda x} + (\lambda - \lambda_1)^m \frac{\partial}{\partial \lambda} [h(\lambda) e^{\lambda x}].$$

The differentiations with respect to  $x$  and  $\lambda$  are independent and the occurring derivatives are continuous, so that we can interchange their order on the left:

$$(10) \quad \frac{\partial}{\partial \lambda} L[e^{\lambda x}] = L\left[\frac{\partial}{\partial \lambda} e^{\lambda x}\right] = L[xe^{\lambda x}].$$

The right side of (9) is zero for  $\lambda = \lambda_1$  because of the factors  $\lambda - \lambda_1$  (and  $m \geq 2$  since we have a multiple root!). Hence  $L[xe^{\lambda_1 x}] = 0$  by (9) and (10). This proves that  $x e^{\lambda_1 x}$  is a solution of (1).

We can repeat this step and produce  $x^2 e^{\lambda_1 x}, \dots, x^{m-1} e^{\lambda_1 x}$  by another  $m - 2$  such differentiations with respect to  $\lambda$ . Going one step further would no longer give zero on the right because the lowest power of  $\lambda - \lambda_1$  would then be  $(\lambda - \lambda_1)^0$ , multiplied by  $m!h(\lambda)$  and  $h(\lambda_1) \neq 0$  because  $h(\lambda)$  has no factors  $\lambda - \lambda_1$ ; so we get *precisely* the solutions in (7).

We finally show that the solutions (7) are linearly independent. For a specific  $n$  this can be seen by calculating their Wronskian, which turns out to be nonzero. For arbitrary  $m$  we can pull out the exponential functions from the Wronskian. This gives  $(e^{\lambda x})^m = e^{\lambda m x}$  times a determinant which by "row operations" can be reduced to the Wronskian of  $1, x, \dots, x^{m-1}$ . The latter is constant and different from zero (equal to  $1!2! \cdots (m-1)!$ ). These functions are solutions of the ODE  $y^{(m)} = 0$ , so that linear independence follows from Theorem 3 in Sec. 3.1. ■

## Multiple Complex Roots

In this case, real solutions are obtained as for complex simple roots above. Consequently, if  $\lambda = \gamma + i\omega$  is a **complex double root**, so is the conjugate  $\bar{\lambda} = \gamma - i\omega$ . Corresponding linearly independent solutions are

$$(11) \quad e^{\gamma x} \cos \omega x, \quad e^{\gamma x} \sin \omega x, \quad x e^{\gamma x} \cos \omega x, \quad x e^{\gamma x} \sin \omega x.$$

The first two of these result from  $e^{\lambda x}$  and  $e^{\bar{\lambda} x}$  as before, and the second two from  $x e^{\lambda x}$  and  $x e^{\bar{\lambda} x}$  in the same fashion. Obviously, the corresponding general solution is

$$(12) \quad y = e^{\gamma x}[(A_1 + A_2 x) \cos \omega x + (B_1 + B_2 x) \sin \omega x].$$

For *complex triple roots* (which hardly ever occur in applications), one would obtain two more solutions  $x^2 e^{\lambda x} \cos \omega x, x^2 e^{\lambda x} \sin \omega x$ , and so on.

## PROBLEM SET 3.2

### 1-6 ODE FOR GIVEN BASIS

Find an ODE (1) for which the given functions form a basis of solutions.

1.  $e^x, e^{2x}, e^{3x}$
2.  $e^{-2x}, x e^{-2x}, x^2 e^{-2x}$
3.  $e^x, e^{-x}, \cos x, \sin x$
4.  $\cos x, \sin x, x \cos x, x \sin x$
5.  $1, x, \cos 2x, \sin 2x$
6.  $e^{-2x}, e^{-x}, e^x, e^{2x}, 1$

### 7-12 GENERAL SOLUTION

Solve the given ODE. (Show the details of your work.)

7.  $y''' + y' = 0$
8.  $y^{iv} - 29y'' + 100y = 0$
9.  $y''' + y'' - y' - y = 0$
10.  $16y^{iv} - 8y'' + y = 0$
11.  $y''' - 3y'' - 4y' + 6y = 0$
12.  $y^{iv} + 3y'' - 4y = 0$

**13–18 INITIAL VALUE PROBLEMS**

Solve by a CAS, giving a general solution and the particular solution and its graph.

13.  $y^{iv} + 0.45y''' - 0.165y'' + 0.0045y' - 0.00175y = 0$ ,  
 $y(0) = 17.4$ ,  $y'(0) = -2.82$ ,  $y''(0) = 2.0485$ ,  
 $y'''(0) = -1.458675$

14.  $4y''' + 8y'' + 41y' + 37y = 0$ ,  $y(0) = 9$ ,  
 $y'(0) = -6.5$ ,  $y''(0) = -39.75$

15.  $y''' + 3.2y'' + 4.81y' = 0$ ,  $y(0) = 3.4$ ,  
 $y'(0) = -4.6$ ,  $y''(0) = 9.91$

16.  $y^{iv} + 4y = 0$ ,  $y(0) = \frac{1}{2}$ ,  $y'(0) = -\frac{3}{2}$ ,  $y''(0) = \frac{5}{2}$ ,  
 $y'''(0) = -\frac{7}{2}$

17.  $y^{iv} - 9y'' - 400y = 0$ ,  $y(0) = 0$ ,  $y'(0) = 0$ ,  
 $y''(0) = 41$ ,  $y'''(0) = 0$

18.  $y''' + 7.5y'' + 14.25y' - 9.125y = 0$ ,  
 $y(0) = 10.05$ ,  $y'(0) = -54.975$ ,  
 $y''(0) = 257.5125$

19. **CAS PROJECT. Wronskians. Euler–Cauchy Equations of Higher Order.** Although Euler–Cauchy equations have *variable* coefficients (powers of  $x$ ), we include them here because they fit quite well into the present methods.

(a) Write a program for calculating Wronskians.

(b) Apply the program to some bases of third-order and fourth-order constant-coefficient ODEs. Compare

the results with those obtained by the program most likely available for Wronskians in your CAS.

(c) Extend the solution method in Sec. 2.5 to any order  $n$ . Solve  $x^3y''' + 2x^2y'' - 4xy' + 4y = 0$  and another ODE of your choice. In each case calculate the Wronskian.

20. **PROJECT. Reduction of Order.** This is of practical interest since a single solution of an ODE can often be guessed. For second order, see Example 7 in Sec. 2.1.

(a) How could you reduce the order of a linear constant-coefficient ODE if a solution is known?

(b) Extend the method to a variable-coefficient ODE

$$y''' + p_2(x)y'' + p_1(x)y' + p_0(x)y = 0.$$

Assuming a solution  $y_1$  to be known, show that another solution is  $y_2(x) = u(x)y_1(x)$  with  $u(x) = \int z(x) dx$  and  $z$  obtained by solving

$$y_1 z'' + (3y_1' + p_2 y_1) z' + (3y_1'' + 2p_2 y_1' + p_1 y_1) z = 0.$$

(c) Reduce

$$x^3 y''' - 3x^2 y'' + (6 - x^2) x y' - (6 - x^2) y = 0,$$

using  $y_1 = x$  (perhaps obtainable by inspection).

21. **CAS EXPERIMENT. Reduction of Order.** Starting with a basis, find third-order ODEs with variable coefficients for which the reduction to second order turns out to be relatively simple.

## 3.3 Nonhomogeneous Linear ODEs

We now turn from homogeneous to nonhomogeneous linear ODEs of  $n$ th order. We write them in standard form

$$(1) \quad y^{(n)} + p_{n-1}(x)y^{(n-1)} + \cdots + p_1(x)y' + p_0(x)y = r(x)$$

with  $y^{(n)} = d^n y/dx^n$  as the first term, which is practical, and  $r(x) \neq 0$ . As for second-order ODEs, a general solution of (1) on an open interval  $I$  of the  $x$ -axis is of the form

$$(2) \quad y(x) = y_h(x) + y_p(x).$$

Here  $y_h(x) = c_1 y_1(x) + \cdots + c_n y_n(x)$  is a general solution of the corresponding homogeneous ODE

$$(3) \quad y^{(n)} + p_{n-1}(x)y^{(n-1)} + \cdots + p_1(x)y' + p_0(x)y = 0$$

on  $I$ . Also,  $y_p$  is any solution of (1) on  $I$  containing no arbitrary constants. If (1) has continuous coefficients and a continuous  $r(x)$  on  $I$ , then a general solution of (1) exists and includes all solutions. Thus (1) has no singular solutions.

An **initial value problem** for (1) consists of (1) and  $n$  **initial conditions**

$$(4) \quad y(x_0) = K_0, \quad y'(x_0) = K_1, \quad \dots, \quad y^{(n-1)}(x_0) = K_{n-1}$$

with  $x_0$  in  $I$ . Under those continuity assumptions it has a unique solution. The ideas of proof are the same as those for  $n = 2$  in Sec. 2.7.

## Method of Undetermined Coefficients

Equation (2) shows that for solving (1) we have to determine a particular solution of (1). For a constant-coefficient equation

$$(5) \quad y^{(n)} + a_{n-1}y^{(n-1)} + \dots + a_1y' + a_0y = r(x)$$

( $a_0, \dots, a_{n-1}$  constant) and special  $r(x)$  as in Sec. 2.7, such a  $y_p(x)$  can be determined by the **method of undetermined coefficients**, as in Sec. 2.7, using the following rules.

(A) **Basic Rule** as in Sec. 2.7.

(B) **Modification Rule.** *If a term in your choice for  $y_p(x)$  is a solution of the homogeneous equation (3), then multiply  $y_p(x)$  by  $x^k$ , where  $k$  is the smallest positive integer such that no term of  $x^k y_p(x)$  is a solution of (3).*

(C) **Sum Rule** as in Sec. 2.7.

The practical application of the method is the same as that in Sec. 2.7. It suffices to illustrate the typical steps of solving an initial value problem and, in particular, the new Modification Rule, which includes the old Modification Rule as a particular case (with  $k = 1$  or  $2$ ). We shall see that the technicalities are the same as for  $n = 2$ , perhaps except for the more involved determination of the constants.

### EXAMPLE 1 Initial Value Problem. Modification Rule

Solve the initial value problem

$$(6) \quad y''' + 3y'' + 3y' + y = 30e^{-x}, \quad y(0) = 3, \quad y'(0) = -3, \quad y''(0) = -47.$$

**Solution.** *Step 1.* The characteristic equation is  $\lambda^3 + 3\lambda^2 + 3\lambda + 1 = (\lambda + 1)^3 = 0$ . It has the triple root  $\lambda = -1$ . Hence a general solution of the homogeneous ODE is

$$\begin{aligned} y_h &= c_1 e^{-x} + c_2 x e^{-x} + c_3 x^2 e^{-x} \\ &= (c_1 + c_2 x + c_3 x^2) e^{-x}. \end{aligned}$$

*Step 2.* If we try  $y_p = C e^{-x}$ , we get  $-C + 3C - 3C + C = 30$ , which has no solution. Try  $Cx e^{-x}$  and  $Cx^2 e^{-x}$ . The Modification Rule calls for

$$y_p = Cx^3 e^{-x}.$$

Then

$$y_p' = C(3x^2 - x^3) e^{-x},$$

$$y_p'' = C(6x - 6x^2 + x^3) e^{-x},$$

$$y_p''' = C(6 - 18x + 9x^2 - x^3) e^{-x}.$$

Substitution of these expressions into (6) and omission of the common factor  $e^{-x}$  gives

$$C(6 - 18x + 9x^2 - x^3) + 3C(6x - 6x^2 + x^3) + 3C(3x^2 - x^3) + Cx^3 = 30.$$

The linear, quadratic, and cubic terms drop out, and  $6C = 30$ . Hence  $C = 5$ . This gives  $y_p = 5x^3e^{-x}$ .

**Step 3.** We now write down  $y = y_h + y_p$ , the general solution of the given ODE. From it we find  $c_1$  by the first initial condition. We insert the value, differentiate, and determine  $c_2$  from the second initial condition, insert the value, and finally determine  $c_3$  from  $y''(0)$  and the third initial condition:

$$\begin{aligned} y = y_h + y_p &= (c_1 + c_2x + c_3x^2)e^{-x} + 5x^3e^{-x}, & y(0) &= c_1 = 3 \\ y' &= [-3 + c_2 + (-c_2 + 2c_3)x + (15 - c_3)x^2 - 5x^3]e^{-x}, & y'(0) &= -3 + c_2 = -3, & c_2 &= 0 \\ y'' &= [3 + 2c_3 + (30 - 4c_3)x + (-30 + c_3)x^2 + 5x^3]e^{-x}, & y''(0) &= 3 + 2c_3 = -47, & c_3 &= -25. \end{aligned}$$

Hence the *answer* to our problem is (Fig. 73)

$$y = (3 - 25x^2)e^{-x} + 5x^3e^{-x}.$$

The curve of  $y$  begins at  $(0, 3)$  with a negative slope, as expected from the initial values, and approaches zero as  $x \rightarrow \infty$ . The dashed curve in Fig. 73 is  $y_p$ . ■

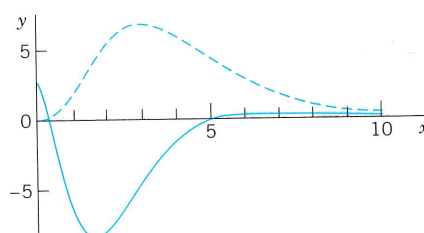


Fig. 73.  $y$  and  $y_p$  (dashed) in Example 1

## Method of Variation of Parameters

The method of variation of parameters (see Sec. 2.10) also extends to arbitrary order  $n$ . It gives a particular solution  $y_p$  for the nonhomogeneous equation (1) (in standard form with  $y^{(n)}$  as the first term!) by the formula

$$\begin{aligned} (7) \quad y_p(x) &= \sum_{k=1}^n y_k(x) \int \frac{W_k(x)}{W(x)} r(x) dx \\ &= y_1(x) \int \frac{W_1(x)}{W(x)} r(x) dx + \cdots + y_n(x) \int \frac{W_n(x)}{W(x)} r(x) dx \end{aligned}$$

on an open interval  $I$  on which the coefficients of (1) and  $r(x)$  are continuous. In (7) the functions  $y_1, \dots, y_n$  form a basis of the homogeneous ODE (3), with Wronskian  $W$ , and  $W_j$  ( $j = 1, \dots, n$ ) is obtained from  $W$  by replacing the  $j$ th column of  $W$  by the column  $[0 \ 0 \ \cdots \ 0 \ 1]^T$ . Thus, when  $n = 2$ , this becomes identical with (2) in Sec. 2.10,

$$W = \begin{vmatrix} y_1 & y_2 \\ y_1' & y_2' \end{vmatrix}, \quad W_1 = \begin{vmatrix} 0 & y_2 \\ 1 & y_2' \end{vmatrix} = -y_2, \quad W_2 = \begin{vmatrix} y_1 & 0 \\ y_1' & 1 \end{vmatrix} = y_1.$$

The proof of (7) uses an extension of the idea of the proof of (2) in Sec. 2.10 and can be found in Ref [A11] listed in App. 1.

**EXAMPLE 2** Variation of Parameters. Nonhomogeneous Euler–Cauchy Equation

Solve the nonhomogeneous Euler–Cauchy equation

$$x^3 y''' - 3x^2 y'' + 6xy' - 6y = x^4 \ln x \quad (x > 0).$$

**Solution.** *Step 1. General solution of the homogeneous ODE.* Substitution of  $y = x^m$  and the derivatives into the homogeneous ODE and deletion of the factor  $x^m$  gives

$$m(m-1)(m-2) - 3m(m-1) + 6m - 6 = 0.$$

The roots are 1, 2, 3 and give as a basis

$$y_1 = x, \quad y_2 = x^2, \quad y_3 = x^3.$$

Hence the corresponding general solution of the homogeneous ODE is

$$y_h = c_1 x + c_2 x^2 + c_3 x^3.$$

*Step 2. Determinants needed in (7).* These are

$$W = \begin{vmatrix} x & x^2 & x^3 \\ 1 & 2x & 3x^2 \\ 0 & 2 & 6x \end{vmatrix} = 2x^3$$

$$W_1 = \begin{vmatrix} 0 & x^2 & x^3 \\ 0 & 2x & 3x^2 \\ 1 & 2 & 6x \end{vmatrix} = x^4$$

$$W_2 = \begin{vmatrix} x & 0 & x^3 \\ 1 & 0 & 3x^2 \\ 0 & 1 & 6x \end{vmatrix} = -2x^3$$

$$W_3 = \begin{vmatrix} x & x^2 & 0 \\ 1 & 2x & 0 \\ 0 & 2 & 1 \end{vmatrix} = x^2.$$

*Step 3. Integration.* In (7) we also need the right side  $r(x)$  of our ODE in standard form, obtained by division of the given equation by the coefficient  $x^3$  of  $y'''$ ; thus,  $r(x) = (x^4 \ln x)/x^3 = x \ln x$ . In (7) we have the simple quotients  $W_1/W = x/2$ ,  $W_2/W = -1$ ,  $W_3/W = 1/(2x)$ . Hence (7) becomes

$$\begin{aligned} y_p &= x \int \frac{x}{2} x \ln x \, dx - x^2 \int x \ln x \, dx + x^3 \int \frac{1}{2x} x \ln x \, dx \\ &= \frac{x}{2} \left( \frac{x^3}{3} \ln x - \frac{x^3}{9} \right) - x^2 \left( \frac{x^2}{2} \ln x - \frac{x^2}{4} \right) + \frac{x^3}{2} (x \ln x - x). \end{aligned}$$

Simplification gives  $y_p = \frac{1}{6}x^4 (\ln x - \frac{11}{6})$ . Hence the answer is

$$y = y_h + y_p = c_1 x + c_2 x^2 + c_3 x^3 + \frac{1}{6}x^4 (\ln x - \frac{11}{6}).$$

Figure 74 shows  $y_p$ . Can you explain the shape of this curve? Its behavior near  $x = 0$ ? The occurrence of a minimum? Its rapid increase? Why would the method of undetermined coefficients not have given the solution? ■



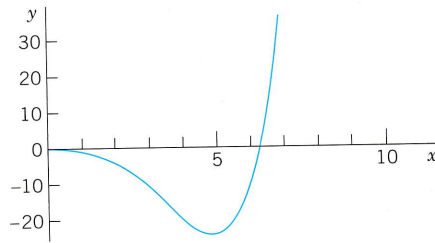


Fig. 74. Particular solution  $y_p$  of the nonhomogeneous Euler–Cauchy equation in Example 2

## Application: Elastic Beams

Whereas second-order ODEs have various applications, some of the more important ones we have seen, higher order ODEs occur much more rarely in engineering work. An important fourth-order ODE governs the bending of elastic beams, such as wooden or iron girders in a building or a bridge.

Vibrations of beams will be considered in Sec. 12.3.

### EXAMPLE 3 Bending of an Elastic Beam under a Load

We consider a beam  $B$  of length  $L$  and constant (e.g., **rectangular**) cross section and homogeneous elastic material (e.g., steel); see Fig. 75. We assume that under its own weight the beam is bent so little that it is practically straight. If we apply a load to  $B$  in a vertical plane through the axis of symmetry (the  $x$ -axis in Fig. 75),  $B$  is bent. Its axis is curved into the so-called **elastic curve**  $C$  (or **deflection curve**). It is shown in elasticity theory that the bending moment  $M(x)$  is proportional to the curvature  $k(x)$  of  $C$ . We assume the bending to be small, so that the deflection  $y(x)$  and its derivative  $y'(x)$  (determining the tangent direction of  $C$ ) are small. Then, by calculus,  $k = y''/(1 + y'^2)^{3/2} \approx y''$ . Hence

$$M(x) = EIy''(x).$$

$EI$  is the constant of proportionality.  $E$  is *Young's modulus of elasticity* of the material of the beam.  $I$  is the moment of inertia of the cross section about the (horizontal)  $z$ -axis in Fig. 75.

Elasticity theory shows further that  $M''(x) = f(x)$ , where  $f(x)$  is the load per unit length. Together,

$$(8) \quad EIy^{(4)} = f(x).$$

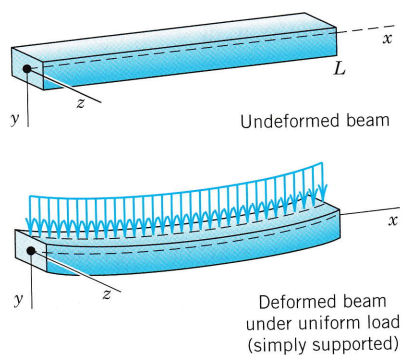


Fig. 75. Elastic Beam

The practically most important supports and corresponding boundary conditions are as follows (see Fig. 76).

- (A) Simply supported  $y = y'' = 0$  at  $x = 0$  and  $L$
- (B) Clamped at both ends  $y = y' = 0$  at  $x = 0$  and  $L$
- (C) Clamped at  $x = 0$ , free at  $x = L$   $y(0) = y'(0) = 0, y''(L) = y'''(L) = 0$ .

The boundary condition  $y = 0$  means no displacement at that point,  $y' = 0$  means a horizontal tangent,  $y'' = 0$  means no bending moment, and  $y''' = 0$  means no shear force.

Let us apply this to the uniformly loaded simply supported beam in Fig. 75. The load is  $f(x) \equiv f_0 = \text{const}$ . Then (8) is

$$(9) \quad y^{iv} = k, \quad k = \frac{f_0}{EI}.$$

This can be solved simply by calculus. Two integrations give

$$y'' = \frac{k}{2} x^2 + c_1x + c_2.$$

$y''(0) = 0$  gives  $c_2 = 0$ . Then  $y''(L) = L(\frac{1}{2}kL + c_1) = 0, c_1 = -kL/2$  (since  $L \neq 0$ ). Hence

$$y'' = \frac{k}{2} (x^2 - Lx).$$

Integrating this twice, we obtain

$$y = \frac{k}{2} \left( \frac{1}{12} x^4 - \frac{L}{6} x^3 + c_3x + c_4 \right)$$

with  $c_4 = 0$  from  $y(0) = 0$ . Then

$$y(L) = \frac{kL}{2} \left( \frac{L^3}{12} - \frac{L^3}{6} + c_3 \right) = 0, \quad c_3 = \frac{L^3}{12}.$$

Inserting the expression for  $k$ , we obtain as our solution

$$y = \frac{f_0}{24EI} (x^4 - 2Lx^3 + L^3x).$$

Since the boundary conditions at both ends are the same, we expect the deflection  $y(x)$  to be "symmetric" with respect to  $L/2$ , that is,  $y(x) = y(L - x)$ . Verify this directly or set  $x = u + L/2$  and show that  $y$  becomes an even function of  $u$ .

$$y = \frac{f_0}{24EI} \left( u^2 - \frac{1}{4} L^2 \right) \left( u^2 - \frac{5}{4} L^2 \right).$$

From this we can see that the maximum deflection in the middle at  $u = 0$  ( $x = L/2$ ) is  $5f_0L^4/(16 \cdot 24EI)$ . Recall that the positive direction points downward. ■

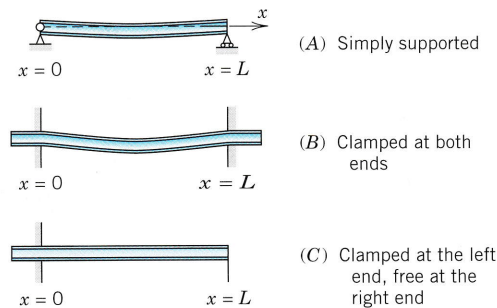


Fig. 76. Supports of a Beam

### PROBLEM SET 3.3

#### 1–8 GENERAL SOLUTION

Solve the following ODEs. (Show the details of your work.)

