# **Gerhard Lammel: "Trends and Advances in Atmospheric and Environmental Chemistry"**

Budgeting atmospheric processes Halogenated SOCs and multicompartmental substances Air-surface mass exchange processes

## **4 Trace substance mass budgets, surface cycling:**

**Emissions, deposition, re-volatilisation** 

## 4.1 Mass budget equation, residence time



WATER S

SOILS

 $dm_{i}/dt = sources - sinks = E_{i} - S_{i} = E_{i} - (k_{i \text{ degrad}}^{(1)} + k_{i \text{ dep}}^{(1)}) m_{i} = m_{i}/\tau$ [g/s]  $dc_{i}/dt = E_{i} - S_{i} = E_{i} - (k_{i \text{ degrad}}^{(1)} + k_{i \text{ dep}}^{(1)}) c_{i} = c_{i}/\tau$ [g/m3/s]

 $dc_{i}/dt = E_{i} - S_{i} = F_{i \text{ em}}/h - (k_{i \text{ degrad}}^{(1)} + k_{i \text{ dep}}^{(1)}) c_{i} = c_{i}/\tau_{air} \qquad [g/m^{3}/s]$ 

- Chemical loss processes of i are 1<sup>st</sup> order in c<sub>i</sub>
- Source processes of i are 0<sup>th</sup> order in c<sub>i</sub>

Depositional loss processes are here expressed as  $1^{st}$  order in  $c_i$  for simplicity For  $dm_i/dt = 0$ , the system is called to be chemically in a <u>steady state</u>

Variability and atmospheric residence time:

$$\begin{array}{ll} dm_i/dt = (F_{i\ in} + E_i) - (F_{i\ out} + S_i) \\ \text{with:} & F_{i\ in}, F_{i\ out} = \text{fluxes over boundary} \\ & E_i, S_i = \text{internal sources and sinks} \\ & m_i = M_{g\ i}/M_{g\ air} < x_i > m_{trop} \\ & M_{g\ i}, M_{g\ air} = \text{molar masses } (M_{air} = 29\ g/\text{mol}) \\ & < x_i > = \text{spatial average of mixing ratio} \\ & m_{trop} = \text{mass of tropospheric air} = 4.25 \times 10^{15}\ t \end{array}$$

$$\begin{split} S_i &= (\Sigma_j \; k_{ij}{}^{(2)} N_j / V + j_i{}^{(1)}) \; N_i / V = k_V{}^{(1)} N_i / V \\ \text{with:} \quad k_{ji}{}^{(2)}, j_i{}^{(1)} = \text{rate coefficients, photolysis rates} \\ &N_i / V, N_j / V = \text{reaction partner number concentrations} \\ &k_V{}^{(1)} = \text{tropospheric average chemical sink rate coefficient} \\ \text{If well mixed or almost well mixed: advective losses } F_i{}_{i \text{ out}} \\ F_i{}_{out} \sim m_i = k_F \; m_i; \qquad \text{with:} \; k_F = \text{empiric parameter} \\ dm_i / dt = F_i{}_{i \text{ in}} + E_i + (k_F + k_V{}^{(1)}) \; m_i \\ \tau_i = (k_F + k_V{}^{(1)})^{-1}; \; \text{with:} \; \tau_i = \text{residence time } (not \; equal \; to \; but < , lifetime `!) \\ & \text{assuming (in 1st approx.) that } k_V{}^{(1)} \neq f(m_i), \; i.e. \; \text{no chemical feedbacks} \\ & \text{leading to } N_j / V = f(N_i / V) \end{split}$$

Averaging over long times (> mixing times) <u>steady state</u>-assumption holds:  $dm_i/dt = \langle F_{i in} \rangle + \langle E_i \rangle - (k_F + k_V^{(1)}) m_i \approx 0$ 

$$N_i/V = \langle N_i/V \rangle + (N_i/V)'(x, y, z, t);$$
  
with:  $\langle N_i/V \rangle =$  temporally and spatially mean number concentration  
 $(N_i/V)' =$  local and temporal number concentration  
x, y, z = space coordinates

Empiric finding (*Junge*, 1974) for the relative standard deviation  $\sigma_i = \sigma_i^* ((N_i/V)^{\circ}) / \langle N_i/V \rangle = 0.14 / \tau_i$ 

with:  $\sigma_i^*((N_i/V)) = absolute$ standard deviation of  $(N_i/V)$ 

 $\rightarrow$  The residence time,  $\tau_i$ , can be inferred from variability, as  $\sigma_i = f(\tau_i)$ 



## 4.2 Emissions

- location: mostly from ground, from stacks, from aircrafts
- temporal profile, e.g. diel, weekly, seasonal, historical trendsspatial distributions