- $y''' - 2y'' - 4y' + 8y = e^{-3x} + 8x^2$
- $y''' + 3y'' - 5y' - 39y = 30 \cos x$
- $y^{iv} + 0.5y'' + 0.0625y = e^{-x} \cos 0.5x$
- $y''' + 2y'' - 5y' - 6y = 100e^{-3x} + 18e^{-x}$
- $x^3y''' + 0.75xy' - 0.75y = 9x^{5.5}$
- $(xD^3 + 4D^2)y = 8e^x$
- $(D^4 + 10D^2 + 9I)y = 13 \cosh 2x$
- $(D^3 - 2D^2 - 9D + 18I)y = e^{2x}$

#### 9–14 INITIAL VALUE PROBLEMS

Solve the following initial value problems. (Show the details.)

- $y''' - 9y'' + 27y' - 27y = 54 \sin 3x, \quad y(0) = 3.5, \quad y'(0) = 13.5, \quad y''(0) = 38.5$
- $y^{iv} - 16y = 128 \cosh 2x, \quad y(0) = 1, \quad y'(0) = 24, \quad y''(0) = 20, \quad y'''(0) = -160$
- $(x^3D^3 - x^2D^2 - 7xD + 16I)y = 9x \ln x, \quad y(1) = 6, \quad Dy(1) = 18, \quad D^2y(1) = 65$
- $(D^4 - 26D^2 + 25I)y = 50(x+1)^2, \quad y(0) = 12.16, \quad Dy(0) = -6, \quad D^2y(0) = 34, \quad D^3y(0) = -130$

$$13. (D^3 + 4D^2 + 85D)y = 135xe^x, \quad y(0) = 10.4, \quad Dy(0) = -18.1, \quad D^2y(0) = -691.6$$

$$14. (2D^3 - D^2 - 8D + 4I)y = \sin x, \quad y(0) = 1, \quad Dy(0) = 0, \quad D^2y(0) = 0$$

#### 15. WRITING PROJECT. Comparison of Methods.

Write a report on the method of undetermined coefficients and the method of variation of parameters, discussing and comparing the advantages and disadvantages of each method. Illustrate your findings with typical examples. Try to show that the method of undetermined coefficients, say, for a third-order ODE with constant coefficients and an exponential function on the right, can be derived from the method of variation of parameters.

#### 16. CAS EXPERIMENT. Undetermined Coefficients.

Since variation of parameters is generally complicated, it seems worthwhile to try to extend the other method. Find out experimentally for what ODEs this is possible and for what not. *Hint:* Work backward, solving ODEs with a CAS and then looking whether the solution could be obtained by undetermined coefficients. For example, consider

$$y''' - 12y'' + 48y' - 64y = x^{1/2}e^{4x} \quad \text{and} \\ x^3y''' + x^2y'' - 6xy' + 6y = x \ln x.$$

## CHAPTER 3 REVIEW QUESTIONS AND PROBLEMS

- What is the superposition or linearity principle? For what  $n$ th-order ODEs does it hold?
- List some other basic theorems that extend from second-order to  $n$ th-order ODEs.
- If you know a general solution of a homogeneous linear ODE, what do you need to obtain from it a general solution of a corresponding nonhomogeneous linear ODE?
- What is an initial value problem for an  $n$ th-order linear ODE?
- What is the Wronskian? What is it used for?
- $(xD^4 + D^3)y = 150x^4$
- $(D^4 - 2D^3 - 8D^2)y = 16 \cos 2x$
- $(D^3 + I)y = 9e^{x/2}$
- $(x^3D^3 - 3x^2D^2 + 6xD - 6I)y = 30x^{-2}$
- $(D^3 - D^2 - D + I)y = e^x$

#### 16–20 INITIAL VALUE PROBLEMS

Solve the given problem. (Show the details.)

#### 6–15 GENERAL SOLUTION

Solve the given ODE. (Show the details of your work.)

- $y''' + 6y'' + 18y' + 40y = 0$
- $4x^2y''' + 12xy'' + 3y' = 0$
- $y^{iv} + 10y'' + 9y = 0$
- $8y''' + 12y'' - 2y' - 3y = 0$
- $(D^3 + 3D^2 + 3D + I)y = x^2$
- $y''' - 2y'' + 4y' - 8y = 0, \quad y(0) = -1, \quad y'(0) = 30, \quad y''(0) = 28$
- $x^3y''' + 7x^2y'' - 2xy' - 10y = 0, \quad y(1) = 1, \quad y'(1) = -7, \quad y''(1) = 44$
- $(D^3 + 25D)y = 32 \cos^2 4x, \quad y(0) = 0, \quad Dy(0) = 0, \quad D^2y(0) = 0$
- $(D^4 + 40D^2 - 441I)y = 8 \cosh x, \quad y(0) = 1.98, \quad Dy(0) = 3, \quad D^2y(0) = -40.02, \quad D^3y(0) = 27$
- $(x^3D^3 + 5x^2D^2 + 2xD - 2I)y = 7x^{3/2}, \quad y(1) = 10.6, \quad Dy(1) = -3.6, \quad D^2y(1) = 31.2$

## SUMMARY OF CHAPTER 3

### Higher Order Linear ODEs

*Compare with the similar Summary of Chap. 2 (the case  $n = 2$ ).*

Chapter 3 extends Chap. 2 from order  $n = 2$  to arbitrary order  $n$ . An  **$n$ th-order linear ODE** is an ODE that can be written

$$(1) \quad y^{(n)} + p_{n-1}(x)y^{(n-1)} + \cdots + p_1(x)y' + p_0(x)y = r(x)$$

with  $y^{(n)} = d^n y/dx^n$  as the first term; we again call this the **standard form**. Equation (1) is called **homogeneous** if  $r(x) \equiv 0$  on a given open interval  $I$  considered, **nonhomogeneous** if  $r(x) \not\equiv 0$  on  $I$ . For the homogeneous ODE

$$(2) \quad y^{(n)} + p_{n-1}(x)y^{(n-1)} + \cdots + p_1(x)y' + p_0(x)y = 0$$

the **superposition principle** (Sec. 3.1) holds, just as in the case  $n = 2$ . A **basis** or **fundamental system** of solutions of (2) on  $I$  consists of  $n$  linearly independent solutions  $y_1, \cdots, y_n$  of (2) on  $I$ . A **general solution** of (2) on  $I$  is a linear combination of these,

$$(3) \quad y = c_1 y_1 + \cdots + c_n y_n \quad (c_1, \cdots, c_n \text{ arbitrary constants}).$$

A **general solution** of the nonhomogeneous ODE (1) on  $I$  is of the form

$$(4) \quad y = y_h + y_p \quad (\text{Sec. 3.3}).$$

Here,  $y_p$  is a particular solution of (1) and is obtained by two methods (**undetermined coefficients** or **variation of parameters**) explained in Sec. 3.3.

An **initial value problem** for (1) or (2) consists of one of these ODEs and  $n$  initial conditions (Secs. 3.1, 3.3)

$$(5) \quad y(x_0) = K_0, \quad y'(x_0) = K_1, \quad \cdots, \quad y^{(n-1)}(x_0) = K_{n-1}$$

with given  $x_0$  in  $I$  and given  $K_0, \cdots, K_{n-1}$ . If  $p_0, \cdots, p_{n-1}, r$  are continuous on  $I$ , then general solutions of (1) and (2) on  $I$  exist, and initial value problems (1), (5) or (2), (5) have a unique solution.

## Systems of ODEs. Phase Plane. Qualitative Methods

Systems of ODEs have various applications (see, for instance, Secs. 4.1 and 4.5). Their theory is outlined in Sec. 4.2 and includes that of a single ODE. The practically important conversion of a single  $n$ th-order ODE to a system is shown in Sec. 4.1.

**Linear systems** (Secs. 4.3, 4.4, 4.6) are best treated by the use of vectors and matrices, of which, however, only a few elementary facts will be needed here, as given in Sec. 4.0 and probably familiar to most students.

**Qualitative methods.** In addition to actually solving systems (Sec. 4.3, 4.6), which is often difficult or even impossible, we shall explain a totally different method, namely, the powerful method of investigating the general behavior of whole families of solutions in the **phase plane** (Sec. 4.3). This approach to systems of ODEs is called a **qualitative method** because it does not need actual solutions (in contrast to a “quantitative method” of actually solving a system).

This *phase plane method*, as it is called, also gives information on **stability** of solutions, which is of general importance in control theory, circuit theory, population dynamics, and so on. Here, *stability of a physical system* means that, roughly speaking, a small change at some instant causes only small changes in the behavior of the system at all later times.

Phase plane methods can be extended to nonlinear systems, for which they are particularly useful. We will show this in Sec. 4.5, which includes a discussion of the pendulum equation and the Lotka-Volterra population model. We finally discuss nonhomogeneous linear systems in Sec. 4.6.

**NOTATION.** Analogous to Chaps. 1–3, we continue to denote unknown functions by  $y$ ; thus,  $y_1(t)$ ,  $y_2(t)$ . This seems preferable to suddenly using  $x$  for functions,  $x_1(t)$ ,  $x_2(t)$ , as is sometimes done in systems of ODEs.

*Prerequisite:* Chap. 2.

*References and Answers to Problems:* App. 1 Part A, and App. 2.

### 4.0 Basics of Matrices and Vectors

In discussing *linear* systems of ODEs we shall use matrices and vectors. This simplifies formulas and clarifies ideas. But we shall need only a few elementary facts (by no means the bulk of material in Chaps. 7 and 8). These facts will very likely be at the disposal of most students. Hence *this section is for reference only. Begin with Sec. 4.1 and consult 4.0 as needed.*



**Vectors.** A column vector  $\mathbf{x}$  with  $n$  components  $x_1, \dots, x_n$  is of the form

$$\mathbf{x} = \begin{bmatrix} x_1 \\ x_2 \\ \vdots \\ x_n \end{bmatrix}, \quad \text{thus if } n = 2, \quad \mathbf{x} = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}.$$

Similarly, a row vector  $\mathbf{v}$  is of the form

$$\mathbf{v} = [v_1 \ \cdots \ v_n], \quad \text{thus if } n = 2, \text{ then} \quad \mathbf{v} = [v_1, \ v_2].$$

## Calculations with Matrices and Vectors

**Equality.** Two  $n \times n$  matrices are *equal* if and only if corresponding entries are equal. Thus for  $n = 2$ , let

$$\mathbf{A} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \quad \text{and} \quad \mathbf{B} = \begin{bmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{bmatrix}.$$

Then  $\mathbf{A} = \mathbf{B}$  if and only if

$$\begin{aligned} a_{11} &= b_{11}, & a_{12} &= b_{12} \\ a_{21} &= b_{21}, & a_{22} &= b_{22}. \end{aligned}$$

Two column vectors (or two row vectors) are *equal* if and only if they both have  $n$  components and corresponding components are equal. Thus, let

$$\mathbf{v} = \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} \quad \text{and} \quad \mathbf{x} = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}. \quad \text{Then} \quad \mathbf{v} = \mathbf{x} \quad \text{if and only if} \quad \begin{aligned} v_1 &= x_1 \\ v_2 &= x_2. \end{aligned}$$

**Addition** is performed by adding corresponding entries (or components); here, matrices must both be  $n \times n$ , and vectors must both have the same number of components. Thus for  $n = 2$ ,

$$(5) \quad \mathbf{A} + \mathbf{B} = \begin{bmatrix} a_{11} + b_{11} & a_{12} + b_{12} \\ a_{21} + b_{21} & a_{22} + b_{22} \end{bmatrix}, \quad \mathbf{v} + \mathbf{x} = \begin{bmatrix} v_1 + x_1 \\ v_2 + x_2 \end{bmatrix}.$$

**Scalar multiplication** (multiplication by a number  $c$ ) is performed by multiplying each entry (or component) by  $c$ . For example, if

$$\mathbf{A} = \begin{bmatrix} 9 & 3 \\ -2 & 0 \end{bmatrix}, \quad \text{then} \quad -7\mathbf{A} = \begin{bmatrix} -63 & -21 \\ 14 & 0 \end{bmatrix}.$$

If

$$\mathbf{v} = \begin{bmatrix} 0.4 \\ -13 \end{bmatrix}, \quad \text{then} \quad 10\mathbf{v} = \begin{bmatrix} 4 \\ -130 \end{bmatrix}.$$

**Matrix Multiplication.** The product  $\mathbf{C} = \mathbf{AB}$  (in this order) of two  $n \times n$  matrices  $\mathbf{A} = [a_{jk}]$  and  $\mathbf{B} = [b_{jk}]$  is the  $n \times n$  matrix  $\mathbf{C} = [c_{jk}]$  with entries

$$(6) \quad c_{jk} = \sum_{m=1}^n a_{jm}b_{mk} \quad \begin{array}{l} j = 1, \dots, n \\ k = 1, \dots, n, \end{array}$$

that is, multiply each entry in the  $j$ th row of  $\mathbf{A}$  by the corresponding entry in the  $k$ th column of  $\mathbf{B}$  and then add these  $n$  products. One says briefly that this is a “multiplication of rows into columns.” For example,

$$\begin{bmatrix} 9 & 3 \\ -2 & 0 \end{bmatrix} \begin{bmatrix} 1 & -4 \\ 2 & 5 \end{bmatrix} = \begin{bmatrix} 9 \cdot 1 + 3 \cdot 2 & 9 \cdot (-4) + 3 \cdot 5 \\ -2 \cdot 1 + 0 \cdot 2 & (-2) \cdot (-4) + 0 \cdot 5 \end{bmatrix} \\ = \begin{bmatrix} 15 & -21 \\ -2 & 8 \end{bmatrix}.$$

**CAUTION!** Matrix multiplication is *not commutative*,  $\mathbf{AB} \neq \mathbf{BA}$  in general. In our example,

$$\begin{bmatrix} 1 & -4 \\ 2 & 5 \end{bmatrix} \begin{bmatrix} 9 & 3 \\ -2 & 0 \end{bmatrix} = \begin{bmatrix} 1 \cdot 9 + (-4) \cdot (-2) & 1 \cdot 3 + (-4) \cdot 0 \\ 2 \cdot 9 + 5 \cdot (-2) & 2 \cdot 3 + 5 \cdot 0 \end{bmatrix} \\ = \begin{bmatrix} 17 & 3 \\ 8 & 6 \end{bmatrix}.$$

Multiplication of an  $n \times n$  matrix  $\mathbf{A}$  by a vector  $\mathbf{x}$  with  $n$  components is defined by the same rule:  $\mathbf{v} = \mathbf{Ax}$  is the vector with the  $n$  components

$$v_j = \sum_{m=1}^n a_{jm}x_m \quad j = 1, \dots, n.$$

For example,

$$\begin{bmatrix} 12 & 7 \\ -8 & 3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 12x_1 + 7x_2 \\ -8x_1 + 3x_2 \end{bmatrix}.$$

## Systems of ODEs as Vector Equations

**Differentiation.** The *derivative* of a matrix (or vector) with variable entries (or components) is obtained by differentiating each entry (or component). Thus, if

$$\mathbf{y}(t) = \begin{bmatrix} y_1(t) \\ y_2(t) \end{bmatrix} = \begin{bmatrix} e^{-2t} \\ \sin t \end{bmatrix}, \quad \text{then} \quad \mathbf{y}'(t) = \begin{bmatrix} y_1'(t) \\ y_2'(t) \end{bmatrix} = \begin{bmatrix} -2e^{-2t} \\ \cos t \end{bmatrix}.$$

Using matrix multiplication and differentiation, we can now write (1) as

$$(7) \quad \mathbf{y}' = \begin{bmatrix} y_1' \\ y_2' \end{bmatrix} = \mathbf{Ay} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \end{bmatrix}, \quad \text{e.g.,} \quad \mathbf{y}' = \begin{bmatrix} -5 & 2 \\ 13 & \frac{1}{2} \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \end{bmatrix}.$$



Similarly for (2) by means of an  $n \times n$  matrix  $\mathbf{A}$  and a column vector  $\mathbf{y}$  with  $n$  components, namely,  $\mathbf{y}' = \mathbf{A}\mathbf{y}$ . The vector equation (7) is equivalent to two equations for the components, and these are precisely the two ODEs in (1).

## Some Further Operations and Terms

**Transposition** is the operation of writing columns as rows and conversely and is indicated by  $T$ . Thus the transpose  $\mathbf{A}^T$  of the  $2 \times 2$  matrix

$$\mathbf{A} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} = \begin{bmatrix} -5 & 2 \\ 13 & \frac{1}{2} \end{bmatrix} \quad \text{is} \quad \mathbf{A}^T = \begin{bmatrix} a_{11} & a_{21} \\ a_{12} & a_{22} \end{bmatrix} = \begin{bmatrix} -5 & 13 \\ 2 & \frac{1}{2} \end{bmatrix}.$$

The transpose of a column vector, say,

$$\mathbf{v} = \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}, \quad \text{is a row vector,} \quad \mathbf{v}^T = [v_1 \quad v_2],$$

and conversely.

**Inverse of a Matrix.** The  $n \times n$  **unit matrix**  $\mathbf{I}$  is the  $n \times n$  matrix with main diagonal 1, 1,  $\dots$ , 1 and all other entries zero. If for a given  $n \times n$  matrix  $\mathbf{A}$  there is an  $n \times n$  matrix  $\mathbf{B}$  such that  $\mathbf{AB} = \mathbf{BA} = \mathbf{I}$ , then  $\mathbf{A}$  is called **nonsingular** and  $\mathbf{B}$  is called the **inverse** of  $\mathbf{A}$  and is denoted by  $\mathbf{A}^{-1}$ ; thus

$$(8) \quad \mathbf{AA}^{-1} = \mathbf{A}^{-1}\mathbf{A} = \mathbf{I}.$$

If  $\mathbf{A}$  has no inverse, it is called **singular**. For  $n = 2$ ,

$$(9) \quad \mathbf{A}^{-1} = \frac{1}{\det \mathbf{A}} \begin{bmatrix} a_{22} & -a_{12} \\ -a_{21} & a_{11} \end{bmatrix},$$

where the **determinant** of  $\mathbf{A}$  is

$$(10) \quad \det \mathbf{A} = \begin{vmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{vmatrix} = a_{11}a_{22} - a_{12}a_{21}.$$

(For general  $n$ , see Sec. 7.7, but this will not be needed in this chapter.)

**Linear Independence.**  $r$  given vectors  $\mathbf{v}^{(1)}, \dots, \mathbf{v}^{(r)}$  with  $n$  components are called a *linearly independent set* or, more briefly, **linearly independent**, if

$$(11) \quad c_1\mathbf{v}^{(1)} + \dots + c_r\mathbf{v}^{(r)} = \mathbf{0}$$

implies that all scalars  $c_1, \dots, c_r$  must be zero; here,  $\mathbf{0}$  denotes the **zero vector**, whose  $n$  components are all zero. If (11) also holds for scalars not all zero (so that at least one of these scalars is not zero), then these vectors are called a *linearly dependent set* or, briefly, **linearly dependent**, because then at least one of them can be expressed as

a **linear combination** of the others; that is, if, for instance,  $c_1 \neq 0$  in (11), then we can obtain

$$\mathbf{v}^{(1)} = -\frac{1}{c_1} (c_2 \mathbf{v}^{(2)} + \cdots + c_r \mathbf{v}^{(r)}).$$

## Eigenvalues, Eigenvectors

Eigenvalues and eigenvectors will be very important in this chapter (and, as a matter of fact, throughout mathematics).

Let  $\mathbf{A} = [a_{jk}]$  be an  $n \times n$  matrix. Consider the equation

$$(12) \quad \mathbf{Ax} = \lambda \mathbf{x}$$

where  $\lambda$  is a scalar (a real or complex number) to be determined and  $\mathbf{x}$  is a vector to be determined. Now for every  $\lambda$  a solution is  $\mathbf{x} = \mathbf{0}$ . A scalar  $\lambda$  such that (12) holds for some vector  $\mathbf{x} \neq \mathbf{0}$  is called an **eigenvalue** of  $\mathbf{A}$ , and this vector is called an **eigenvector** of  $\mathbf{A}$  corresponding to this eigenvalue  $\lambda$ .

We can write (12) as  $\mathbf{Ax} - \lambda \mathbf{x} = \mathbf{0}$  or

$$(13) \quad (\mathbf{A} - \lambda \mathbf{I})\mathbf{x} = \mathbf{0}.$$

These are  $n$  linear algebraic equations in the  $n$  unknowns  $x_1, \dots, x_n$  (the components of  $\mathbf{x}$ ). For these equations to have a solution  $\mathbf{x} \neq \mathbf{0}$ , the determinant of the coefficient matrix  $\mathbf{A} - \lambda \mathbf{I}$  must be zero. This is proved as a basic fact in linear algebra (Theorem 4 in Sec. 7.7). In this chapter we need this only for  $n = 2$ . Then (13) is

$$(14) \quad \begin{bmatrix} a_{11} - \lambda & a_{12} \\ a_{21} & a_{22} - \lambda \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix};$$

in components,

$$(14^*) \quad \begin{aligned} (a_{11} - \lambda)x_1 + a_{12}x_2 &= 0 \\ a_{21}x_1 + (a_{22} - \lambda)x_2 &= 0. \end{aligned}$$

Now  $\mathbf{A} - \lambda \mathbf{I}$  is singular if and only if its determinant  $\det(\mathbf{A} - \lambda \mathbf{I})$ , called the **characteristic determinant** of  $\mathbf{A}$  (also for general  $n$ ), is zero. This gives

$$(15) \quad \begin{aligned} \det(\mathbf{A} - \lambda \mathbf{I}) &= \begin{vmatrix} a_{11} - \lambda & a_{12} \\ a_{21} & a_{22} - \lambda \end{vmatrix} \\ &= (a_{11} - \lambda)(a_{22} - \lambda) - a_{12}a_{21} \\ &= \lambda^2 - (a_{11} + a_{22})\lambda + a_{11}a_{22} - a_{12}a_{21} = 0. \end{aligned}$$

This quadratic equation in  $\lambda$  is called the **characteristic equation** of  $\mathbf{A}$ . Its solutions are the eigenvalues  $\lambda_1$  and  $\lambda_2$  of  $\mathbf{A}$ . First determine these. Then use (14\*) with  $\lambda = \lambda_1$  to determine an eigenvector  $\mathbf{x}^{(1)}$  of  $\mathbf{A}$  corresponding to  $\lambda_1$ . Finally use (14\*) with  $\lambda = \lambda_2$  to find an eigenvector  $\mathbf{x}^{(2)}$  of  $\mathbf{A}$  corresponding to  $\lambda_2$ . Note that if  $\mathbf{x}$  is an eigenvector of  $\mathbf{A}$ , so is  $k\mathbf{x}$  for any  $k \neq 0$ .

**EXAMPLE 1 Eigenvalue Problem**

Find the eigenvalues and eigenvectors of the matrix

$$(16) \quad \mathbf{A} = \begin{bmatrix} -4.0 & 4.0 \\ -1.6 & 1.2 \end{bmatrix}.$$

**Solution.** The characteristic equation is the quadratic equation

$$\det[\mathbf{A} - \lambda\mathbf{I}] = \begin{vmatrix} -4 - \lambda & 4 \\ -1.6 & 1.2 - \lambda \end{vmatrix} = \lambda^2 + 2.8\lambda + 1.6 = 0.$$

It has the solutions  $\lambda_1 = -2$  and  $\lambda_2 = -0.8$ . These are the eigenvalues of  $\mathbf{A}$ .

Eigenvectors are obtained from (14\*). For  $\lambda = \lambda_1 = -2$  we have from (14\*)

$$\begin{aligned} (-4.0 + 2.0)x_1 + 4.0x_2 &= 0 \\ -1.6x_1 + (1.2 + 2.0)x_2 &= 0. \end{aligned}$$

A solution of the first equation is  $x_1 = 2$ ,  $x_2 = 1$ . This also satisfies the second equation. (Why?). Hence an eigenvector of  $\mathbf{A}$  corresponding to  $\lambda_1 = -2.0$  is

$$(17) \quad \mathbf{x}^{(1)} = \begin{bmatrix} 2 \\ 1 \end{bmatrix}. \quad \text{Similarly,} \quad \mathbf{x}^{(2)} = \begin{bmatrix} 1 \\ 0.8 \end{bmatrix}$$

is an eigenvector of  $\mathbf{A}$  corresponding to  $\lambda_2 = -0.8$ , as obtained from (14\*) with  $\lambda = \lambda_2$ . Verify this. ■

## 4.1 Systems of ODEs as Models

We first illustrate with a few typical examples that systems of ODEs can serve as models in various applications. We further show that a higher order ODE (with the highest derivative standing alone on one side) can be reduced to a first-order system. Both facts account for the practical importance of these systems.

**EXAMPLE 1 Mixing Problem Involving Two Tanks**

A mixing problem involving a single tank is modeled by a single ODE, and you may first review the corresponding Example 3 in Sec. 1.3 because the principle of modeling will be the same for two tanks. The model will be a system of two first-order ODEs.

Tank  $T_1$  and  $T_2$  in Fig. 77 contain initially 100 gal of water each. In  $T_1$  the water is pure, whereas 150 lb of fertilizer are dissolved in  $T_2$ . By circulating liquid at a rate of 2 gal/min and stirring (to keep the mixture uniform) the amounts of fertilizer  $y_1(t)$  in  $T_1$  and  $y_2(t)$  in  $T_2$  change with time  $t$ . How long should we let the liquid circulate so that  $T_1$  will contain at least half as much fertilizer as there will be left in  $T_2$ ?

**Solution.** *Step 1. Setting up the model.* As for a single tank, the time rate of change  $y_1'(t)$  of  $y_1(t)$  equals inflow minus outflow. Similarly for tank  $T_2$ . From Fig. 77 we see that

$$y_1' = \text{Inflow/min} - \text{Outflow/min} = \frac{2}{100}y_2 - \frac{2}{100}y_1 \quad (\text{Tank } T_1)$$

$$y_2' = \text{Inflow/min} - \text{Outflow/min} = \frac{2}{100}y_1 - \frac{2}{100}y_2 \quad (\text{Tank } T_2).$$

Hence the mathematical model of our mixture problem is the system of first-order ODEs

$$y_1' = -0.02y_1 + 0.02y_2 \quad (\text{Tank } T_1)$$

$$y_2' = 0.02y_1 - 0.02y_2 \quad (\text{Tank } T_2).$$

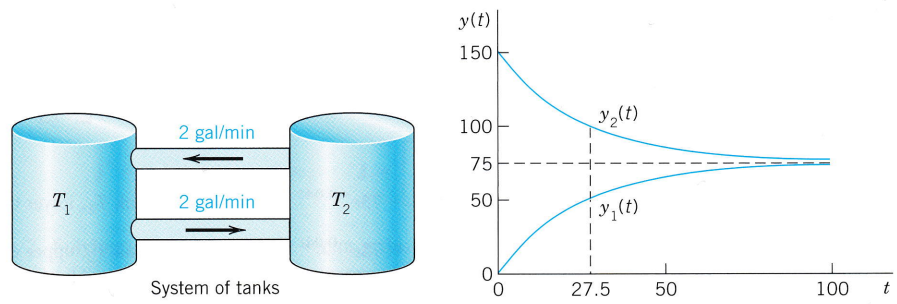


Fig. 77. Fertilizer content in Tanks  $T_1$  (lower curve) and  $T_2$

As a vector equation with column vector  $\mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \end{bmatrix}$  and matrix  $\mathbf{A}$  this becomes

$$\mathbf{y}' = \mathbf{A}\mathbf{y}, \quad \text{where} \quad \mathbf{A} = \begin{bmatrix} -0.02 & 0.02 \\ 0.02 & -0.02 \end{bmatrix}.$$

**Step 2. General solution.** As for a single equation, we try an exponential function of  $t$ ,

$$(1) \quad \mathbf{y} = \mathbf{x}e^{\lambda t}. \quad \text{Then} \quad \mathbf{y}' = \lambda \mathbf{x}e^{\lambda t} = \mathbf{A}\mathbf{x}e^{\lambda t}.$$

Dividing the last equation  $\lambda \mathbf{x}e^{\lambda t} = \mathbf{A}\mathbf{x}e^{\lambda t}$  by  $e^{\lambda t}$  and interchanging the left and right sides, we obtain

$$\mathbf{A}\mathbf{x} = \lambda \mathbf{x}.$$

We need nontrivial solutions (solutions that are not identically zero). Hence we have to look for eigenvalues and eigenvectors of  $\mathbf{A}$ . The eigenvalues are the solutions of the characteristic equation

$$(2) \quad \det(\mathbf{A} - \lambda \mathbf{I}) = \begin{vmatrix} -0.02 - \lambda & 0.02 \\ 0.02 & -0.02 - \lambda \end{vmatrix} = (-0.02 - \lambda)^2 - 0.02^2 = \lambda(\lambda + 0.04) = 0.$$

We see that  $\lambda_1 = 0$  (which can very well happen—don't get mixed up—it is *eigenvectors* that must not be zero) and  $\lambda_2 = -0.04$ . Eigenvectors are obtained from (14\*) in Sec. 4.0 with  $\lambda = 0$  and  $\lambda = -0.04$ . For our present  $\mathbf{A}$  this gives [we need only the first equation in (14\*)]

$$-0.02x_1 + 0.02x_2 = 0 \quad \text{and} \quad (-0.02 + 0.04)x_1 + 0.02x_2 = 0,$$

respectively. Hence  $x_1 = x_2$  and  $x_1 = -x_2$ , respectively, and we can take  $x_1 = x_2 = 1$  and  $x_1 = -x_2 = 1$ . This gives two eigenvectors corresponding to  $\lambda_1 = 0$  and  $\lambda_2 = -0.04$ , respectively, namely,

$$\mathbf{x}^{(1)} = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \quad \text{and} \quad \mathbf{x}^{(2)} = \begin{bmatrix} 1 \\ -1 \end{bmatrix}.$$

From (1) and the superposition principle (which continues to hold for systems of homogeneous linear ODEs) we thus obtain a solution

$$(3) \quad \mathbf{y} = c_1 \mathbf{x}^{(1)} e^{\lambda_1 t} + c_2 \mathbf{x}^{(2)} e^{\lambda_2 t} = c_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} + c_2 \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{-0.04t}$$

where  $c_1$  and  $c_2$  are arbitrary constants. Later we shall call this a **general solution**.

**Step 3. Use of initial conditions.** The initial conditions are  $y_1(0) = 0$  (no fertilizer in tank  $T_1$ ) and  $y_2(0) = 150$ . From this and (3) with  $t = 0$  we obtain

$$\mathbf{y}(0) = c_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} + c_2 \begin{bmatrix} 1 \\ -1 \end{bmatrix} = \begin{bmatrix} c_1 + c_2 \\ c_1 - c_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 150 \end{bmatrix}.$$

In components this is  $c_1 + c_2 = 0$ ,  $c_1 - c_2 = 150$ . The solution is  $c_1 = 75$ ,  $c_2 = -75$ . This gives the answer

$$\mathbf{y} = 75\mathbf{x}^{(1)} - 75\mathbf{x}^{(2)}e^{-0.04t} = 75 \begin{bmatrix} 1 \\ 1 \end{bmatrix} - 75 \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{-0.04t}.$$

In components,

$$\begin{aligned} y_1 &= 75 - 75e^{-0.04t} && \text{(Tank } T_1, \text{ lower curve)} \\ y_2 &= 75 + 75e^{-0.04t} && \text{(Tank } T_2, \text{ upper curve).} \end{aligned}$$

Figure 77 shows the exponential increase of  $y_1$  and the exponential decrease of  $y_2$  to the common limit 75 lb. Did you expect this for physical reasons? Can you physically explain why the curves look “symmetric”? Would the limit change if  $T_1$  initially contained 100 lb of fertilizer and  $T_2$  contained 50 lb?

**Step 4. Answer.**  $T_1$  contains half the fertilizer amount of  $T_2$  if it contains  $1/3$  of the total amount, that is, 50 lb. Thus

$$y_1 = 75 - 75e^{-0.04t} = 50, \quad e^{-0.04t} = \frac{1}{3}, \quad t = (\ln 3)/0.04 = 27.5.$$

Hence the fluid should circulate for at least about half an hour. ■

### EXAMPLE 2 Electrical Network

Find the currents  $I_1(t)$  and  $I_2(t)$  in the network in Fig. 78. Assume all currents and charges to be zero at  $t = 0$ , the instant when the switch is closed.

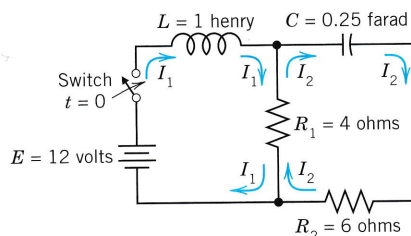


Fig. 78. Electrical network in Example 2

**Solution. Step 1. Setting up the mathematical model.** The model of this network is obtained from Kirchhoff's voltage law, as in Sec. 2.9 (where we considered single circuits). Let  $I_1(t)$  and  $I_2(t)$  be the currents in the left and right loops, respectively. In the left loop the voltage drops are  $L I_1' = I_1'$  [V] over the inductor and  $R_1(I_1 - I_2) = 4(I_1 - I_2)$  [V] over the resistor, the difference because  $I_1$  and  $I_2$  flow through the resistor in opposite directions. By Kirchhoff's voltage law the sum of these drops equals the voltage of the battery; that is,  $I_1' + 4(I_1 - I_2) = 12$ , hence

$$(4a) \quad I_1' = -4I_1 + 4I_2 + 12.$$

In the right loop the voltage drops are  $R_2 I_2 = 6I_2$  [V] and  $R_1(I_2 - I_1) = 4(I_2 - I_1)$  [V] over the resistors and  $(1/C) \int I_2 dt = 4 \int I_2 dt$  [V] over the capacitor, and their sum is zero,

$$6I_2 + 4(I_2 - I_1) + 4 \int I_2 dt = 0 \quad \text{or} \quad 10I_2 - 4I_1 + 4 \int I_2 dt = 0.$$

Division by 10 and differentiation gives  $I_2' - 0.4I_1' + 0.4I_2 = 0$ .

To simplify the solution process, we first get rid of  $0.4I_1'$ , which by (4a) equals  $0.4(-4I_1 + 4I_2 + 12)$ . Substitution into the present ODE gives

$$I_2' = 0.4I_1' - 0.4I_2 = 0.4(-4I_1 + 4I_2 + 12) - 0.4I_2$$

and by simplification

$$(4b) \quad I_2' = -1.6I_1 + 1.2I_2 + 4.8.$$

In matrix form, (4) is (we write  $\mathbf{J}$  since  $\mathbf{I}$  is the unit matrix)

$$(5) \quad \mathbf{J}' = \mathbf{A}\mathbf{J} + \mathbf{g}, \quad \text{where} \quad \mathbf{J} = \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}, \quad \mathbf{A} = \begin{bmatrix} -4.0 & 4.0 \\ -1.6 & 1.2 \end{bmatrix}, \quad \mathbf{g} = \begin{bmatrix} 12.0 \\ 4.8 \end{bmatrix}.$$

**Step 2. Solving (5).** Because of the vector  $\mathbf{g}$  this is a *nonhomogeneous* system, and we try to proceed as for a single ODE, solving first the *homogeneous* system  $\mathbf{J}' = \mathbf{A}\mathbf{J}$  (thus  $\mathbf{J}' - \mathbf{A}\mathbf{J} = \mathbf{0}$ ) by substituting  $\mathbf{J} = \mathbf{x}e^{\lambda t}$ . This gives

$$\mathbf{J}' = \lambda \mathbf{x}e^{\lambda t} = \mathbf{A}\mathbf{x}e^{\lambda t}, \quad \text{hence} \quad \mathbf{A}\mathbf{x} = \lambda \mathbf{x}.$$

Hence to obtain a nontrivial solution, we again need the eigenvalues and eigenvectors. For the present matrix  $\mathbf{A}$  they are derived in Example 1 in Sec. 4.0:

$$\lambda_1 = -2, \quad \mathbf{x}^{(1)} = \begin{bmatrix} 2 \\ 1 \end{bmatrix}; \quad \lambda_2 = -0.8, \quad \mathbf{x}^{(2)} = \begin{bmatrix} 1 \\ 0.8 \end{bmatrix}.$$

Hence a "general solution" of the homogeneous system is

$$\mathbf{J}_h = c_1 \mathbf{x}^{(1)} e^{-2t} + c_2 \mathbf{x}^{(2)} e^{-0.8t}.$$

For a particular solution of the nonhomogeneous system (5), since  $\mathbf{g}$  is constant, we try a constant column vector  $\mathbf{J}_p = \mathbf{a}$  with components  $a_1, a_2$ . Then  $\mathbf{J}_p' = \mathbf{0}$ , and substitution into (5) gives  $\mathbf{A}\mathbf{a} + \mathbf{g} = \mathbf{0}$ ; in components,

$$\begin{aligned} -4.0a_1 + 4.0a_2 + 12.0 &= 0 \\ -1.6a_1 + 1.2a_2 + 4.8 &= 0. \end{aligned}$$

The solution is  $a_1 = 3, a_2 = 0$ ; thus  $\mathbf{a} = \begin{bmatrix} 3 \\ 0 \end{bmatrix}$ . Hence

$$(6) \quad \mathbf{J} = \mathbf{J}_h + \mathbf{J}_p = c_1 \mathbf{x}^{(1)} e^{-2t} + c_2 \mathbf{x}^{(2)} e^{-0.8t} + \mathbf{a};$$

in components,

$$\begin{aligned} I_1 &= 2c_1 e^{-2t} + c_2 e^{-0.8t} + 3 \\ I_2 &= c_1 e^{-2t} + 0.8c_2 e^{-0.8t}. \end{aligned}$$

The initial conditions give

$$\begin{aligned} I_1(0) &= 2c_1 + c_2 + 3 = 0 \\ I_2(0) &= c_1 + 0.8c_2 = 0. \end{aligned}$$

Hence  $c_1 = -4$  and  $c_2 = 5$ . As the solution of our problem we thus obtain

$$(7) \quad \mathbf{J} = -4\mathbf{x}^{(1)} e^{-2t} + 5\mathbf{x}^{(2)} e^{-0.8t} + \mathbf{a}.$$

In components (Fig. 79b),

$$\begin{aligned} I_1 &= -8e^{-2t} + 5e^{-0.8t} + 3 \\ I_2 &= -4e^{-2t} + 4e^{-0.8t}. \end{aligned}$$

Now comes an important idea, on which we shall elaborate further, beginning in Sec. 4.3. Figure 79a shows  $I_1(t)$  and  $I_2(t)$  as two separate curves. Figure 79b shows these two currents as a single curve  $[I_1(t), I_2(t)]$  in the  $I_1I_2$ -plane. This is a parametric representation with time  $t$  as the parameter. It is often important to know in which sense such a curve is traced. This can be indicated by an arrow in the sense of increasing  $t$ , as is shown. The  $I_1I_2$ -plane is called the **phase plane** of our system (5), and the curve in Fig. 79b is called a **trajectory**. We shall see that such "**phase plane representations**" are far more important than graphs as in Fig. 79a because they will give a much better qualitative overall impression of the general behavior of whole families of solutions, not merely of one solution as in the present case. ■

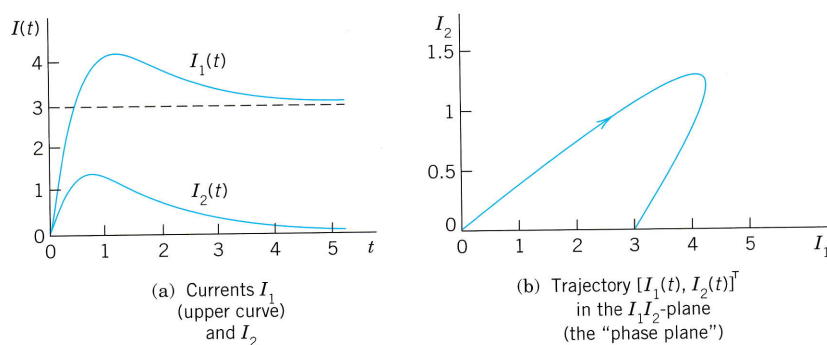


Fig. 79. Currents in Example 2

## Conversion of an $n$ th-Order ODE to a System

We show that an  $n$ th-order ODE of the general form (8) (see Theorem 1) can be converted to a system of  $n$  first-order ODEs. This is practically and theoretically important—practically because it permits the study and solution of single ODEs by methods for systems, and theoretically because it opens a way of including the theory of higher order ODEs into that of first-order systems. This conversion is another reason for the importance of systems, in addition to their use as models in various basic applications. The idea of the conversion is simple and straightforward, as follows.

### THEOREM 1

#### Conversion of an ODE

An  $n$ th-order ODE

$$(8) \quad y^{(n)} = F(t, y, y', \dots, y^{(n-1)})$$

can be converted to a system of  $n$  first-order ODEs by setting

$$(9) \quad y_1 = y, \quad y_2 = y', \quad y_3 = y'', \quad \dots, \quad y_n = y^{(n-1)}.$$

This system is of the form

$$(10) \quad \begin{aligned} y_1' &= y_2 \\ y_2' &= y_3 \\ &\vdots \\ y_{n-1}' &= y_n \\ y_n' &= F(t, y_1, y_2, \dots, y_n). \end{aligned}$$

**PROOF** The first  $n - 1$  of these  $n$  ODEs follow immediately from (9) by differentiation. Also,  $y_n' = y^{(n)}$  by (9), so that the last equation in (10) results from the given ODE (8). ■

**EXAMPLE 3** Mass on a Spring

To gain confidence in the conversion method, let us apply it to an old friend of ours, modeling the free motions of a mass on a spring (see Sec. 2.4)

$$my'' + cy' + ky = 0 \quad \text{or} \quad y'' = -\frac{c}{m}y' - \frac{k}{m}y.$$

For this ODE (8) the system (10) is linear and homogeneous,

$$\begin{aligned} y_1' &= y_2 \\ y_2' &= -\frac{k}{m}y_1 - \frac{c}{m}y_2. \end{aligned}$$

Setting  $\mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \end{bmatrix}$ , we get in matrix form

$$\mathbf{y}' = \mathbf{A}\mathbf{y} = \begin{bmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{c}{m} \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \end{bmatrix}.$$

The characteristic equation is

$$\det(\mathbf{A} - \lambda\mathbf{I}) = \begin{vmatrix} -\lambda & 1 \\ -\frac{k}{m} & -\frac{c}{m} - \lambda \end{vmatrix} = \lambda^2 + \frac{c}{m}\lambda + \frac{k}{m} = 0.$$

It agrees with that in Sec. 2.4. For an illustrative computation, let  $m = 1$ ,  $c = 2$ , and  $k = 0.75$ . Then

$$\lambda^2 + 2\lambda + 0.75 = (\lambda + 0.5)(\lambda + 1.5) = 0.$$

This gives the eigenvalues  $\lambda_1 = -0.5$  and  $\lambda_2 = -1.5$ . Eigenvectors follow from the first equation in  $\mathbf{A} - \lambda\mathbf{I} = \mathbf{0}$ , which is  $-\lambda x_1 + x_2 = 0$ . For  $\lambda_1$  this gives  $0.5x_1 + x_2 = 0$ , say,  $x_1 = 2$ ,  $x_2 = -1$ . For  $\lambda_2 = -1.5$  it gives  $1.5x_1 + x_2 = 0$ , say,  $x_1 = 1$ ,  $x_2 = -1.5$ . These eigenvectors

$$\mathbf{x}^{(1)} = \begin{bmatrix} 2 \\ -1 \end{bmatrix}, \quad \mathbf{x}^{(2)} = \begin{bmatrix} 1 \\ -1.5 \end{bmatrix} \quad \text{give} \quad \mathbf{y} = c_1 \begin{bmatrix} 2 \\ -1 \end{bmatrix} e^{-0.5t} + c_2 \begin{bmatrix} 1 \\ -1.5 \end{bmatrix} e^{-1.5t}.$$

This vector solution has the first component

$$y = y_1 = 2c_1 e^{-0.5t} + c_2 e^{-1.5t}$$

which is the expected solution. The second component is its derivative

$$y_2 = y_1' = y' = -c_1 e^{-0.5t} - 1.5c_2 e^{-1.5t}. \quad \blacksquare$$

**PROBLEM SET 4.1****1-6** MIXING PROBLEMS

- Find out without calculation whether doubling the flow rate in Example 1 has the same effect as halving the tank sizes. (Give a reason.)
- What happens in Example 1 if we replace  $T_2$  by a tank containing 500 gal of water and 150 lb of fertilizer dissolved in it?
- Derive the eigenvectors in Example 1 without consulting this book.
- In Example 1 find a "general solution" for any ratio  $a = (\text{flow rate})/(\text{tank size})$ , tank sizes being equal. Comment on the result.
- If you extend Example 1 by a tank  $T_3$  of the same size as the others and connected to  $T_2$  by two tubes with



flow rates as between  $T_1$  and  $T_2$ , what system of ODEs will you get?