#### Example: non-methane hydrocarbons (NMHC)

#### Global budget (Tg/a)

Natural	1150	terrestrial vegetation
	2	marine biosphere

Anthropogenic 120 of which are:

52 % transport

- 7 % fossil fuels, stationary
- 5 % chemical, petrochemical industries
- 9 % oil and gas production

27 % solvents

(Ehhalt, 1986; Guenther et al., 1996)

# **Global** Model results



(Crutzen & Gidel, 1983)

#### Global distributions CO (ppbv) @ 970 and 510 hPa, monthly mean





Legende	Global	Prozen
	643×1012	Technologische Quellen
	- 636 × 1012	Deposition am Boden
	- 2054 ×1012	CO + OH Oxidation
	566 × 1012	CH4 + OH Oxidations - Quellen
	± 194 × 1012	Transport
	1483×1012	Tropische Quellen

(Model results: Horowitz et al., 2003; Crutzen & Gidel, 1983)

Distributions – spatial, seasonal

Regional distribution CO (ppbv) @ 300 m 60°N/90°E (ZOTTO)



nolluted air ma

polluted air masses

background

background in the marine boundary layer 60°N

(courtesy of Chi & Andreae 2013)

#### Land use and atmosphere in South America

0.0 0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 1.0



wet season

-40

-50



-10

-20

-30

September 20000907 700 mb

dry season

#### Difference Vegetation Index

## CO column density

(Ranson & Wickland, 2001)



#### **Biomass burning**

Example of the spatial distribution of nighttime active fires given by the ATSR satellite sensor



example of burnt area provided by the GBA-2000 product (*Tansey et al., 2008*)

## Halogenated SOCs and multicompartmental substances Introduction: concerns persistence, bioaccumulation and effects

Many (most) semivolatile and persistent organic substances are accumulating in high latitudes (despite source distribution). Example  $\alpha$ -hexachlorocyclohexane ( $\alpha$ -HCH)



Higher levels in the N Pacific (Iwata et al., 1993)



FIGURE 2. Variation in the concentration of  $\alpha$ -HCH in the upper water column with latitude:  $\alpha$ -HCH (ng L<sup>-1</sup>) = 0.0206 × latitude + 0.72 ( $r^2 = 0.11$ ).

N-S gradient in the Bering and Chukchi Seas (Jantunen & Bidleman, 1995)

## Decreasing trends in air and water not necessarily followed in organisms: Bioaccumulation along food chains







## 6.2.2.2 SOCs surface exchange 6.2.2.1 Air-sea exchange

= volatilisation and dry deposition of (gaseous) molecules

- gas flux through interface F = - $v_{wg}$  ( $c_w - c_{wi}$ ) = - $v_{gw}$  ( $c_{gi} - c_g$ ) [mol/m<sup>2</sup>/s] with  $c_{wi} = c_g / K_{aw}$ 

- all physics hidden in v; equilibrium established at the interface itself

#### <u>*Two film model*</u> (or: two film theory of gas absorption)

- existence of 2 stagnant layers on either side of the interface = transition zone from fully turbulent to molecular conditions

- provide resistance additively  $R_{aw} = R_a + R_w \Leftrightarrow 1/v_{aw} = 1/v_w + 1/(v_a K_{aw})$ 



(Liss & Slater, 1974; Schwarzenbach et al., 2002)

$$\mathbf{F}_{aw} = \mathbf{k}_{mt} \left( \mathbf{c}_{w} - \mathbf{c}_{a} / \mathbf{K}_{aw} \right)$$

Mass transfer coefficient k<sub>mt</sub> (often K<sub>ol</sub>) H'= dimensionless Henry coefficient K<sub>aw</sub>

(courtesy of M. Tsapakis)

#### Two film model (followed)

- there is a water-phase and an air-phase controlled regime existing

-  $1/v_{aw} = 1/v_w + 1/(v_a K_{aw})$  means that in the water-phase controlled regime the overall transfer velocity is independent, in the air-phase related regime linearly dependent of  $K_{aw}$ . This asymmetry, however, is only related to the decision to relate all concentrations to the reference phase water.