6. Find a "general solution" of the system in Prob. 5.

### 7–10 ELECTRICAL NETWORKS

7. Find the currents in Example 2 if the initial currents are 0 and  $-3$  A (minus meaning that  $I_2(0)$  flows against the direction of the arrow).  
 8. Find the currents in Example 2 if the resistance of  $R_1$  and  $R_2$  is doubled (general solution only). First, guess.  
 9. What are the limits of the currents in Example 2? Explain them in terms of physics.  
 10. Find the currents in Example 2 if the capacitance is changed to  $C = 1/5.4$  F (farad).

### 11–15 CONVERSION TO SYSTEMS

Find a general solution of the given ODE (a) by first converting it to a system, (b), as given. (Show the details of your work.)

11.  $y'' - 4y = 0$                       12.  $y'' + 2y' - 24y = 0$   
 13.  $y'' - y' = 0$                         14.  $y'' + 15y' + 50y = 0$   
 15.  $64y'' - 48y' - 7y = 0$

16. **TEAM PROJECT. Two Masses on Springs.** (a) Set up the model for the (undamped) system in Fig. 80.

(b) Solve the system of ODEs obtained. *Hint.* Try  $\mathbf{y} = \mathbf{x}e^{\omega t}$  and set  $\omega^2 = \lambda$ . Proceed as in Example 1 or 2.

(c) Describe the influence of initial conditions on the possible kind of motions.

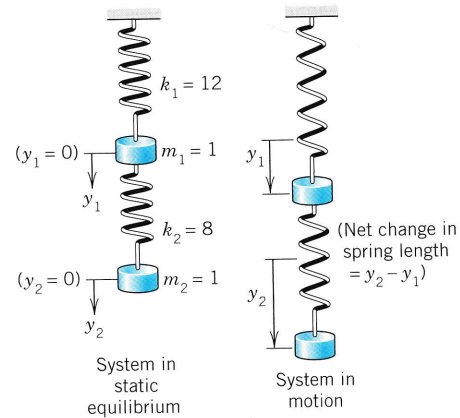


Fig. 80. Mechanical system in Team Project 16

## 4.2 Basic Theory of Systems of ODEs

In this section we discuss some basic concepts and facts about systems of ODEs that are quite similar to those for single ODEs.

The first-order systems in the last section were special cases of the more general system

$$\begin{aligned} y_1' &= f_1(t, y_1, \dots, y_n) \\ y_2' &= f_2(t, y_1, \dots, y_n) \\ &\dots \\ y_n' &= f_n(t, y_1, \dots, y_n). \end{aligned} \quad (1)$$

We can write the system (1) as a vector equation by introducing the column vectors  $\mathbf{y} = [y_1 \ \dots \ y_n]^T$  and  $\mathbf{f} = [f_1 \ \dots \ f_n]^T$  (where  $\top$  means *transposition* and saves us the space that would be needed for writing  $\mathbf{y}$  and  $\mathbf{f}$  as columns). This gives

$$\mathbf{y}' = \mathbf{f}(t, \mathbf{y}). \quad (1)$$

This system (1) includes almost all cases of practical interest. For  $n = 1$  it becomes  $y_1' = f_1(t, y_1)$  or, simply,  $y' = f(t, y)$ , well known to us from Chap. 1.

A **solution** of (1) on some interval  $a < t < b$  is a set of  $n$  differentiable functions

$$y_1 = h_1(t), \quad \dots, \quad y_n = h_n(t)$$

on  $a < t < b$  that satisfy (1) throughout this interval. In vector form, introducing the “solution vector”  $\mathbf{h} = [h_1 \ \cdots \ h_n]^T$  (a column vector!) we can write

$$\mathbf{y} = \mathbf{h}(t).$$

An **initial value problem** for (1) consists of (1) and  $n$  given **initial conditions**

$$(2) \quad y_1(t_0) = K_1, \quad y_2(t_0) = K_2, \quad \cdots, \quad y_n(t_0) = K_n,$$

in vector form,  $\mathbf{y}(t_0) = \mathbf{K}$ , where  $t_0$  is a specified value of  $t$  in the interval considered and the components of  $\mathbf{K} = [K_1 \ \cdots \ K_n]^T$  are given numbers. Sufficient conditions for the existence and uniqueness of a solution of an initial value problem (1), (2) are stated in the following theorem, which extends the theorems in Sec. 1.7 for a single equation. (For a proof, see Ref. [A7].)

**THEOREM 1**

**Existence and Uniqueness Theorem**

Let  $f_1, \cdots, f_n$  in (1) be continuous functions having continuous partial derivatives  $\partial f_1/\partial y_1, \cdots, \partial f_1/\partial y_n, \cdots, \partial f_n/\partial y_1, \cdots, \partial f_n/\partial y_n$  in some domain  $R$  of  $t, y_1, y_2, \cdots, y_n$ -space containing the point  $(t_0, K_1, \cdots, K_n)$ . Then (1) has a solution on some interval  $t_0 - \alpha < t < t_0 + \alpha$  satisfying (2), and this solution is unique.

### Linear Systems

Extending the notion of a *linear* ODE, we call (1) a **linear system** if it is linear in  $y_1, \cdots, y_n$ ; that is, if it can be written

$$(3) \quad \begin{aligned} y_1' &= a_{11}(t)y_1 + \cdots + a_{1n}(t)y_n + g_1(t) \\ &\vdots \\ y_n' &= a_{n1}(t)y_1 + \cdots + a_{nn}(t)y_n + g_n(t). \end{aligned}$$

In vector form, this becomes

$$(3) \quad \mathbf{y}' = \mathbf{A}\mathbf{y} + \mathbf{g}$$

where  $\mathbf{A} = \begin{bmatrix} a_{11} & \cdots & a_{1n} \\ \cdot & \cdots & \cdot \\ a_{n1} & \cdots & a_{nn} \end{bmatrix}, \quad \mathbf{y} = \begin{bmatrix} y_1 \\ \vdots \\ y_n \end{bmatrix}, \quad \mathbf{g} = \begin{bmatrix} g_1 \\ \vdots \\ g_n \end{bmatrix}.$

This system is called **homogeneous** if  $\mathbf{g} = \mathbf{0}$ , so that it is

$$(4) \quad \mathbf{y}' = \mathbf{A}\mathbf{y}.$$

If  $\mathbf{g} \neq \mathbf{0}$ , then (3) is called **nonhomogeneous**. The system in Example 1 in the last section is homogeneous and in Example 2 nonhomogeneous. The system in Example 3 is homogeneous.

For a linear system (3) we have  $\partial f_1/\partial y_1 = a_{11}(t), \dots, \partial f_n/\partial y_n = a_{nn}(t)$  in Theorem 1. Hence for a linear system we simply obtain the following.

**THEOREM 2****Existence and Uniqueness in the Linear Case**

Let the  $a_{jk}$ 's and  $g_j$ 's in (3) be continuous functions of  $t$  on an open interval  $\alpha < t < \beta$  containing the point  $t = t_0$ . Then (3) has a solution  $\mathbf{y}(t)$  on this interval satisfying (2), and this solution is unique.

As for a single homogeneous linear ODE we have

**THEOREM 3****Superposition Principle or Linearity Principle**

If  $\mathbf{y}^{(1)}$  and  $\mathbf{y}^{(2)}$  are solutions of the **homogeneous linear** system (4) on some interval, so is any linear combination  $\mathbf{y} = c_1\mathbf{y}^{(1)} + c_2\mathbf{y}^{(2)}$ .

**PROOF** Differentiating and using (4), we obtain

$$\begin{aligned} \mathbf{y}' &= [c_1\mathbf{y}^{(1)} + c_2\mathbf{y}^{(2)}]' \\ &= c_1\mathbf{y}^{(1)'} + c_2\mathbf{y}^{(2)'} \\ &= c_1\mathbf{A}\mathbf{y}^{(1)} + c_2\mathbf{A}\mathbf{y}^{(2)} \\ &= \mathbf{A}(c_1\mathbf{y}^{(1)} + c_2\mathbf{y}^{(2)}) = \mathbf{A}\mathbf{y}. \end{aligned}$$

The general theory of linear systems of ODEs is quite similar to that of a single linear ODE in Secs. 2.6 and 2.7. To see this, we explain the most basic concepts and facts. For proofs we refer to more advanced texts, such as [A7].

**Basis. General Solution. Wronskian**

By a **basis** or a **fundamental system** of solutions of the homogeneous system (4) on some interval  $J$  we mean a linearly independent set of  $n$  solutions  $\mathbf{y}^{(1)}, \dots, \mathbf{y}^{(n)}$  of (4) on that interval. (We write  $J$  because we need  $\mathbf{I}$  to denote the unit matrix.) We call a corresponding linear combination

$$(5) \quad \mathbf{y} = c_1\mathbf{y}^{(1)} + \dots + c_n\mathbf{y}^{(n)} \quad (c_1, \dots, c_n \text{ arbitrary})$$

a **general solution** of (4) on  $J$ . It can be shown that if the  $a_{jk}(t)$  in (4) are continuous on  $J$ , then (4) has a basis of solutions on  $J$ , hence a general solution, which includes every solution of (4) on  $J$ .

We can write  $n$  solutions  $\mathbf{y}^{(1)}, \dots, \mathbf{y}^{(n)}$  of (4) on some interval  $J$  as columns of an  $n \times n$  matrix

$$(6) \quad \mathbf{Y} = [\mathbf{y}^{(1)} \quad \dots \quad \mathbf{y}^{(n)}].$$

The determinant of  $\mathbf{Y}$  is called the **Wronskian** of  $\mathbf{y}^{(1)}, \dots, \mathbf{y}^{(n)}$ , written

$$(7) \quad W(\mathbf{y}^{(1)}, \dots, \mathbf{y}^{(n)}) = \begin{vmatrix} y_1^{(1)} & y_1^{(2)} & \cdots & y_1^{(n)} \\ y_2^{(1)} & y_2^{(2)} & \cdots & y_2^{(n)} \\ \cdot & \cdot & \cdots & \cdot \\ y_n^{(1)} & y_n^{(2)} & \cdots & y_n^{(n)} \end{vmatrix}.$$

The columns are these solutions, each in terms of components. These solutions form a basis on  $J$  if and only if  $W$  is not zero at any  $t_1$  in this interval.  $W$  either is identically zero or is nowhere zero in  $J$ . (This is similar to Secs. 2.6 and 3.1.)

If the solutions  $\mathbf{y}^{(1)}, \dots, \mathbf{y}^{(n)}$  in (5) form a basis (a fundamental system), then (6) is often called a **fundamental matrix**. Introducing a column vector  $\mathbf{c} = [c_1 \ c_2 \ \cdots \ c_n]^T$ , we can now write (5) simply as

$$(8) \quad \mathbf{y} = \mathbf{Y}\mathbf{c}.$$

Furthermore, we can relate (7) to Sec. 2.6, as follows. If  $y$  and  $z$  are solutions of a second-order homogeneous linear ODE, their Wronskian is

$$W(y, z) = \begin{vmatrix} y & z \\ y' & z' \end{vmatrix}.$$

To write this ODE as a system, we have to set  $y = y_1$ ,  $y' = y_1' = y_2$  and similarly for  $z$  (see Sec. 4.1). But then  $W(y, z)$  becomes (7), except for notation.

## 4.3 Constant-Coefficient Systems. Phase Plane Method

Continuing, we now assume that our homogeneous linear system

$$(1) \quad \mathbf{y}' = \mathbf{A}\mathbf{y}$$

under discussion has *constant coefficients*, so that the  $n \times n$  matrix  $\mathbf{A} = [a_{jk}]$  has entries not depending on  $t$ . We want to solve (1). Now a single ODE  $y' = ky$  has the solution  $y = Ce^{kt}$ . So let us try

$$(2) \quad \mathbf{y} = \mathbf{x}e^{\lambda t}.$$

Substitution into (1) gives  $\mathbf{y}' = \lambda \mathbf{x}e^{\lambda t} = \mathbf{A}\mathbf{y} = \mathbf{A}\mathbf{x}e^{\lambda t}$ . Dividing by  $e^{\lambda t}$ , we obtain the **eigenvalue problem**

$$(3) \quad \mathbf{A}\mathbf{x} = \lambda \mathbf{x}.$$

Thus the nontrivial solutions of (1) (solutions that are not zero vectors) are of the form (2), where  $\lambda$  is an eigenvalue of  $\mathbf{A}$  and  $\mathbf{x}$  is a corresponding eigenvector.

We assume that  $\mathbf{A}$  has a linearly independent set of  $n$  eigenvectors. This holds in most applications, in particular if  $\mathbf{A}$  is symmetric ( $a_{kj} = a_{jk}$ ) or skew-symmetric ( $a_{kj} = -a_{jk}$ ) or has  $n$  different eigenvalues.

Let those eigenvectors be  $\mathbf{x}^{(1)}, \dots, \mathbf{x}^{(n)}$  and let them correspond to eigenvalues  $\lambda_1, \dots, \lambda_n$  (which may be all different, or some—or even all—may be equal). Then the corresponding solutions (2) are

$$(4) \quad \mathbf{y}^{(1)} = \mathbf{x}^{(1)} e^{\lambda_1 t}, \quad \dots, \quad \mathbf{y}^{(n)} = \mathbf{x}^{(n)} e^{\lambda_n t}.$$

Their Wronskian  $W = W(\mathbf{y}^{(1)}, \dots, \mathbf{y}^{(n)})$  [(7) in Sec. 4.2] is given by

$$W = (\mathbf{y}^{(1)}, \dots, \mathbf{y}^{(n)}) = \begin{vmatrix} x_1^{(1)} e^{\lambda_1 t} & \dots & x_1^{(n)} e^{\lambda_n t} \\ x_2^{(1)} e^{\lambda_1 t} & \dots & x_2^{(n)} e^{\lambda_n t} \\ \cdot & \dots & \cdot \\ x_n^{(1)} e^{\lambda_1 t} & \dots & x_n^{(n)} e^{\lambda_n t} \end{vmatrix} = e^{\lambda_1 t + \dots + \lambda_n t} \begin{vmatrix} x_1^{(1)} & \dots & x_1^{(n)} \\ x_2^{(1)} & \dots & x_2^{(n)} \\ \cdot & \dots & \cdot \\ x_n^{(1)} & \dots & x_n^{(n)} \end{vmatrix}.$$

On the right, the exponential function is never zero, and the determinant is not zero either because its columns are the  $n$  linearly independent eigenvectors. This proves the following theorem, whose assumption is true if the matrix  $\mathbf{A}$  is symmetric or skew-symmetric, or if the  $n$  eigenvalues of  $\mathbf{A}$  are all different.

### THEOREM 1

#### General Solution

If the constant matrix  $\mathbf{A}$  in the system (1) has a linearly independent set of  $n$  eigenvectors, then the corresponding solutions  $\mathbf{y}^{(1)}, \dots, \mathbf{y}^{(n)}$  in (4) form a basis of solutions of (1), and the corresponding general solution is

$$(5) \quad \mathbf{y} = c_1 \mathbf{x}^{(1)} e^{\lambda_1 t} + \dots + c_n \mathbf{x}^{(n)} e^{\lambda_n t}.$$

## How to Graph Solutions in the Phase Plane

We shall now concentrate on systems (1) with constant coefficients consisting of two ODEs

$$(6) \quad \mathbf{y}' = \mathbf{A}\mathbf{y}; \quad \text{in components,} \quad \begin{aligned} y_1' &= a_{11}y_1 + a_{12}y_2 \\ y_2' &= a_{21}y_1 + a_{22}y_2. \end{aligned}$$

Of course, we can graph solutions of (6),

$$(7) \quad \mathbf{y}(t) = \begin{bmatrix} y_1(t) \\ y_2(t) \end{bmatrix},$$

as two curves over the  $t$ -axis, one for each component of  $\mathbf{y}(t)$ . (Figure 79a in Sec. 4.1 shows an example.) But we can also graph (7) as a single curve in the  $y_1y_2$ -plane. This is a *parametric representation* (*parametric equation*) with parameter  $t$ . (See Fig. 79b for an example. Many more follow. Parametric equations also occur in calculus.) Such a curve is called a **trajectory** (or sometimes an *orbit* or *path*) of (6). The  $y_1y_2$ -plane is called the **phase plane**.<sup>1</sup> If we fill the phase plane with trajectories of (6), we obtain the so-called **phase portrait** of (6).

### EXAMPLE 1 Trajectories in the Phase Plane (Phase Portrait)

In order to see what is going on, let us find and graph solutions of the system

$$(8) \quad \mathbf{y}' = \mathbf{A}\mathbf{y} = \begin{bmatrix} -3 & 1 \\ 1 & -3 \end{bmatrix} \mathbf{y}, \quad \text{thus} \quad \begin{aligned} y_1' &= -3y_1 + y_2 \\ y_2' &= y_1 - 3y_2. \end{aligned}$$

**Solution.** By substituting  $\mathbf{y} = \mathbf{x}e^{\lambda t}$  and  $\mathbf{y}' = \lambda\mathbf{x}e^{\lambda t}$  and dropping the exponential function we get  $\mathbf{A}\mathbf{x} = \lambda\mathbf{x}$ . The characteristic equation is

$$\det(\mathbf{A} - \lambda\mathbf{I}) = \begin{vmatrix} -3 - \lambda & 1 \\ 1 & -3 - \lambda \end{vmatrix} = \lambda^2 + 6\lambda + 8 = 0.$$

This gives the eigenvalues  $\lambda_1 = -2$  and  $\lambda_2 = -4$ . Eigenvectors are then obtained from

$$(-3 - \lambda)x_1 + x_2 = 0.$$

For  $\lambda_1 = -2$  this is  $-x_1 + x_2 = 0$ . Hence we can take  $\mathbf{x}^{(1)} = [1 \ 1]^T$ . For  $\lambda_2 = -4$  this becomes  $x_1 + x_2 = 0$ , and an eigenvector is  $\mathbf{x}^{(2)} = [1 \ -1]^T$ . This gives the general solution

$$\mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = c_1\mathbf{y}^{(1)} + c_2\mathbf{y}^{(2)} = c_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-2t} + c_2 \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{-4t}.$$

Figure 81 on p. 142 shows a phase portrait of some of the trajectories (to which more trajectories could be added if so desired). The two straight trajectories correspond to  $c_1 = 0$  and  $c_2 = 0$  and the others to other choices of  $c_1, c_2$ . ■

Studies of solutions in the phase plane have recently become quite important, along with advances in computer graphics, because a phase portrait gives a good general qualitative impression of the entire family of solutions. This method becomes particularly valuable in the frequent cases when solving an ODE or a system is inconvenient or impossible.

## Critical Points of the System (6)

The point  $\mathbf{y} = \mathbf{0}$  in Fig. 81 seems to be a common point of all trajectories, and we want to explore the reason for this remarkable observation. The answer will follow by calculus. Indeed, from (6) we obtain

$$(9) \quad \frac{dy_2}{dy_1} = \frac{y_2' dt}{y_1' dt} = \frac{y_2'}{y_1'} = \frac{a_{21}y_1 + a_{22}y_2}{a_{11}y_1 + a_{12}y_2}.$$

<sup>1</sup>A name that comes from physics, where it is the  $y$ -( $mv$ )-plane, used to plot a motion in terms of position  $y$  and velocity  $y' = v$  ( $m = \text{mass}$ ); but the name is now used quite generally for the  $y_1y_2$ -plane.

The use of the phase plane is a **qualitative method**, a method of obtaining general qualitative information on solutions without actually solving an ODE or a system. This method was created by HENRI POINCARÉ (1854–1912), a great French mathematician, whose work was also fundamental in complex analysis, divergent series, topology, and astronomy.

This associates with every point  $P: (y_1, y_2)$  a unique tangent direction  $dy_2/dy_1$  of the trajectory passing through  $P$ , except for the point  $P = P_0: (0, 0)$ , where the right side of (9) becomes  $0/0$ . This point  $P_0$ , at which  $dy_2/dy_1$  becomes undetermined, is called a **critical point** of (6).

## Five Types of Critical Points

There are five types of critical points depending on the geometric shape of the trajectories near them. They are called **improper nodes**, **proper nodes**, **saddle points**, **centers**, and **spiral points**. We define and illustrate them in Examples 1–5.

### EXAMPLE 1 (Continued) Improper Node (Fig. 81)

An **improper node** is a critical point  $P_0$  at which all the trajectories, except for two of them, have the same limiting direction of the tangent. The two exceptional trajectories also have a limiting direction of the tangent at  $P_0$  which, however, is different.

The system (8) has an improper node at  $\mathbf{0}$ , as its phase portrait Fig. 81 shows. The common limiting direction at  $\mathbf{0}$  is that of the eigenvector  $\mathbf{x}^{(1)} = [1 \ 1]^T$  because  $e^{-4t}$  goes to zero faster than  $e^{-2t}$  as  $t$  increases. The two exceptional limiting tangent directions are those of  $\mathbf{x}^{(2)} = [1 \ -1]^T$  and  $-\mathbf{x}^{(2)} = [-1 \ 1]^T$ . ■

### EXAMPLE 2 Proper Node (Fig. 82)

A **proper node** is a critical point  $P_0$  at which every trajectory has a definite limiting direction and for any given direction  $\mathbf{d}$  at  $P_0$  there is a trajectory having  $\mathbf{d}$  as its limiting direction.

The system

$$(10) \quad \mathbf{y}' = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \mathbf{y}, \quad \text{thus} \quad \begin{aligned} y_1' &= y_1 \\ y_2' &= y_2 \end{aligned}$$

has a proper node at the origin (see Fig. 82). Indeed, the matrix is the unit matrix. Its characteristic equation  $(1 - \lambda)^2 = 0$  has the root  $\lambda = 1$ . Any  $\mathbf{x} \neq \mathbf{0}$  is an eigenvector, and we can take  $[1 \ 0]^T$  and  $[0 \ 1]^T$ . Hence a general solution is

$$\mathbf{y} = c_1 \begin{bmatrix} 1 \\ 0 \end{bmatrix} e^t + c_2 \begin{bmatrix} 0 \\ 1 \end{bmatrix} e^t \quad \text{or} \quad \begin{aligned} y_1 &= c_1 e^t \\ y_2 &= c_2 e^t \end{aligned} \quad \text{or} \quad c_1 y_2 = c_2 y_1. \quad \blacksquare$$

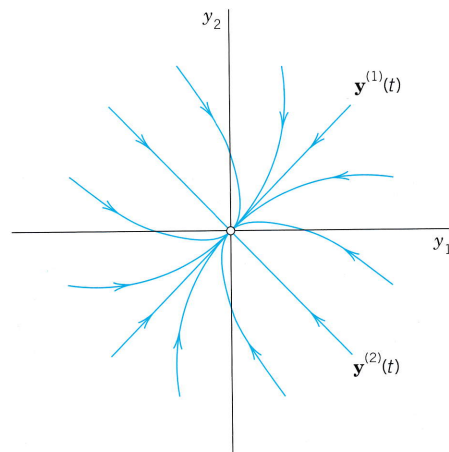


Fig. 81. Trajectories of the system (8) (Improper node)

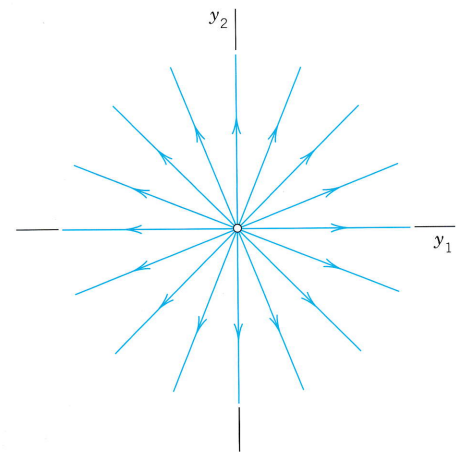


Fig. 82. Trajectories of the system (10) (Proper node)

**EXAMPLE 3 Saddle Point (Fig. 83)**

A **saddle point** is a critical point  $P_0$  at which there are two incoming trajectories, two outgoing trajectories, and all the other trajectories in a neighborhood of  $P_0$  bypass  $P_0$ .

The system

$$(11) \quad \mathbf{y}' = \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix} \mathbf{y}, \quad \text{thus} \quad \begin{aligned} y_1' &= y_1 \\ y_2' &= -y_2 \end{aligned}$$

has a saddle point at the origin. Its characteristic equation  $(1 - \lambda)(-1 - \lambda) = 0$  has the roots  $\lambda_1 = 1$  and  $\lambda_2 = -1$ . For  $\lambda = 1$  an eigenvector  $[1 \ 0]^T$  is obtained from the second row of  $(\mathbf{A} - \lambda\mathbf{I})\mathbf{x} = \mathbf{0}$ , that is,  $0x_1 + (-1 - 1)x_2 = 0$ . For  $\lambda_2 = -1$  the first row gives  $[0 \ 1]^T$ . Hence a general solution is

$$\mathbf{y} = c_1 \begin{bmatrix} 1 \\ 0 \end{bmatrix} e^t + c_2 \begin{bmatrix} 0 \\ 1 \end{bmatrix} e^{-t} \quad \text{or} \quad \begin{aligned} y_1 &= c_1 e^t \\ y_2 &= c_2 e^{-t} \end{aligned} \quad \text{or} \quad y_1 y_2 = \text{const.}$$

This is a family of hyperbolas (and the coordinate axes); see Fig. 83. ■

**EXAMPLE 4 Center (Fig. 84)**

A **center** is a critical point that is enclosed by infinitely many closed trajectories.

The system

$$(12) \quad \mathbf{y}' = \begin{bmatrix} 0 & 1 \\ -4 & 0 \end{bmatrix} \mathbf{y}, \quad \text{thus} \quad \begin{aligned} y_1' &= y_2 \\ y_2' &= -4y_1 \end{aligned}$$

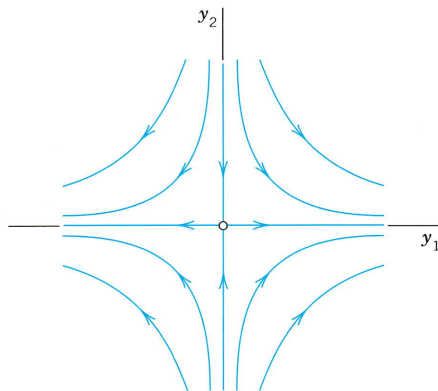
has a center at the origin. The characteristic equation  $\lambda^2 + 4 = 0$  gives the eigenvalues  $2i$  and  $-2i$ . For  $2i$  an eigenvector follows from the first equation  $-2ix_1 + x_2 = 0$  of  $(\mathbf{A} - \lambda\mathbf{I})\mathbf{x} = \mathbf{0}$ , say,  $[1 \ 2i]^T$ . For  $\lambda = -2i$  that equation is  $-(-2i)x_1 + x_2 = 0$  and gives, say,  $[1 \ -2i]^T$ . Hence a complex general solution is

$$(12^*) \quad \mathbf{y} = c_1 \begin{bmatrix} 1 \\ 2i \end{bmatrix} e^{2it} + c_2 \begin{bmatrix} 1 \\ -2i \end{bmatrix} e^{-2it}, \quad \text{thus} \quad \begin{aligned} y_1 &= c_1 e^{2it} + c_2 e^{-2it} \\ y_2 &= 2ic_1 e^{2it} - 2ic_2 e^{-2it}. \end{aligned}$$

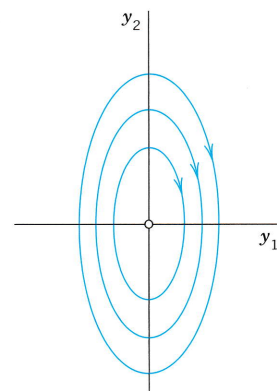
The next step would be the transformation of this solution to real form by the Euler formula (Sec. 2.2). But we were just curious to see what kind of eigenvalues we obtain in the case of a center. Accordingly, we do not continue, but start again from the beginning and use a shortcut. We rewrite the given equations in the form  $y_1' = y_2$ ,  $4y_1 = -y_2'$ ; then the product of the left sides must equal the product of the right sides,

$$4y_1 y_1' = -y_2 y_2'. \quad \text{By integration,} \quad 2y_1^2 + \frac{1}{2}y_2^2 = \text{const.}$$

This is a family of ellipses (see Fig. 84) enclosing the center at the origin. ■



**Fig. 83.** Trajectories of the system (11) (Saddle point)



**Fig. 84.** Trajectories of the system (12) (Center)



**EXAMPLE 5** Spiral Point (Fig. 85)

A **spiral point** is a critical point  $P_0$  about which the trajectories spiral, approaching  $P_0$  as  $t \rightarrow \infty$  (or tracing these spirals in the opposite sense, away from  $P_0$ ).

The system

$$(13) \quad \mathbf{y}' = \begin{bmatrix} -1 & 1 \\ -1 & -1 \end{bmatrix} \mathbf{y}, \quad \text{thus} \quad \begin{aligned} y_1' &= -y_1 + y_2 \\ y_2' &= -y_1 - y_2 \end{aligned}$$

has a spiral point at the origin, as we shall see. The characteristic equation is  $\lambda^2 + 2\lambda + 2 = 0$ . It gives the eigenvalues  $-1 + i$  and  $-1 - i$ . Corresponding eigenvectors are obtained from  $(-1 - \lambda)x_1 + x_2 = 0$ . For  $\lambda = -1 + i$  this becomes  $-ix_1 + x_2 = 0$  and we can take  $\begin{bmatrix} 1 \\ i \end{bmatrix}^T$  as an eigenvector. Similarly, an eigenvector corresponding to  $-1 - i$  is  $\begin{bmatrix} 1 \\ -i \end{bmatrix}^T$ . This gives the complex general solution

$$\mathbf{y} = c_1 \begin{bmatrix} 1 \\ i \end{bmatrix} e^{(-1+i)t} + c_2 \begin{bmatrix} 1 \\ -i \end{bmatrix} e^{(-1-i)t}.$$

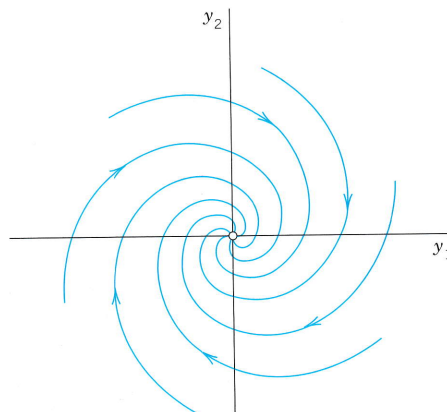
The next step would be the transformation of this complex solution to a real general solution by the Euler formula. But, as in the last example, we just wanted to see what eigenvalues to expect in the case of a spiral point. Accordingly, we start again from the beginning and instead of that rather lengthy systematic calculation we use a shortcut. We multiply the first equation in (13) by  $y_1$ , the second by  $y_2$ , and add, obtaining

$$y_1 y_1' + y_2 y_2' = -(y_1^2 + y_2^2).$$

We now introduce polar coordinates  $r, t$ , where  $r^2 = y_1^2 + y_2^2$ . Differentiating this with respect to  $t$  gives  $2rr' = 2y_1 y_1' + 2y_2 y_2'$ . Hence the previous equation can be written

$$rr' = -r^2, \quad \text{Thus,} \quad r' = -r, \quad dr/r = -dt, \quad \ln|r| = -t + c^*, \quad r = ce^{-t}.$$

For each real  $c$  this is a spiral, as claimed. (see Fig. 85). ■



**Fig. 85.** Trajectories of the system (13) (Spiral point)

**EXAMPLE 6** No Basis of Eigenvectors Available. Degenerate Node (Fig. 86)

This cannot happen if  $\mathbf{A}$  in (1) is symmetric ( $a_{kj} = a_{jk}$ , as in Examples 1–3) or skew-symmetric ( $a_{kj} = -a_{jk}$ , thus  $a_{jj} = 0$ ). And it does not happen in many other cases (see Examples 4 and 5). Hence it suffices to explain the method to be used by an example.

Find and graph a general solution of

$$(14) \quad \mathbf{y}' = \mathbf{A}\mathbf{y} = \begin{bmatrix} 4 & 1 \\ -1 & 2 \end{bmatrix} \mathbf{y}.$$

**Solution.**  $\mathbf{A}$  is not skew-symmetric! Its characteristic equation is

$$\det(\mathbf{A} - \lambda\mathbf{I}) = \begin{vmatrix} 4 - \lambda & 1 \\ -1 & 2 - \lambda \end{vmatrix} = \lambda^2 - 6\lambda + 9 = (\lambda - 3)^2 = 0.$$

It has a double root  $\lambda = 3$ . Hence eigenvectors are obtained from  $(4 - \lambda)x_1 + x_2 = 0$ , thus from  $x_1 + x_2 = 0$ , say,  $\mathbf{x}^{(1)} = [1 \ -1]^T$  and nonzero multiples of it (which do not help). The method now is to substitute

$$\mathbf{y}^{(2)} = \mathbf{x}te^{\lambda t} + \mathbf{u}e^{\lambda t}$$

with constant  $\mathbf{u} = [u_1 \ u_2]^T$  into (14). (The  $\mathbf{x}t$ -term alone, the analog of what we did in Sec. 2.2 in the case of a double root, would not be enough. Try it.) This gives

$$\mathbf{y}^{(2)'} = \mathbf{x}e^{\lambda t} + \lambda\mathbf{x}te^{\lambda t} + \lambda\mathbf{u}e^{\lambda t} = \mathbf{A}\mathbf{y}^{(2)} = \mathbf{A}\mathbf{x}te^{\lambda t} + \mathbf{A}\mathbf{u}e^{\lambda t}.$$

On the right,  $\mathbf{A}\mathbf{x} = \lambda\mathbf{x}$ . Hence the terms  $\lambda\mathbf{x}te^{\lambda t}$  cancel, and then division by  $e^{\lambda t}$  gives

$$\mathbf{x} + \lambda\mathbf{u} = \mathbf{A}\mathbf{u}, \quad \text{thus} \quad (\mathbf{A} - \lambda\mathbf{I})\mathbf{u} = \mathbf{x}.$$

Here  $\lambda = 3$  and  $\mathbf{x} = [1 \ -1]^T$ , so that

$$(\mathbf{A} - 3\mathbf{I})\mathbf{u} = \begin{bmatrix} 4 - 3 & 1 \\ -1 & 2 - 3 \end{bmatrix} \mathbf{u} = \begin{bmatrix} 1 \\ -1 \end{bmatrix}, \quad \text{thus} \quad \begin{aligned} u_1 + u_2 &= 1 \\ -u_1 - u_2 &= -1. \end{aligned}$$

A solution, linearly independent of  $\mathbf{x} = [1 \ -1]^T$ , is  $\mathbf{u} = [0 \ 1]^T$ . This yields the answer (Fig. 86)

$$\mathbf{y} = c_1\mathbf{y}^{(1)} + c_2\mathbf{y}^{(2)} = c_1 \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{3t} + c_2 \left( \begin{bmatrix} 1 \\ -1 \end{bmatrix} t + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \right) e^{3t}.$$

The critical point at the origin is often called a **degenerate node**.  $c_1\mathbf{y}^{(1)}$  gives the heavy straight line, with  $c_1 > 0$  the lower part and  $c_1 < 0$  the upper part of it.  $\mathbf{y}^{(2)}$  gives the right part of the heavy curve from 0 through the second, first, and—finally—fourth quadrants.  $-\mathbf{y}^{(2)}$  gives the other part of that curve. ■

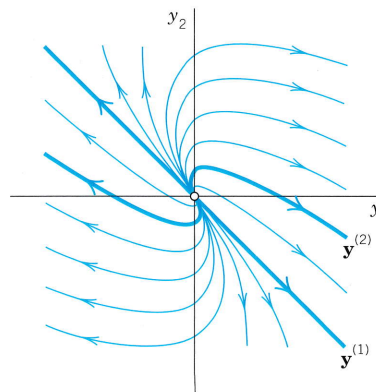


Fig. 86. Degenerate node in Example 6

We mention that for a system (1) with three or more equations and a triple eigenvalue with only one linearly independent eigenvector, one will get two solutions, as just discussed, and a third linearly independent one from

$$\mathbf{y}^{(3)} = \frac{1}{2}\mathbf{x}t^2e^{\lambda t} + \mathbf{u}te^{\lambda t} + \mathbf{v}e^{\lambda t} \quad \text{with } \mathbf{v} \text{ from } \quad \mathbf{u} + \lambda\mathbf{v} = \mathbf{A}\mathbf{v}.$$

### PROBLEM SET 4.3

#### 1–9 GENERAL SOLUTION

Find a real general solution of the following systems. (Show the details.)

1.  $y_1' = 3y_2$   
 $y_2' = 12y_1$
2.  $y_1' = 5y_2$   
 $y_2' = 5y_1$
3.  $y_1' = y_1 + y_2$   
 $y_2' = y_1 + y_2$
4.  $y_1' = 9y_1 + 13.5y_2$   
 $y_2' = 1.5y_1 + 9y_2$
5.  $y_1' = 4y_2$   
 $y_2' = -4y_1$
6.  $y_1' = 2y_1 - 2y_2$   
 $y_2' = 2y_1 + 2y_2$
7.  $y_1' = 2y_1 + 8y_2 - 4y_3$   
 $y_2' = -4y_1 - 10y_2 + 2y_3$   
 $y_3' = -4y_1 - 4y_2 - 4y_3$
8.  $y_1' = 8y_1 - y_2$   
 $y_2' = y_1 + 10y_2$
9.  $y_1' = -y_1 + y_2 + 0.4y_3$   
 $y_2' = y_1 - 0.1y_2 + 1.4y_3$   
 $y_3' = 0.4y_1 + 1.4y_2 + 0.2y_3$

#### 10–15 INITIAL VALUE PROBLEMS

Solve the following initial value problems. (Show the details.)

10.  $y_1' = y_1 + y_2$   
 $y_2' = 4y_1 + y_2$   
 $y_1(0) = 1, y_2(0) = 6$
11.  $y_1' = y_1 + 2y_2$   
 $y_2' = \frac{1}{2}y_1 + y_2$   
 $y_1(0) = 16, y_2(0) = -2$
12.  $y_1' = 3y_1 + 2y_2$   
 $y_2' = 2y_1 + 3y_2$   
 $y_1(0) = 7, y_2(0) = 7$
13.  $y_1' = \frac{1}{2}y_1 - 2y_2$   
 $y_2' = -\frac{3}{2}y_1 + y_2$   
 $y_1(0) = 0.4, y_2(0) = 3.8$
14.  $y_1' = -y_1 + 5y_2$   
 $y_2' = -y_1 + 3y_2$   
 $y_1(0) = 7, y_2(0) = 2$
15.  $y_1' = 2y_1 + 5y_2$   
 $y_2' = 5y_1 + 12.5y_2$   
 $y_1(0) = 12, y_2(0) = 1$

#### 16–17 CONVERSION

Find a general solution by conversion to a single ODE.

16. The system in Prob. 8.
17. The system in Example 5.
18. (Mixing problem, Fig. 87) Each of the two tanks contains 400 gal of water, in which initially 100 lb (Tank  $T_1$ ) and 40 lb (Tank  $T_2$ ) of fertilizer are dissolved. The inflow, circulation, and outflow are shown in Fig. 87. The mixture is kept uniform by stirring. Find the fertilizer contents  $y_1(t)$  in  $T_1$  and  $y_2(t)$  in  $T_2$ .

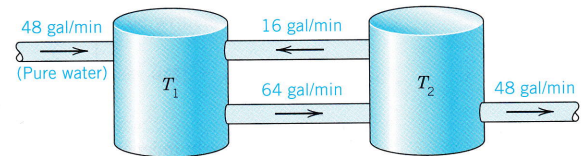


Fig. 87. Tanks in Problem 18

19. (Network) Show that a model for the currents  $I_1(t)$  and  $I_2(t)$  in Fig. 88 is

$$\frac{1}{C} \int I_1 dt + R(I_1 - I_2) = 0, \quad LI_2' + R(I_2 - I_1) = 0.$$

Find a general solution, assuming that  $R = 20 \Omega$ ,  $L = 0.5 \text{ H}$ ,  $C = 2 \cdot 10^{-4} \text{ F}$ .

20. CAS PROJECT. Phase Portraits. Graph some of the figures in this section, in particular Fig. 86 on the degenerate node, in which the vector  $\mathbf{y}^{(2)}$  depends on  $t$ . In each figure highlight a trajectory that satisfies an initial condition of your choice.

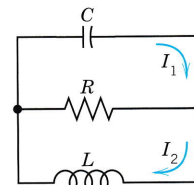


Fig. 88. Network in Problem 19

## 4.4 Criteria for Critical Points. Stability

We continue our discussion of homogeneous linear systems with constant coefficients

$$(1) \mathbf{y}' = \mathbf{A}\mathbf{y} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \mathbf{y}, \quad \text{in components,} \quad \begin{aligned} y_1' &= a_{11}y_1 + a_{12}y_2 \\ y_2' &= a_{21}y_1 + a_{22}y_2. \end{aligned}$$

From the examples in the last section we have seen that we can obtain an overview of families of solution curves if we represent them parametrically as  $\mathbf{y}(t) = [y_1(t) \ y_2(t)]^T$  and graph them as curves in the  $y_1y_2$ -plane, called the **phase plane**. Such a curve is called a **trajectory** of (1), and their totality is known as the **phase portrait** of (1).

Now we have seen that solutions are of the form

$$\mathbf{y}(t) = \mathbf{x}e^{\lambda t}. \quad \text{Substitution into (1) gives} \quad \mathbf{y}'(t) = \lambda \mathbf{x}e^{\lambda t} = \mathbf{A}\mathbf{y} = \mathbf{A}\mathbf{x}e^{\lambda t}.$$

Dropping the common factor  $e^{\lambda t}$ , we have

$$(2) \quad \mathbf{A}\mathbf{x} = \lambda \mathbf{x}.$$

Hence  $\mathbf{y}(t)$  is a (nonzero) solution of (1) if  $\lambda$  is an eigenvalue of  $\mathbf{A}$  and  $\mathbf{x}$  a corresponding eigenvector.

Our examples in the last section show that the general form of the phase portrait is determined to a large extent by the type of **critical point** of the system (1) defined as a point at which  $dy_2/dy_1$  becomes undetermined,  $0/0$ ; here [see (9) in Sec. 4.3]

$$(3) \quad \frac{dy_2}{dy_1} = \frac{y_2' dt}{y_1' dt} = \frac{a_{21}y_1 + a_{22}y_2}{a_{11}y_1 + a_{12}y_2}.$$

We also recall from Sec. 4.3 that there are various types of critical points, and we shall now see how these types are related to the eigenvalues. The latter are solutions  $\lambda = \lambda_1$  and  $\lambda_2$  of the characteristic equation

$$(4) \quad \det(\mathbf{A} - \lambda \mathbf{I}) = \begin{vmatrix} a_{11} - \lambda & a_{12} \\ a_{21} & a_{22} - \lambda \end{vmatrix} = \lambda^2 - (a_{11} + a_{22})\lambda + \det \mathbf{A} = 0.$$

This is a quadratic equation  $\lambda^2 - p\lambda + q = 0$  with coefficients  $p, q$  and discriminant  $\Delta$  given by

$$(5) \quad p = a_{11} + a_{22}, \quad q = \det \mathbf{A} = a_{11}a_{22} - a_{12}a_{21}, \quad \Delta = p^2 - 4q.$$

From calculus we know that the solutions of this equation are

$$(6) \quad \lambda_1 = \frac{1}{2}(p + \sqrt{\Delta}), \quad \lambda_2 = \frac{1}{2}(p - \sqrt{\Delta}).$$

Furthermore, the product representation of the equation gives

$$\lambda^2 - p\lambda + q = (\lambda - \lambda_1)(\lambda - \lambda_2) = \lambda^2 - (\lambda_1 + \lambda_2)\lambda + \lambda_1\lambda_2.$$

Hence  $p$  is the sum and  $q$  the product of the eigenvalues. Also  $\lambda_1 - \lambda_2 = \sqrt{\Delta}$  from (6). Together,

$$(7) \quad p = \lambda_1 + \lambda_2, \quad q = \lambda_1\lambda_2, \quad \Delta = (\lambda_1 - \lambda_2)^2.$$

This gives the criteria in Table 4.1 for classifying critical points. A derivation will be indicated later in this section.