Schematic of overall air-water exchange velocity  $v_{aw}$  as a function of the air-water partition coefficient  $K_{aw}$ . Symmetry as equally frequent renewed surfaces are assumed (not realistic).  $F = -k_{mt w} (c_w - c_{wi}) = -k_{mt a} (c_{ai} - c_a) [mol/m^2/s]$ defined positive for flux from air to water

 $c_{ai} = K_{aw} c_{wi}$ 

with actual bulk  $(c_{w,}c_{a})$  and equilibrium  $(c_{wi}, c_{ai})$  concentrations in water and air

 $F = -k_{mt net} [c_w - c_a R_g T/(c_w H(T,s))] ; salinity s, H [Pa m<sup>3</sup>/mol]),$  $R_g = 8.206 m<sup>3</sup>Pa/K/mol$ 

 $H(T,s) = R_g T K_{aw}(T,s) = R_g T K_{aw}(T) \times 10^{K_s c_s} ; \text{Setschenow constant } K_s \text{ [L/mol]} \\ K_s = 0.04 \log K_{ow} + 0.114 (Ni \& Yalkowsky, 2003)$ 

Resistance by boundary layers: reciprocal transfer coefficients (,piston velocity' k<sub>mt w</sub>, k<sub>mt g</sub> [m/s])

 $R = 1/k_{mt net} = 1/k_{mt w} + R_gT/(k_{mt g} H(T,s)) [s/m]$ consideration of 1 side sufficient for most gases

#### **However:**

Stagnant film model (which ignores non-diffusive mass transport) implies  $F = (D/z)\Delta c$  with diffusion layer thickness z (can be estimated).  $F \sim D$  is not really true.

#### **Other existing conceptual models of air-sea mass exchange:**

- Surface renewal model (interface periodically renewed by turbulence eddies) implies  $F = 2(D/t_a\pi)^{0.5}\Delta c \sim D^{0.5}$ . However, the model is not useful, as the characteristic surface renewal time,  $t_a$ , is not known or experimentally accessible.

- Turbulent fluid flow based model
- Turbulence enhancement by bubbles model: bubbles are created by breaking waves (u > 13 m/s)
- Surface film effects: no direct inhibition but indirect (hydrodynamic: wave dampening (3.6 < u < 13 m/s), suppression of surface renewal...) effects

These conceptual models are not predictive / fail as they are limited to individual processes which in reality combine

#### (review: Johnson, 2000)



Overall air-water transfer velocity as a function of Henry's law coefficient for 2 very different wind regimes.

Result: magnitude of air-water transfer velocity v is determined mainly by wind speed, less by substance (Henry coefficient)

Result of lab and field measurements:  $v_w$  is positively correlated with wind speed, faster for  $u_{10} > 10$  m s<sup>-1</sup>

→ Parameterisations in models are empirically based. Wind dependence:

- 3 linear regimes for the piston velocity  $k_w$
- quadratic  $k_{w CO2}(u) = 0.31 u^2 (Sc/660)^{0.5} cm/s$

(Liss & Merlivat, 1986) (Wanninkhoff, 1992) Empiric relationships to for  $H_2O$ ,  $CO_2$ , and derived for unknown molecule i:

$$\begin{split} k_{\text{mt a H2O}} &= 0.83 \text{ cm s}^{-1} \rightarrow k_{\text{mt g i}} = 0.83 \ (18/M_{\text{gi}})^{0.5} \text{ cm s}^{-1} \text{ ; molecular mass } M_{\text{gi}} \\ (g/\text{mol}) \\ k_{\text{mt w CO2}} &= 0.0056 \text{ cm s}^{-1} \rightarrow k_{\text{mt w i}} = 0.0056 \ (44/M_{\text{gi}})^{0.5} \text{ cm s}^{-1} \\ & (Atlas \& Giam, 1986) \\ k_{\text{mt a H2O}} &= 0.2 \ u_{10} + 0.23 \rightarrow k_{\text{mt g i}} = (D_{\text{g i}}/D_{\text{g H2O}})^{0.67} \ v_{\text{g H2O}} \\ & (Mackay \& Yeun, 1983) \end{split}$$

$$\begin{split} k_{mt w} &= 36 \times (0.2 \ u_{10} + 0.3) \times (D_{i g}/D_{H2O g})^{0.61} \quad ; \text{ wind velocity in 10 m height } u_{10} \\ k_{mt a} &= 0.01 \times (0.45 \ u_{10}^{1.64}) \times (Sc_i/Sc_{CO2})^{-0.5} \quad ; \text{ Schmidt number } Sc := \nu /D \\ & \text{Kinematic viscosity } \nu := \text{fluid viscosity } \mu/\text{fluid density } \rho \\ & (Murphy, 1995) \end{split}$$

Volatilisation rate v determined by sea surface temperature t, wind speed u and concentration in seawater c. Here: p(T), H(T),  $K_{ow}$ ,  $k_{oc}(T)$  and c of DDT Coefficients of determination  $R^2$  (linear correlation) used to find out which of the parameters explains most of the variance of the volatilisation rate.  $R_{tv}^2$ 



Model experiment with transient historic emissions 1950-1990

(Stemmler & Lammel, 2011)



(Stemmler & Lammel, 2009)