**Table 4.1 Eigenvalue Criteria for Critical Points**  
(Derivation after Table 4.2)

Name	$p = \lambda_1 + \lambda_2$	$q = \lambda_1\lambda_2$	$\Delta = (\lambda_1 - \lambda_2)^2$	Comments on $\lambda_1, \lambda_2$
(a) Node		$q > 0$	$\Delta \geq 0$	Real, same sign
(b) Saddle point		$q < 0$		Real, opposite sign
(c) Center	$p = 0$	$q > 0$		Pure imaginary
(d) Spiral point	$p \neq 0$		$\Delta < 0$	Complex, not pure imaginary

## Stability

Critical points may also be classified in terms of their stability. Stability concepts are basic in engineering and other applications. They are suggested by physics, where **stability** means, roughly speaking, that a small change (a small disturbance) of a physical system at some instant changes the behavior of the system only slightly at all future times  $t$ . For critical points, the following concepts are appropriate.

### DEFINITIONS

#### Stable, Unstable, Stable and Attractive

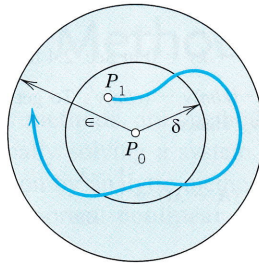
A critical point  $P_0$  of (1) is called **stable**<sup>2</sup> if, roughly, all trajectories of (1) that at some instant are close to  $P_0$  remain close to  $P_0$  at all future times; precisely: if for every disk  $D_\epsilon$  of radius  $\epsilon > 0$  with center  $P_0$  there is a disk  $D_\delta$  of radius  $\delta > 0$  with center  $P_0$  such that every trajectory of (1) that has a point  $P_1$  (corresponding to  $t = t_1$ , say) in  $D_\delta$  has all its points corresponding to  $t \geq t_1$  in  $D_\epsilon$ . See Fig. 89.

$P_0$  is called **unstable** if  $P_0$  is not stable.

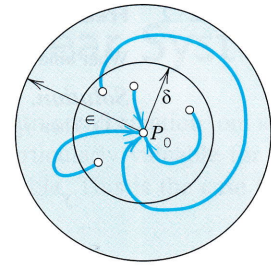
$P_0$  is called **stable and attractive** (or *asymptotically stable*) if  $P_0$  is stable and every trajectory that has a point in  $D_\delta$  approaches  $P_0$  as  $t \rightarrow \infty$ . See Fig. 90.

Classification criteria for critical points in terms of stability are given in Table 4.2. Both tables are summarized in the **stability chart** in Fig. 91. In this chart the region of instability is dark blue.

<sup>2</sup>In the sense of the Russian mathematician ALEXANDER MICHAILOVICH LJAPUNOV (1857–1918), whose work was fundamental in stability theory for ODEs. This is perhaps the most appropriate definition of stability (and the only we shall use), but there are others, too.



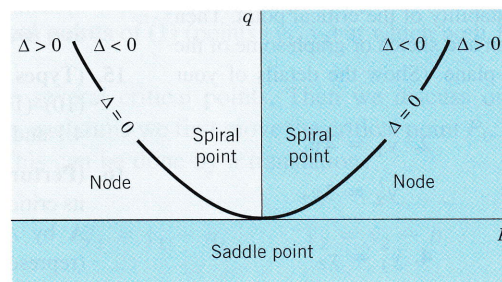
**Fig. 89.** Stable critical point  $P_0$  of (1) (The trajectory initiating at  $P_1$  stays in the disk of radius  $\epsilon$ )



**Fig. 90.** Stable and attractive critical point  $P_0$  of (1)

**Table 4.2 Stability Criteria for Critical Points**

Type of Stability	$p = \lambda_1 + \lambda_2$	$q = \lambda_1\lambda_2$
(a) Stable and attractive	$p < 0$	$q > 0$
(b) Stable	$p \leq 0$	$q > 0$
(c) Unstable	$p > 0$	OR $q < 0$



**Fig. 91.** Stability chart of the system (1) with  $p, q, \Delta$  defined in (5).  
 Stable and attractive: The second quadrant without the  $q$ -axis.  
 Stability also on the positive  $q$ -axis (which corresponds to centers).  
 Unstable: Dark blue region

We indicate how the criteria in Tables 4.1 and 4.2 are obtained. If  $q = \lambda_1\lambda_2 > 0$ , both eigenvalues are positive or both are negative or complex conjugates. If also  $p = \lambda_1 + \lambda_2 < 0$ , both are negative or have a negative real part. Hence  $P_0$  is stable and attractive. The reasoning for the other two lines in Table 4.2 is similar.

If  $\Delta < 0$ , the eigenvalues are complex conjugates, say,  $\lambda_1 = \alpha + i\beta$  and  $\lambda_2 = \alpha - i\beta$ . If also  $p = \lambda_1 + \lambda_2 = 2\alpha < 0$ , this gives a spiral point that is stable and attractive. If  $p = 2\alpha > 0$ , this gives an unstable spiral point.

If  $p = 0$ , then  $\lambda_2 = -\lambda_1$  and  $q = \lambda_1\lambda_2 = -\lambda_1^2$ . If also  $q > 0$ , then  $\lambda_1^2 = -q < 0$ , so that  $\lambda_1$ , and thus  $\lambda_2$ , must be pure imaginary. This gives periodic solutions, their trajectories being closed curves around  $P_0$ , which is a center.

**EXAMPLE 1 Application of the Criteria in Tables 4.1 and 4.2**

In Example 1, Sec. 4.3, we have  $\mathbf{y}' = \begin{bmatrix} -3 & 1 \\ 1 & -3 \end{bmatrix} \mathbf{y}$ ,  $p = -6$ ,  $q = 8$ ,  $\Delta = 4$ , a node by Table 4.1(a), which is stable and attractive by Table 4.2(a). ■

**EXAMPLE 2 Free Motions of a Mass on a Spring**

What kind of critical point does  $my'' + cy' + ky = 0$  in Sec. 2.4 have?

**Solution.** Division by  $m$  gives  $y'' = -(k/m)y - (c/m)y'$ . To get a system, set  $y_1 = y$ ,  $y_2 = y'$  (see Sec. 4.1). Then  $y_2' = y'' = -(k/m)y_1 - (c/m)y_2$ . Hence

$$y' = \begin{bmatrix} 0 & 1 \\ -k/m & -c/m \end{bmatrix} y, \quad \det(\mathbf{A} - \lambda\mathbf{I}) = \begin{vmatrix} -\lambda & 1 \\ -k/m & -c/m - \lambda \end{vmatrix} = \lambda^2 + \frac{c}{m}\lambda + \frac{k}{m} = 0.$$

We see that  $p = -c/m$ ,  $q = k/m$ ,  $\Delta = (c/m)^2 - 4k/m$ . From this and Tables 4.1 and 4.2 we obtain the following results. Note that in the last three cases the discriminant  $\Delta$  plays an essential role.

*No damping.*  $c = 0$ ,  $p = 0$ ,  $q > 0$ , a center.

*Underdamping.*  $c^2 < 4mk$ ,  $p < 0$ ,  $q > 0$ ,  $\Delta < 0$ , a stable and attractive spiral point.

*Critical damping.*  $c^2 = 4mk$ ,  $p < 0$ ,  $q > 0$ ,  $\Delta = 0$ , a stable and attractive node.

*Overdamping.*  $c^2 > 4mk$ ,  $p < 0$ ,  $q > 0$ ,  $\Delta > 0$ , a stable and attractive node. ■

**PROBLEM SET 4.4****1-9 TYPE AND STABILITY OF CRITICAL POINT**

Determine the type and stability of the critical point. Then find a real general solution and sketch or graph some of the trajectories in the phase plane. (Show the details of your work.)

- |                         |                         |
|-------------------------|-------------------------|
| 1. $y_1' = 2y_2$        | 2. $y_1' = 4y_1$        |
| $y_2' = 8y_1$           | $y_2' = 3y_2$           |
| 3. $y_1' = 2y_1 + y_2$  | 4. $y_1' = y_2$         |
| $y_2' = y_1 + 2y_2$     | $y_2' = -5y_1 - 2y_2$   |
| 5. $y_1' = -4y_1 + y_2$ | 6. $y_1' = y_1 + 10y_2$ |
| $y_2' = y_1 - 4y_2$     | $y_2' = 7y_1 - 8y_2$    |
| 7. $y_1' = -2y_2$       | 8. $y_1' = 3y_1 + 5y_2$ |
| $y_2' = 8y_1$           | $y_2' = -5y_1 - 3y_2$   |
| 9. $y_1' = y_1 + 2y_2$  |                         |
| $y_2' = 2y_1 + y_2$     |                         |

**10-12 FORM OF TRAJECTORIES**

What kind of curves are the trajectories of the following ODEs in the phase plane?

10.  $y'' + 5y' = 0$   
 11.  $y'' - k^2y = 0$   
 12.  $y'' + \frac{1}{16}y = 0$
13. (**Damped oscillation**) Solve  $y'' + 4y' + 5y = 0$ . What kind of curves do you get as trajectories?

14. (**Transformation of variable**) What happens to the system (1) and its critical point if you introduce  $\tau = -t$  as a new independent variable?
15. (**Types of critical points**) Discuss the critical points in (10)–(14) in Sec. 4.3 by applying the criteria in Tables 4.1 and 4.2 in this section.
16. (**Perturbation of center**) If a system has a center as its critical point, what happens if you replace the matrix  $\mathbf{A}$  by  $\tilde{\mathbf{A}} = \mathbf{A} + k\mathbf{I}$  with any real number  $k \neq 0$  (representing measurement errors in the diagonal entries)?
17. (**Perturbation**) The system in Example 4 in Sec. 4.3 has a center as its critical point. Replace each  $a_{jk}$  in Example 4, Sec. 4.3, by  $a_{jk} + b$ . Find values of  $b$  such that you get (a) a saddle point, (b) a stable and attractive node, (c) a stable and attractive spiral, (d) an unstable spiral, (e) an unstable node.
18. **CAS EXPERIMENT. Phase Portraits.** Graph phase portraits for the systems in Prob. 17 with the values of  $b$  suggested in the answer. Try to illustrate how the phase portrait changes “continuously” under a continuous change of  $b$ .
19. **WRITING EXPERIMENT. Stability.** Stability concepts are basic in physics and engineering. Write a two-part report of 3 pages each (A) on general applications in which stability plays a role (be as precise as you can), and (B) on material related to stability in this section. Use your own formulations and examples; do not copy.
20. (**Stability chart**) Locate the critical points of the systems (10)–(14) in Sec. 4.3 and of Probs. 1, 3, 5 in this problem set on the stability chart.

## 4.5 Qualitative Methods for Nonlinear Systems

**Qualitative methods** are methods of obtaining qualitative information on solutions without actually solving a system. These methods are particularly valuable for systems whose solution by analytic methods is difficult or impossible. This is the case for many practically important **nonlinear systems**

$$(1) \quad \mathbf{y}' = \mathbf{f}(\mathbf{y}), \quad \text{thus} \quad \begin{aligned} y_1' &= f_1(y_1, y_2) \\ y_2' &= f_2(y_1, y_2). \end{aligned}$$

In this section we extend **phase plane methods**, as just discussed, from linear systems to nonlinear systems (1). We assume that (1) is **autonomous**, that is, the independent variable  $t$  does not occur explicitly. (All examples in the last section are autonomous.) We shall again exhibit entire families of solutions. This is an advantage over numeric methods, which give only one (approximate) solution at a time.

Concepts needed from the last section are the **phase plane** (the  $y_1y_2$ -plane), **trajectories** (solution curves of (1) in the phase plane), the **phase portrait** of (1) (the totality of these trajectories), and **critical points** of (1) (points  $(y_1, y_2)$  at which both  $f_1(y_1, y_2)$  and  $f_2(y_1, y_2)$  are zero).

Now (1) may have several critical points. Then we discuss one after another. As a technical convenience, each time we first move the critical point  $P_0: (a, b)$  to be considered to the origin  $(0, 0)$ . This can be done by a translation

$$\tilde{y}_1 = y_1 - a, \quad \tilde{y}_2 = y_2 - b$$

which moves  $P_0$  to  $(0, 0)$ . Thus we can assume  $P_0$  to be the origin  $(0, 0)$ , and for simplicity we continue to write  $y_1, y_2$  (instead of  $\tilde{y}_1, \tilde{y}_2$ ). We also assume that  $P_0$  is **isolated**, that is, it is the only critical point of (1) within a (sufficiently small) disk with center at the origin. If (1) has only finitely many critical points, this is automatically true. (Explain!)

### Linearization of Nonlinear Systems

How can we determine the kind and stability property of a critical point  $P_0: (0, 0)$  of (1)? In most cases this can be done by **linearization** of (1) near  $P_0$ , writing (1) as  $\mathbf{y}' = \mathbf{f}(\mathbf{y}) = \mathbf{A}\mathbf{y} + \mathbf{h}(\mathbf{y})$  and dropping  $\mathbf{h}(\mathbf{y})$ , as follows.

Since  $P_0$  is critical,  $f_1(0, 0) = 0, f_2(0, 0) = 0$ , so that  $f_1$  and  $f_2$  have no constant terms and we can write

$$(2) \quad \mathbf{y}' = \mathbf{A}\mathbf{y} + \mathbf{h}(\mathbf{y}), \quad \text{thus} \quad \begin{aligned} y_1' &= a_{11}y_1 + a_{12}y_2 + h_1(y_1, y_2) \\ y_2' &= a_{21}y_1 + a_{22}y_2 + h_2(y_1, y_2). \end{aligned}$$

$\mathbf{A}$  is constant (independent of  $t$ ) since (1) is autonomous. One can prove the following (proof in Ref. [A7], pp. 375–388, listed in App. 1).



## THEOREM 1

## Linearization

If  $f_1$  and  $f_2$  in (1) are continuous and have continuous partial derivatives in a neighborhood of the critical point  $P_0: (0, 0)$ , and if  $\det \mathbf{A} \neq 0$  in (2), then the kind and stability of the critical point of (1) are the same as those of the **linearized system**

$$(3) \quad \mathbf{y}' = \mathbf{A}\mathbf{y}, \quad \text{thus} \quad \begin{aligned} y_1' &= a_{11}y_1 + a_{12}y_2 \\ y_2' &= a_{21}y_1 + a_{22}y_2. \end{aligned}$$

Exceptions occur if  $\mathbf{A}$  has equal or pure imaginary eigenvalues; then (1) may have the same kind of critical point as (3) or a spiral point.

## EXAMPLE 1

## Free Undamped Pendulum. Linearization

Figure 92a shows a pendulum consisting of a body of mass  $m$  (the bob) and a rod of length  $L$ . Determine the locations and types of the critical points. Assume that the mass of the rod and air resistance are negligible.

**Solution.** *Step 1. Setting up the mathematical model.* Let  $\theta$  denote the angular displacement, measured counterclockwise from the equilibrium position. The weight of the bob is  $mg$  ( $g$  the acceleration of gravity). It causes a restoring force  $mg \sin \theta$  tangent to the curve of motion (circular arc) of the bob. By Newton's second law, at each instant this force is balanced by the force of acceleration  $mL\theta''$ , where  $L\theta''$  is the acceleration; hence the resultant of these two forces is zero, and we obtain as the mathematical model

$$mL\theta'' + mg \sin \theta = 0.$$

Dividing this by  $mL$ , we have

$$(4) \quad \theta'' + k \sin \theta = 0 \quad \left( k = \frac{g}{L} \right).$$

When  $\theta$  is very small, we can approximate  $\sin \theta$  rather accurately by  $\theta$  and obtain as an *approximate* solution  $A \cos \sqrt{k}t + B \sin \sqrt{k}t$ , but the *exact* solution for any  $\theta$  is not an elementary function.

*Step 2. Critical points  $(0, 0), \pm(2\pi, 0), \pm(4\pi, 0), \dots$ , Linearization.* To obtain a system of ODEs, we set  $\theta = y_1, \theta' = y_2$ . Then from (4) we obtain a nonlinear system (1) of the form

$$(4^*) \quad \begin{aligned} y_1' &= f_1(y_1, y_2) = y_2 \\ y_2' &= f_2(y_1, y_2) = -k \sin y_1. \end{aligned}$$

The right sides are both zero when  $y_2 = 0$  and  $\sin y_1 = 0$ . This gives infinitely many critical points  $(n\pi, 0)$ , where  $n = 0, \pm 1, \pm 2, \dots$ . We consider  $(0, 0)$ . Since the Maclaurin series is

$$\sin y_1 = y_1 - \frac{1}{6}y_1^3 + \dots \approx y_1,$$

the linearized system at  $(0, 0)$  is

$$\mathbf{y}' = \mathbf{A}\mathbf{y} = \begin{bmatrix} 0 & 1 \\ -k & 0 \end{bmatrix} \mathbf{y}, \quad \text{thus} \quad \begin{aligned} y_1' &= y_2 \\ y_2' &= -ky_1. \end{aligned}$$

To apply our criteria in Sec. 4.4 we calculate  $p = a_{11} + a_{22} = 0$ ,  $q = \det \mathbf{A} = k = g/L (> 0)$ , and  $\Delta = p^2 - 4q = -4k$ . From this and Table 4.1(c) in Sec. 4.4 we conclude that  $(0, 0)$  is a center, which is always stable. Since  $\sin \theta = \sin y_1$  is periodic with period  $2\pi$ , the critical points  $(n\pi, 0)$ ,  $n = \pm 2, \pm 4, \dots$ , are all centers.

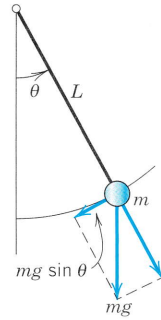
*Step 3. Critical points  $\pm(\pi, 0), \pm(3\pi, 0), \pm(5\pi, 0), \dots$ , Linearization.* We now consider the critical point  $(\pi, 0)$ , setting  $\theta - \pi = y_1$  and  $(\theta - \pi)' = \theta' = y_2$ . Then in (4),

$$\sin \theta = \sin(y_1 + \pi) = -\sin y_1 = -y_1 + \frac{1}{6}y_1^3 - \dots \approx -y_1$$

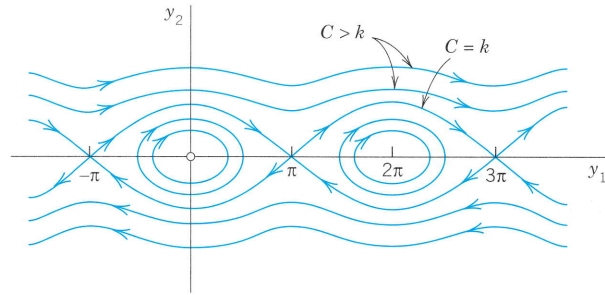
and the linearized system at  $(\pi, 0)$  is now

$$\mathbf{y}' = \mathbf{A}\mathbf{y} = \begin{bmatrix} 0 & 1 \\ k & 0 \end{bmatrix} \mathbf{y}, \quad \text{thus} \quad \begin{aligned} y_1' &= y_2 \\ y_2' &= ky_1. \end{aligned}$$

We see that  $p = 0$ ,  $q = -k (< 0)$ , and  $\Delta = -4q = 4k$ . Hence, by Table 4.1(b), this gives a saddle point, which is always unstable. Because of periodicity, the critical points  $(n\pi, 0)$ ,  $n = \pm 1, \pm 3, \dots$ , are all saddle points. These results agree with the impression we get from Fig. 92b. ■



(a) Pendulum



(b) Solution curves  $y_2(y_1)$  of (4) in the phase plane

Fig. 92. Example 1 ( $C$  will be explained in Example 4.)

**EXAMPLE 2 Linearization of the Damped Pendulum Equation**

To gain further experience in investigating critical points, as another practically important case, let us see how Example 1 changes when we add a damping term  $c\theta'$  (damping proportional to the angular velocity) to equation (4), so that it becomes

$$(5) \quad \theta'' + c\theta' + k \sin \theta = 0$$

where  $k > 0$  and  $c \geq 0$  (which includes our previous case of no damping,  $c = 0$ ). Setting  $\theta = y_1$ ,  $\theta' = y_2$ , as before, we obtain the nonlinear system (use  $\theta'' = y_2'$ )

$$\begin{aligned} y_1' &= y_2 \\ y_2' &= -k \sin y_1 - cy_2. \end{aligned}$$

We see that the critical points have the same locations as before, namely,  $(0, 0)$ ,  $(\pm\pi, 0)$ ,  $(\pm 2\pi, 0)$ ,  $\dots$ . We consider  $(0, 0)$ . Linearizing  $\sin y_1 \approx y_1$  as in Example 1, we get the linearized system at  $(0, 0)$

$$(6) \quad \mathbf{y}' = \mathbf{A}\mathbf{y} = \begin{bmatrix} 0 & 1 \\ -k & -c \end{bmatrix} \mathbf{y}, \quad \text{thus} \quad \begin{aligned} y_1' &= y_2 \\ y_2' &= -ky_1 - cy_2. \end{aligned}$$

This is identical with the system in Example 2 of Sec 4.4, except for the (positive!) factor  $m$  (and except for the physical meaning of  $y_1$ ). Hence for  $c = 0$  (no damping) we have a center (see Fig. 92b), for small damping we have a spiral point (see Fig. 93), and so on.

We now consider the critical point  $(\pi, 0)$ . We set  $\theta - \pi = y_1$ ,  $(\theta - \pi)' = \theta' = y_2$  and linearize

$$\sin \theta = \sin (y_1 + \pi) = -\sin y_1 \approx -y_1.$$

This gives the new linearized system at  $(\pi, 0)$

$$(6^*) \quad \mathbf{y}' = \mathbf{A}\mathbf{y} = \begin{bmatrix} 0 & 1 \\ k & -c \end{bmatrix} \mathbf{y}, \quad \text{thus} \quad \begin{aligned} y_1' &= y_2 \\ y_2' &= ky_1 - cy_2. \end{aligned}$$

For our criteria in Sec 4.4 we calculate  $p = a_{11} + a_{22} = -c$ ,  $q = \det \mathbf{A} = -k$ , and  $\Delta = p^2 - 4q = c^2 + 4k$ . This gives the following results for the critical point at  $(\pi, 0)$ .

*No damping.*  $c = 0$ ,  $p = 0$ ,  $q < 0$ ,  $\Delta > 0$ , a saddle point. See Fig. 92b.

*Damping.*  $c > 0$ ,  $p < 0$ ,  $q < 0$ ,  $\Delta > 0$ , a saddle point. See Fig. 93.

Since  $\sin y_1$  is periodic with period  $2\pi$ , the critical points  $(\pm 2\pi, 0)$ ,  $(\pm 4\pi, 0)$ ,  $\dots$  are of the same type as  $(0, 0)$ , and the critical points  $(-\pi, 0)$ ,  $(\pm 3\pi, 0)$ ,  $\dots$  are of the same type as  $(\pi, 0)$ , so that our task is finished.

Figure 93 shows the trajectories in the case of damping. What we see agrees with our physical intuition. Indeed, damping means loss of energy. Hence instead of the closed trajectories of periodic solutions in Fig. 92b we now have trajectories spiraling around one of the critical points  $(0, 0)$ ,  $(\pm 2\pi, 0)$ ,  $\dots$ . Even the wavy trajectories corresponding to whirly motions eventually spiral around one of these points. Furthermore, there are no more trajectories that connect critical points (as there were in the undamped case for the saddle points). ■

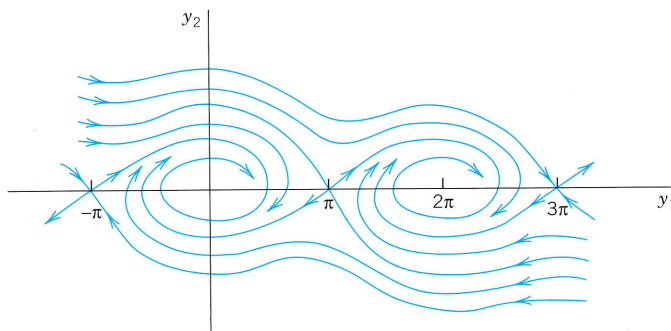


Fig. 93. Trajectories in the phase plane for the damped pendulum in Example 2

## Lotka–Volterra Population Model

### EXAMPLE 3 Predator–Prey Population Model<sup>3</sup>

This model concerns two species, say, rabbits and foxes, and the foxes prey on the rabbits.

**Step 1. Setting up the model.** We assume the following.

1. Rabbits have unlimited food supply. Hence if there were no foxes, their number  $y_1(t)$  would grow exponentially,  $y_1' = ay_1$ .
2. Actually,  $y_1$  is decreased because of the kill by foxes, say, at a rate proportional to  $y_1y_2$ , where  $y_2(t)$  is the number of foxes. Hence  $y_1' = ay_1 - by_1y_2$ , where  $a > 0$  and  $b > 0$ .
3. If there were no rabbits, then  $y_2(t)$  would exponentially decrease to zero,  $y_2' = -ly_2$ . However,  $y_2$  is increased by a rate proportional to the number of encounters between predator and prey; together we have  $y_2' = -ly_2 + ky_1y_2$ , where  $k > 0$  and  $l > 0$ .

This gives the (nonlinear!) Lotka–Volterra system

$$(7) \quad \begin{aligned} y_1' &= f_1(y_1, y_2) = ay_1 - by_1y_2 \\ y_2' &= f_2(y_1, y_2) = ky_1y_2 - ly_2. \end{aligned}$$

<sup>3</sup>Introduced by ALFRED J. LOTKA (1880–1949), American biophysicist, and VITO VOLTERRA (1860–1940), Italian mathematician, the initiator of functional analysis (see [GR7] in App. 1).

**Step 2. Critical point (0, 0), Linearization.** We see from (7) that the critical points are the solutions of

$$(7^*) \quad f_1(y_1, y_2) = y_1(a - by_2) = 0, \quad f_2(y_1, y_2) = y_2(ky_1 - l) = 0.$$

The solutions are  $(y_1, y_2) = (0, 0)$  and  $(\frac{l}{k}, \frac{a}{b})$ . We consider  $(0, 0)$ . Dropping  $-by_1y_2$  and  $ky_1y_2$  from (7) gives the linearized system

$$y' = \begin{bmatrix} a & 0 \\ 0 & -l \end{bmatrix} y.$$

Its eigenvalues are  $\lambda_1 = a > 0$  and  $\lambda_2 = -l < 0$ . They have opposite signs, so that we get a saddle point.

**Step 3. Critical point (l/k, a/b), Linearization.** We set  $y_1 = \tilde{y}_1 + l/k, y_2 = \tilde{y}_2 + a/b$ . Then the critical point  $(l/k, a/b)$  corresponds to  $(\tilde{y}_1, \tilde{y}_2) = (0, 0)$ . Since  $\tilde{y}'_1 = y'_1, \tilde{y}'_2 = y'_2$ , we obtain from (7) [factorized as in (8)]

$$\begin{aligned} \tilde{y}'_1 &= \left(\tilde{y}_1 + \frac{l}{k}\right) \left[ a - b\left(\tilde{y}_2 + \frac{a}{b}\right) \right] = \left(\tilde{y}_1 + \frac{l}{k}\right) (-b\tilde{y}_2) \\ \tilde{y}'_2 &= \left(\tilde{y}_2 + \frac{a}{b}\right) \left[ k\left(\tilde{y}_1 + \frac{l}{k}\right) - l \right] = \left(\tilde{y}_2 + \frac{a}{b}\right) k\tilde{y}_1. \end{aligned}$$

Dropping the two nonlinear terms  $-b\tilde{y}_1\tilde{y}_2$  and  $k\tilde{y}_1\tilde{y}_2$ , we have the linearized system

$$(7^{**}) \quad \begin{aligned} (a) \quad \tilde{y}'_1 &= -\frac{lb}{k} \tilde{y}_2 \\ (b) \quad \tilde{y}'_2 &= \frac{ak}{b} \tilde{y}_1. \end{aligned}$$

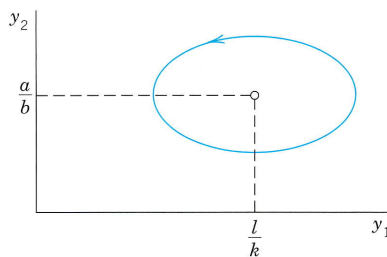
The left side of (a) times the right side of (b) must equal the right side of (a) times the left side of (b),

$$\frac{ak}{b} \tilde{y}_1 \tilde{y}'_1 = -\frac{lb}{k} \tilde{y}_2 \tilde{y}'_2. \quad \text{By integration,} \quad \frac{ak}{b} \tilde{y}_1^2 + \frac{lb}{k} \tilde{y}_2^2 = \text{const.}$$

This is a family ellipses, so that the critical point  $(l/k, a/b)$  of the linearized system (7\*\*) is a center (Fig. 94). It can be shown by a complicated analysis that the nonlinear system (7) also has a center (rather than a spiral point) at  $(l/k, a/b)$  surrounded by closed trajectories (not ellipses).

We see that the predators and prey have a cyclic variation about the critical point. Let us move counterclockwise around the ellipse, beginning at the right vertex, where the rabbits have a maximum number. Foxes are sharply increasing in number until they reach a maximum at the upper vertex, and the number of rabbits is then sharply decreasing until it reaches a minimum at the left vertex, and so on. Cyclic variations of this kind have been observed in nature, for example, for lynx and snowshoe hare near the Hudson Bay, with a cycle of about 10 years.

For models of more complicated situations and a systematic discussion, see C. W. Clark, *Mathematical Bioeconomics* (Wiley, 1976). ■



**Fig. 94.** Ecological equilibrium point and trajectory of the linearized Lotka–Volterra system (7\*\*)

## Transformation to a First-Order Equation in the Phase Plane

Another phase plane method is based on the idea of transforming a second-order **autonomous ODE** (an ODE in which  $t$  does not occur explicitly)

$$F(y, y', y'') = 0$$

to first order by taking  $y = y_1$  as the independent variable, setting  $y' = y_2$  and transforming  $y''$  by the chain rule,

$$y'' = y_2' = \frac{dy_2}{dt} = \frac{dy_2}{dy_1} \frac{dy_1}{dt} = \frac{dy_2}{dy_1} y_2.$$

Then the ODE becomes of first order,

$$(8) \quad F\left(y_1, y_2, \frac{dy_2}{dy_1} y_2\right) = 0$$

and can sometimes be solved or treated by direction fields. We illustrate this for the equation in Example 1 and shall gain much more insight into the behavior of solutions.

### EXAMPLE 4 An ODE (8) for the Free Undamped Pendulum

If in (4)  $\theta'' + k \sin \theta = 0$  we set  $\theta = y_1$ ,  $\theta' = y_2$  (the angular velocity) and use

$$\theta'' = \frac{dy_2}{dt} = \frac{dy_2}{dy_1} \frac{dy_1}{dt} = \frac{dy_2}{dy_1} y_2, \quad \text{we get} \quad \frac{dy_2}{dy_1} y_2 = -k \sin y_1.$$

Separation of variables gives  $y_2 dy_2 = -k \sin y_1 dy_1$ . By integration,

$$(9) \quad \frac{1}{2}y_2^2 = k \cos y_1 + C \quad (C \text{ constant}).$$

Multiplying this by  $mL^2$ , we get

$$\frac{1}{2}m(Ly_2)^2 - mL^2k \cos y_1 = mL^2C.$$

We see that these three terms are **energies**. Indeed,  $y_2$  is the angular velocity, so that  $Ly_2$  is the velocity and the first term is the kinetic energy. The second term (including the minus sign) is the potential energy of the pendulum, and  $mL^2C$  is its total energy, which is constant, as expected from the law of conservation of energy, because there is no damping (no loss of energy). The type of motion depends on the total energy, hence on  $C$ , as follows.

Figure 92b on p. 153 shows trajectories for various values of  $C$ . These graphs continue periodically with period  $2\pi$  to the left and to the right. We see that some of them are ellipse-like and closed, others are wavy, and there are two trajectories (passing through the saddle points  $(n\pi, 0)$ ,  $n = \pm 1, \pm 3, \dots$ ) that separate those two types of trajectories. From (9) we see that the smallest possible  $C$  is  $C = -k$ ; then  $y_2 = 0$ , and  $\cos y_1 = 1$ , so that the pendulum is at rest. The pendulum will change its direction of motion if there are points at which  $y_2 = \theta' = 0$ . Then  $k \cos y_1 + C = 0$  by (9). If  $y_1 = \pi$ , then  $\cos y_1 = -1$  and  $C = k$ . Hence if  $-k < C < k$ , then the pendulum reverses its direction for a  $|y_1| = |\theta| < \pi$ , and for these values of  $C$  with  $|C| < k$  the pendulum oscillates. This corresponds to the closed trajectories in the figure. However, if  $C > k$ , then  $y_2 = 0$  is impossible and the pendulum makes a whirly motion that appears as a wavy trajectory in the  $y_1y_2$ -plane. Finally, the value  $C = k$  corresponds to the two "separating trajectories" in Fig. 92b connecting the saddle points. ■

The phase plane method of deriving a single first-order equation (8) may be of practical interest not only when (8) can be solved (as in Example 4) but also when solution is not possible and we have to utilize direction fields (Sec. 1.2). We illustrate this with a very famous example:

**EXAMPLE 5 Self-Sustained Oscillations. Van der Pol Equation**

There are physical systems such that for small oscillations, energy is fed into the system, whereas for large oscillations, energy is taken from the system. In other words, large oscillations will be damped, whereas for small oscillations there is “negative damping” (feeding of energy into the system). For physical reasons we expect such a system to approach a periodic behavior, which will thus appear as a closed trajectory in the phase plane, called a **limit cycle**. A differential equation describing such vibrations is the famous **van der Pol equation**<sup>4</sup>

$$(10) \quad y'' - \mu(1 - y^2)y' + y = 0 \quad (\mu > 0, \text{ constant}).$$

It first occurred in the study of electrical circuits containing vacuum tubes. For  $\mu = 0$  this equation becomes  $y'' + y = 0$  and we obtain harmonic oscillations. Let  $\mu > 0$ . The damping term has the factor  $-\mu(1 - y^2)$ . This is negative for small oscillations, when  $y^2 < 1$ , so that we have “negative damping,” is zero for  $y^2 = 1$  (no damping), and is positive if  $y^2 > 1$  (positive damping, loss of energy). If  $\mu$  is small, we expect a limit cycle that is almost a circle because then our equation differs but little from  $y'' + y = 0$ . If  $\mu$  is large, the limit cycle will probably look different.

Setting  $y = y_1, y' = y_2$  and using  $y'' = (dy_2/dy_1)y_2$  as in (8), we have from (10)

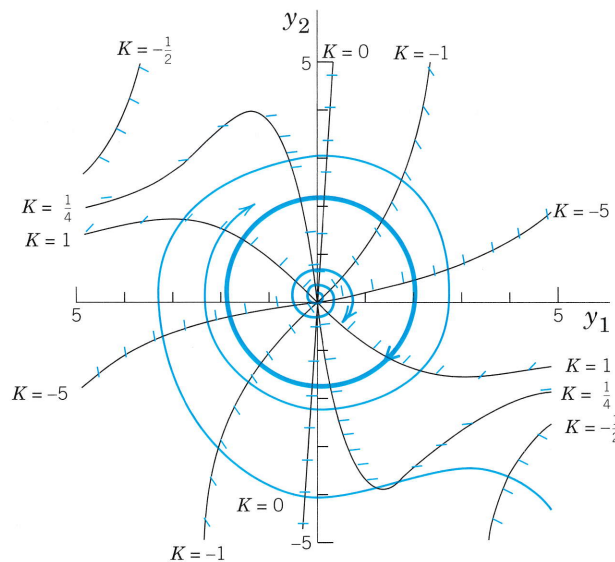
$$(11) \quad \frac{dy_2}{dy_1} y_2 - \mu(1 - y_1^2)y_2 + y_1 = 0.$$

The isoclines in the  $y_1y_2$ -plane (the phase plane) are the curves  $dy_2/dy_1 = K = \text{const}$ , that is,

$$\frac{dy_2}{dy_1} = \mu(1 - y_1^2) - \frac{y_1}{y_2} = K.$$

Solving algebraically for  $y_2$ , we see that the isoclines are given by

$$y_2 = \frac{y_1}{\mu(1 - y_1^2) - K} \quad (\text{Figs. 95, 96}).$$



**Fig. 95.** Direction field for the van der Pol equation with  $\mu = 0.1$  in the phase plane, showing also the limit cycle and two trajectories. See also Fig. 8 in Sec. 1.2.

<sup>4</sup>BALTHASAR VAN DER POL (1889–1959), Dutch physicist and engineer.

Figure 95 shows some isoclines when  $\mu$  is small,  $\mu = 0.1$ , the limit cycle (almost a circle), and two (blue) trajectories approaching it, one from the outside and the other from the inside, of which only the initial portion, a small spiral, is shown. Due to this approach by trajectories, a limit cycle differs conceptually from a closed curve (a trajectory) surrounding a center, which is not approached by trajectories. For larger  $\mu$  the limit cycle no longer resembles a circle, and the trajectories approach it more rapidly than for smaller  $\mu$ . Figure 96 illustrates this for  $\mu = 1$ .

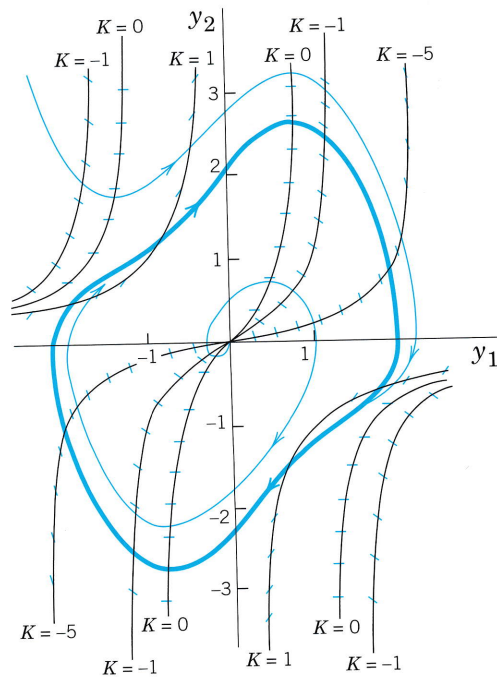


Fig. 96. Direction field for the van der Pol equation with  $\mu = 1$  in the phase plane, showing also the limit cycle and two trajectories approaching it

## PROBLEM SET 4.5

### 1-12 CRITICAL POINTS, LINEARIZATION

Determine the location and type of all critical points by linearization. In Probs. 7-12 first transform the ODE to a system. (Show the details of your work.)

1.  $y_1' = y_2 + y_2^2$       2.  $y_1' = 4y_1 - y_1^2$   
 $y_2' = 3y_1$                        $y_2' = y_2$
3.  $y_1' = 4y_2$               4.  $y_1' = -3y_1 + y_2 - y_2^2$   
 $y_2' = 2y_1 - y_1^2$                $y_2' = y_1 - 3y_2$
5.  $y_1' = -y_1 + y_2 - y_2^2$     6.  $y_1' = y_2 - y_2^2$   
 $y_2' = -y_1 - y_2$                $y_2' = y_1 - y_1^2$
7.  $y'' + y - 4y^2 = 0$       8.  $y'' + 9y + y^2 = 0$

9.  $y'' + \cos y = 0$       10.  $y'' + \sin y = 0$
11.  $y'' + 4y - y^3 = 0$     12.  $y'' + y' + 2y - y^2 = 0$
13. (Trajectories) What kind of curves are the trajectories of  $yy'' + 2y'^2 = 0$ ?
14. (Trajectories) Write the ODE  $y'' - 4y + y^3 = 0$  as a system, solve it for  $y_2$  as a function of  $y_1$ , and sketch or graph some of the trajectories in the phase plane.
15. (Trajectories) What is the radius of a real general solution of  $y'' + y = 0$  in the phase plane?
16. (Trajectories) In Prob. 14 add a linear damping term to get  $y'' + 2y' - 4y + y^3 = 0$ . Using arguments from mechanics and a comparison with Prob. 14, as well as with Examples 1 and 2, guess the type of each critical point. Then determine these types by linearization. (Show all details of your work.)

17. **(Pendulum)** To what state (position, speed, direction of motion) do the four points of intersection of a closed trajectory with the axes in Fig. 92b correspond? The point of intersection of a wavy curve with the  $y_2$ -axis?
18. **(Limit cycle)** What is the essential difference between a limit cycle and a closed trajectory surrounding a center?
19. **CAS EXPERIMENT. Deformation of Limit Cycle.** Convert the van der Pol equation to a system. Graph the limit cycle and some approaching trajectories for  $\mu = 0.2, 0.4, 0.6, 0.8, 1.0, 1.5, 2.0$ . Try to observe how the limit cycle changes its form continuously if you vary  $\mu$  continuously. Describe in words how the limit cycle is deformed with growing  $\mu$ .
20. **TEAM PROJECT. Self-sustained oscillations.**  
**(a) Van der Pol Equation.** Determine the type of the critical point at  $(0, 0)$  when  $\mu > 0$ ,  $\mu = 0$ ,  $\mu < 0$ .

Show that if  $\mu \rightarrow 0$ , the isoclines approach straight lines through the origin. Why is this to be expected?

**(b) Rayleigh equation.** Show that the so-called Rayleigh equation<sup>5</sup>

$$Y'' - \mu(1 - \frac{1}{3}Y'^2)Y' + Y = 0 \quad (\mu > 0)$$

also describes self-sustained oscillations and that by differentiating it and setting  $y = Y'$  one obtains the van der Pol equation.

**(c) Duffing equation.** The Duffing equation is

$$y'' + \omega_0^2 y + \beta y^3 = 0$$

where usually  $|\beta|$  is small, thus characterizing a small deviation of the restoring force from linearity.  $\beta > 0$  and  $\beta < 0$  are called the cases of a *hard spring* and a *soft spring*, respectively. Find the equation of the trajectories in the phase plane. (Note that for  $\beta > 0$  all these curves are closed.)

## 4.6 Nonhomogeneous Linear Systems of ODEs

In this last section of Chap. 4 we discuss methods for solving nonhomogeneous linear systems of ODEs

$$(1) \quad \mathbf{y}' = \mathbf{A}\mathbf{y} + \mathbf{g} \quad (\text{see Sec. 4.2})$$

where the vector  $\mathbf{g}(t)$  is not identically zero. We assume  $\mathbf{g}(t)$  and the entries of the  $n \times n$  matrix  $\mathbf{A}(t)$  to be continuous on some interval  $J$  of the  $t$ -axis. From a general solution  $\mathbf{y}^{(h)}(t)$  of the homogeneous system  $\mathbf{y}' = \mathbf{A}\mathbf{y}$  on  $J$  and a **particular solution**  $\mathbf{y}^{(p)}(t)$  of (1) on  $J$  [i.e., a solution of (1) containing no arbitrary constants], we get a solution of (1),

$$(2) \quad \mathbf{y} = \mathbf{y}^{(h)} + \mathbf{y}^{(p)}.$$

$\mathbf{y}$  is called a **general solution** of (1) on  $J$  because it includes every solution of (1) on  $J$ . This follows from Theorem 2 in Sec. 4.2 (see Prob. 1 of this section).

Having studied homogeneous linear systems in Secs. 4.1–4.4, our present task will be to explain methods for obtaining particular solutions of (1). We discuss the method of undetermined coefficients and the method of the variation of parameters; these have counterparts for a single ODE, as we know from Secs. 2.7 and 2.10.

<sup>5</sup>LORD RAYLEIGH (JOHN WILLIAM STRUTT) (1842–1919), great English physicist and mathematician, professor at Cambridge and London, known by his important contributions to the theory of waves, elasticity theory, hydrodynamics, and various other branches of applied mathematics and theoretical physics. In 1904 he received the Nobel Prize in physics.



## Method of Undetermined Coefficients

As for a single ODE, this method is suitable if the entries of  $\mathbf{A}$  are constants and the components of  $\mathbf{g}$  are constants, positive integer powers of  $t$ , exponential functions, or cosines and sines. In such a case a particular solution  $\mathbf{y}^{(p)}$  is assumed in a form similar to  $\mathbf{g}$ ; for instance,  $\mathbf{y}^{(p)} = \mathbf{u} + \mathbf{v}t + \mathbf{w}t^2$  if  $\mathbf{g}$  has components quadratic in  $t$ , with  $\mathbf{u}, \mathbf{v}, \mathbf{w}$  to be determined by substitution into (1). This is similar to Sec. 2.7, except for the Modification Rule. It suffices to show this by an example.

### EXAMPLE 1 Method of Undetermined Coefficients. Modification Rule

Find a general solution of

$$(3) \quad \mathbf{y}' = \mathbf{A}\mathbf{y} + \mathbf{g} = \begin{bmatrix} -3 & 1 \\ 1 & -3 \end{bmatrix} \mathbf{y} + \begin{bmatrix} -6 \\ 2 \end{bmatrix} e^{-2t}.$$

**Solution.** A general equation of the homogeneous system is (see Example 1 in Sec. 4.3)

$$(4) \quad \mathbf{y}^{(h)} = c_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-2t} + c_2 \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{-4t}.$$

Since  $\lambda = -2$  is an eigenvalue of  $\mathbf{A}$ , the function  $e^{-2t}$  on the right also appears in  $\mathbf{y}^{(h)}$ , and we must apply the Modification Rule by setting

$$\mathbf{y}^{(p)} = \mathbf{u}te^{-2t} + \mathbf{v}e^{-2t} \quad (\text{rather than } \mathbf{u}e^{-2t}).$$

Note that the first of these two terms is the analog of the modification in Sec. 2.7, but it would not be sufficient here. (Try it.) By substitution,

$$\mathbf{y}^{(p)'} = \mathbf{u}e^{-2t} - 2\mathbf{u}te^{-2t} - 2\mathbf{v}e^{-2t} = \mathbf{A}\mathbf{u}te^{-2t} + \mathbf{A}\mathbf{v}e^{-2t} + \mathbf{g}.$$

Equating the  $te^{-2t}$ -terms on both sides, we have  $-2\mathbf{u} = \mathbf{A}\mathbf{u}$ . Hence  $\mathbf{u}$  is an eigenvector of  $\mathbf{A}$  corresponding to  $\lambda = -2$ ; thus [see (5)]  $\mathbf{u} = a[1 \ 1]^T$  with any  $a \neq 0$ . Equating the other terms gives

$$\mathbf{u} - 2\mathbf{v} = \mathbf{A}\mathbf{v} + \begin{bmatrix} -6 \\ 2 \end{bmatrix} \quad \text{thus} \quad \begin{bmatrix} a \\ a \end{bmatrix} - \begin{bmatrix} 2v_1 \\ 2v_2 \end{bmatrix} = \begin{bmatrix} -3v_1 + v_2 \\ v_1 - 3v_2 \end{bmatrix} + \begin{bmatrix} -6 \\ 2 \end{bmatrix}.$$

Collecting terms and reshuffling gives

$$v_1 - v_2 = -a - 6$$

$$-v_1 + v_2 = -a + 2.$$

By addition,  $0 = -2a - 4$ ,  $a = -2$ , and then  $v_2 = v_1 + 4$ , say,  $v_1 = k$ ,  $v_2 = k + 4$ , thus,  $\mathbf{v} = [k \ k + 4]^T$ . We can simply choose  $k = 0$ . This gives the *answer*

$$(5) \quad \mathbf{y} = \mathbf{y}^{(h)} + \mathbf{y}^{(p)} = c_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-2t} + c_2 \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{-4t} - 2 \begin{bmatrix} 1 \\ 1 \end{bmatrix} te^{-2t} + \begin{bmatrix} 0 \\ 4 \end{bmatrix} e^{-2t}.$$

For other  $k$  we get other  $\mathbf{v}$ ; for instance,  $k = -2$  gives  $\mathbf{v} = [-2 \ 2]^T$ , so that the *answer* becomes

$$(5^*) \quad \mathbf{y} = c_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-2t} + c_2 \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{-4t} - 2 \begin{bmatrix} 1 \\ 1 \end{bmatrix} te^{-2t} + \begin{bmatrix} -2 \\ 2 \end{bmatrix} e^{-2t}, \quad \text{etc.} \quad \blacksquare$$

## Method of Variation of Parameters

This method can be applied to nonhomogeneous linear systems

$$(6) \quad \mathbf{y}' = \mathbf{A}(t)\mathbf{y} + \mathbf{g}(t)$$

with variable  $\mathbf{A} = \mathbf{A}(t)$  and general  $\mathbf{g}(t)$ . It yields a particular solution  $\mathbf{y}^{(p)}$  of (6) on some open interval  $J$  on the  $t$ -axis if a general solution of the homogeneous system  $\mathbf{y}' = \mathbf{A}(t)\mathbf{y}$  on  $J$  is known. We explain the method in terms of the previous example.

### EXAMPLE 2 Solution by the Method of Variation of Parameters

Solve (3) in Example 1.

**Solution.** A basis of solutions of the homogeneous system is  $[e^{-2t} \quad e^{-2t}]^T$  and  $[e^{-4t} \quad -e^{-4t}]^T$ . Hence the general solution (4) of the homogeneous system may be written

$$(7) \quad \mathbf{y}^{(h)} = \begin{bmatrix} e^{-2t} & e^{-4t} \\ e^{-2t} & -e^{-4t} \end{bmatrix} \begin{bmatrix} c_1 \\ c_2 \end{bmatrix} = \mathbf{Y}(t)\mathbf{c}.$$

Here,  $\mathbf{Y}(t) = [\mathbf{y}^{(1)} \quad \mathbf{y}^{(2)}]^T$  is the fundamental matrix (see Sec. 4.2). As in Sec. 2.10 we replace the constant vector  $\mathbf{c}$  by a variable vector  $\mathbf{u}(t)$  to obtain a particular solution

$$\mathbf{y}^{(p)} = \mathbf{Y}(t)\mathbf{u}(t).$$

Substitution into (3)  $\mathbf{y}' = \mathbf{A}\mathbf{y} + \mathbf{g}$  gives

$$(8) \quad \mathbf{Y}'\mathbf{u} + \mathbf{Y}\mathbf{u}' = \mathbf{A}\mathbf{Y}\mathbf{u} + \mathbf{g}.$$

Now since  $\mathbf{y}^{(1)}$  and  $\mathbf{y}^{(2)}$  are solutions of the homogeneous system, we have

$$\mathbf{y}^{(1)'} = \mathbf{A}\mathbf{y}^{(1)}, \quad \mathbf{y}^{(2)'} = \mathbf{A}\mathbf{y}^{(2)}, \quad \text{thus} \quad \mathbf{Y}' = \mathbf{A}\mathbf{Y}.$$

Hence  $\mathbf{Y}'\mathbf{u} = \mathbf{A}\mathbf{Y}\mathbf{u}$ , so that (8) reduces to

$$\mathbf{Y}\mathbf{u}' = \mathbf{g}. \quad \text{The solution is} \quad \mathbf{u}' = \mathbf{Y}^{-1}\mathbf{g};$$

here we use that the inverse  $\mathbf{Y}^{-1}$  of  $\mathbf{Y}$  (Sec. 4.0) exists because the determinant of  $\mathbf{Y}$  is the Wronskian  $W$ , which is not zero for a basis. Equation (9) in Sec. 4.0 gives the form of  $\mathbf{Y}^{-1}$ ,

$$\mathbf{Y}^{-1} = \frac{1}{-2e^{-6t}} \begin{bmatrix} -e^{-4t} & -e^{-4t} \\ -e^{-2t} & e^{-2t} \end{bmatrix} = \frac{1}{2} \begin{bmatrix} e^{2t} & e^{2t} \\ e^{4t} & -e^{4t} \end{bmatrix}.$$

We multiply this by  $\mathbf{g}$ , obtaining

$$\mathbf{u}' = \mathbf{Y}^{-1}\mathbf{g} = \frac{1}{2} \begin{bmatrix} e^{2t} & e^{2t} \\ e^{4t} & -e^{4t} \end{bmatrix} \begin{bmatrix} -6e^{-2t} \\ 2e^{-2t} \end{bmatrix} = \frac{1}{2} \begin{bmatrix} -4 \\ -8e^{2t} \end{bmatrix} = \begin{bmatrix} -2 \\ -4e^{2t} \end{bmatrix}.$$

Integration is done componentwise (just as differentiation) and gives

$$\mathbf{u}(t) = \int_0^t \begin{bmatrix} -2 \\ -4e^{2\tilde{t}} \end{bmatrix} d\tilde{t} = \begin{bmatrix} -2t \\ -2e^{2t} + 2 \end{bmatrix}$$

(where  $+2$  comes from the lower limit of integration). From this and  $\mathbf{Y}$  in (7) we obtain

$$\mathbf{Y}\mathbf{u} = \begin{bmatrix} e^{-2t} & e^{-4t} \\ e^{-2t} & -e^{-4t} \end{bmatrix} \begin{bmatrix} -2t \\ -2e^{2t} + 2 \end{bmatrix} = \begin{bmatrix} -2te^{-2t} - 2e^{-2t} + 2e^{-4t} \\ -2te^{-2t} + 2e^{-2t} - 2e^{-4t} \end{bmatrix} = \begin{bmatrix} -2t - 2 \\ -2t + 2 \end{bmatrix} e^{-2t} + \begin{bmatrix} 2 \\ -2 \end{bmatrix} e^{-4t}.$$

The last term on the right is a solution of the homogeneous system. Hence we can absorb it into  $\mathbf{y}^{(h)}$ . We thus obtain as a general solution of the system (3), in agreement with (5\*),

$$(9) \quad \mathbf{y} = c_1 \begin{bmatrix} 1 \\ 1 \end{bmatrix} e^{-2t} + c_2 \begin{bmatrix} 1 \\ -1 \end{bmatrix} e^{-4t} - 2 \begin{bmatrix} 1 \\ 1 \end{bmatrix} te^{-2t} + \begin{bmatrix} -2 \\ 2 \end{bmatrix} e^{-2t}. \quad \blacksquare$$

## PROBLEM SET 4.6

1. (General solution) Prove that (2) includes every solution of (1).

### 2-9 GENERAL SOLUTION

Find a general solution. (Show the details of your work.)

2.  $y_1' = y_2 + t$

$y_2' = y_1 - 3t$

3.  $y_1' = 4y_2 + 9t$

$y_2' = -4y_1 + 5$

4.  $y_1' = y_1 + y_2 + 5 \cos t$

$y_2' = 3y_1 - y_2 - 5 \sin t$

5.  $y_1' = 2y_1 + 2y_2 + 12$

$y_2' = 5y_1 - y_2 - 30$

6.  $y_1' = -y_1 + y_2 + e^{-2t}$

$y_2' = -y_1 - y_2 - e^{-2t}$

7.  $y_1' = -14y_1 + 10y_2 + 162$

$y_2' = -5y_1 + y_2 - 324t$

8.  $y_1' = 10y_1 - 6y_2 + 10(1 - t - t^2)$

$y_2' = 6y_1 - 10y_2 + 4 - 20t - 6t^2$

9.  $y_1' = -3y_1 - 4y_2 + 11t + 15$

$y_2' = 5y_1 + 6y_2 + 3e^{-t} - 15t - 20$

### 10. CAS EXPERIMENT. Undetermined Coefficients.

Find out experimentally how general you must choose  $\mathbf{y}^{(p)}$ , in particular when the components of  $\mathbf{g}$  have a different form (e.g., as in Prob. 9). Write a short report, covering also the situation in the case of the modification rule.

### 11-16 INITIAL VALUE PROBLEM

Solve (showing details):

11.  $y_1' = -2y_2 + 4t$

$y_2' = 2y_1 - 2t$

$y_1(0) = 4, y_2(0) = \frac{1}{2}$

12.  $y_1' = 4y_2 + 5e^t$

$y_2' = -y_1 - 20e^{-t}$

$y_1(0) = 1, y_2(0) = 0$

13.  $y_1' = y_1 + 2y_2 + e^{2t} - 2t$

$y_2' = -y_2 + 1 + t$

$y_1(0) = 1, y_2(0) = -4$

14.  $y_1' = 3y_1 - 4y_2 + 20 \cos t$

$y_2' = y_1 - 2y_2$

$y_1(0) = 0, y_2(0) = 8$

15.  $y_1' = 4y_2 + 3e^{3t}$

$y_2' = 2y_2 - 15e^{-3t}$

$y_1(0) = 2, y_2(0) = 2$

16.  $y_1' = 4y_1 + 8y_2 + 2 \cos t - 16 \sin t$

$y_2' = 6y_1 + 2y_2 + \cos t - 14 \sin t$

$y_1(0) = 15, y_2(0) = 13$

17. (Network) Find the currents in Fig. 97 when  $R = 2.5 \Omega$ ,  $L = 1 \text{ H}$ ,  $C = 0.04 \text{ F}$ ,  $E(t) = 845 \sin t \text{ V}$ , and  $I_1(0) = 0$ ,  $I_2(0) = 0$ . (Show the details.)

18. (Network) Find the currents in Fig. 97 when  $R = 1 \Omega$ ,  $L = 10 \text{ H}$ ,  $C = 1.25 \text{ F}$ ,  $E(t) = 10 \text{ kV}$ , and  $I_1(0) = 0$ ,  $I_2(0) = 0$ . (Show the details.)

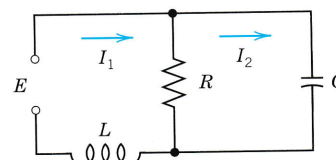


Fig. 97. Network in Probs. 17, 18

19. (Network) Find the currents in Fig. 98 when  $R_1 = 2 \Omega$ ,  $R_2 = 8 \Omega$ ,  $L = 1 \text{ H}$ ,  $C = 0.5 \text{ F}$ ,  $E = 200 \text{ V}$ . (Show the details.)

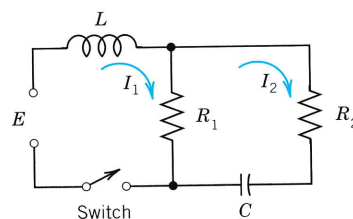


Fig. 98. Network in Prob. 19

### 20. WRITING PROJECT. Undetermined Coefficients.

Write a short report in which you compare the application of the method of undetermined coefficients to a single ODE and to a system of two ODEs, using ODEs and systems of your choice.

## CHAPTER 4 REVIEW QUESTIONS AND PROBLEMS

- State some applications that can be modeled by systems of ODEs.
- What is population dynamics? Give examples.
- How can you transform an ODE into a system of ODEs?
- What are qualitative methods for systems? Why are they important?
- What is the phase plane? The phase plane method? The phase portrait of a system of ODEs?
- What is a critical point of a system of ODEs? How did we classify these points?
- What are eigenvalues? What role did they play in this chapter?
- What does stability mean in general? In connection with critical points?
- What does linearization of a system mean? Give an example.
- What is a limit cycle? When may it occur in mechanics?

**11–19 GENERAL SOLUTION. CRITICAL POINTS**

Find a general solution. Determine the kind and stability of the critical point. (Show the details of your work.)

- $y_1' = 4y_2$   
 $y_2' = 16y_1$
- $y_1' = 9y_1$   
 $y_2' = y_2$
- $y_1' = y_2$   
 $y_2' = 6y_1 - 5y_2$
- $y_1' = 3y_1 - 3y_2$   
 $y_2' = 3y_1 + 3y_2$
- $y_1' = 1.5y_1 - 6y_2$   
 $y_2' = -4.5y_1 + 3y_2$
- $y_1' = -3y_1 - 2y_2$   
 $y_2' = -2y_1 - 3y_2$
- $y_1' = 3y_1 + 2y_2$   
 $y_2' = 2y_1 + 3y_2$
- $y_1' = 3y_1 + 5y_2$   
 $y_2' = -5y_1 - 3y_2$
- $y_1' = -y_1 + 2y_2$   
 $y_2' = -2y_1 - y_2$

**20–25 NONHOMOGENEOUS SYSTEMS**

Find a general solution. (Show the details.)

- $y_1' = 3y_2 + 6t$   
 $y_2' = 12y_1 + 1$
- $y_1' = y_1 + 2y_2 + e^{2t}$   
 $y_2' = -y_2 + 1.5e^{-2t}$
- $y_1' = y_1 + y_2 + \sin t$   
 $y_2' = 4y_1 + y_2$

- $y_1' = 4y_1 + 3y_2 + 2$   
 $y_2' = -6y_1 - 5y_2 + 4e^{-t}$
- $y_1' = y_1 - 2y_2 - \sin t$   
 $y_2' = 3y_1 - 4y_2 - \cos t$
- $y_1' = y_1 + 2y_2 + t^2$   
 $y_2' = 2y_1 + y_2 - t^2$

- (Mixing problem)** Tank  $T_1$  in Fig. 99 contains initially 200 gal of water in which 160 lb of salt are dissolved. Tank  $T_2$  contains initially 100 gal of pure water. Liquid is pumped through the system as indicated, and the mixtures are kept uniform by stirring. Find the amounts of salt  $y_1(t)$  and  $y_2(t)$  in  $T_1$  and  $T_2$ , respectively.

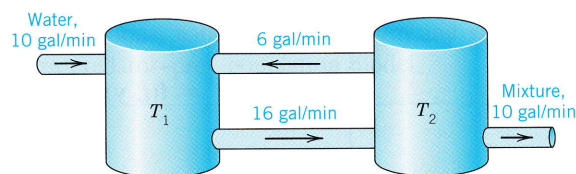


Fig. 99. Tanks in Problem 26

- (Critical point)** What kind of critical point does  $y' = Ay$  have if  $A$  has the eigenvalues  $-6$  and  $1$ ?
- (Network)** Find the currents in Fig. 100, where  $R_1 = 0.5 \Omega$ ,  $R_2 = 0.7 \Omega$ ,  $L_1 = 0.4 \text{ H}$ ,  $L_2 = 0.5 \text{ H}$ ,  $E = 1 \text{ kV} = 1000 \text{ V}$ , and  $I_1(0) = 0$ ,  $I_2(0) = 0$ .

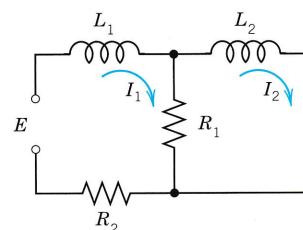


Fig. 100. Network in Problem 28

- (Network)** Find the currents in Fig. 101 when  $R = 10 \Omega$ ,  $L = 1.25 \text{ H}$ ,  $C = 0.002 \text{ F}$ , and  $I_1(0) = I_2(0) = 3 \text{ A}$ .

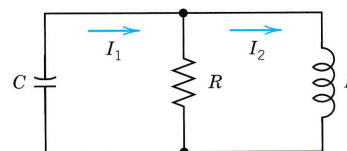


Fig. 101. Network in Problem 29

**30–33** LINEARIZATION

Determine the location and kind of all critical points of the given nonlinear system by linearization.

30.  $y_1' = y_2$

$y_2' = 4y_1 - y_1^3$

31.  $y_1' = -9y_2$

$y_2' = \sin y_1$

32.  $y_1' = \cos y_2$

$y_2' = 3y_1$

33.  $y_1' = y_2 - 2y_2^2$

$y_2' = y_1 - 2y_1^2$

**SUMMARY OF CHAPTER 4****Systems of ODEs. Phase Plane. Qualitative Methods**

Whereas single electric circuits or single mass–spring systems are modeled by single ODEs (Chap. 2), networks of several circuits, systems of several masses and springs, and other engineering problems lead to **systems of ODEs**, involving several unknown functions  $y_1(t), \dots, y_n(t)$ . Of central interest are **first-order systems** (Sec. 4.2):

$$\mathbf{y}' = \mathbf{f}(t, \mathbf{y}), \quad \text{in components,} \quad \begin{array}{l} y_1' = f_1(t, y_1, \dots, y_n) \\ \vdots \\ y_n' = f_n(t, y_1, \dots, y_n), \end{array}$$

to which higher order ODEs and systems of ODEs can be reduced (Sec. 4.1). In this summary we let  $n = 2$ , so that

$$(1) \quad \mathbf{y}' = \mathbf{f}(t, \mathbf{y}), \quad \text{in components,} \quad \begin{array}{l} y_1' = f_1(t, y_1, y_2) \\ y_2' = f_2(t, y_1, y_2) \end{array}$$

Then we can represent solution curves as **trajectories** in the **phase plane** (the  $y_1y_2$ -plane), investigate their totality [the “**phase portrait**” of (1)], and study the kind and **stability** of the **critical points** (points at which both  $f_1$  and  $f_2$  are zero), and classify them as **nodes**, **saddle points**, **centers**, or **spiral points** (Secs. 4.3, 4.4). These phase plane methods are **qualitative**; with their use we can discover various general properties of solutions without actually solving the system. They are primarily used for **autonomous systems**, that is, systems in which  $t$  does not occur explicitly.

A **linear system** is of the form

$$(2) \quad \mathbf{y}' = \mathbf{A}\mathbf{y} + \mathbf{g}, \quad \text{where} \quad \mathbf{A} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}, \quad \mathbf{y} = \begin{bmatrix} y_1 \\ y_2 \end{bmatrix}, \quad \mathbf{g} = \begin{bmatrix} g_1 \\ g_2 \end{bmatrix}.$$

If  $\mathbf{g} = \mathbf{0}$ , the system is called **homogeneous** and is of the form

$$(3) \quad \mathbf{y}' = \mathbf{A}\mathbf{y}.$$

If  $a_{11}, \dots, a_{22}$  are constants, it has solutions  $\mathbf{y} = \mathbf{x}e^{\lambda t}$ , where  $\lambda$  is a solution of the quadratic equation

$$\begin{vmatrix} a_{11} - \lambda & a_{12} \\ a_{21} & a_{22} - \lambda \end{vmatrix} = (a_{11} - \lambda)(a_{22} - \lambda) - a_{12}a_{21} = 0$$

and  $\mathbf{x} \neq \mathbf{0}$  has components  $x_1, x_2$  determined up to a multiplicative constant by

$$(a_{11} - \lambda)x_1 + a_{12}x_2 = 0.$$

(These  $\lambda$ 's are called the **eigenvalues** and these vectors  $\mathbf{x}$  **eigenvectors** of the matrix  $\mathbf{A}$ . Further explanation is given in Sec. 4.0.)

A system (2) with  $\mathbf{g} \neq \mathbf{0}$  is called **nonhomogeneous**. Its general solution is of the form  $\mathbf{y} = \mathbf{y}_h + \mathbf{y}_p$ , where  $\mathbf{y}_h$  is a general solution of (3) and  $\mathbf{y}_p$  a particular solution of (2). Methods of determining the latter are discussed in Sec. 4.6.

The discussion of critical points of linear systems based on eigenvalues is summarized in Tables 4.1 and 4.2 in Sec. 4.4. It also applies to nonlinear systems if the latter are first linearized. The key theorem for this is Theorem 1 in Sec. 4.5, which also includes three famous applications, namely the pendulum and van der Pol equations and the Lotka–Volterra predator–prey population model.